# Project Development and Environment Study S.R. 31 

From S.R. 80 (Palm Beach Blvd) to S.R. 78 (Bayshore Rd.)

## Project Traffic Analysis Report Addendum

Financial Project ID: 441942-1-22-01
ETDM No.: 14359
Lee County, Florida
The environmental review, consultation, and other actions required by applicable federal environmental laws for this project are being, or have been, carried out by FDOT pursuant to 23 U.S.C. § 327 and a Memorandum of Understanding dated December 14, 2016 and executed by FHWA and FDOT.

Prepared for the

## Florida Department of Transportation District One



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## Section 1.0 <br> EXECUTIVE SUMMARY

This is an addendum to the Project Traffic Analysis Report (PTAR) which was submitted in April 2020. This addendum was prepared to document the following:

- The change of project analysis years to Opening Year (2025) and Design Year (2045) to be consistent with the "SR 31 PD\&E Study from SR 78 to Cook Brown Road", which is to the immediate north of this study. The PTAR submitted in April 2020 shows Opening Year (2026) and Design Year (2046).
- Revised safety evaluation of SR 31 study corridor (segment only) for a five-year period of 2017-2021.
- Revisions to Annual Average Daily Traffic (AADT) and Design Hour Volumes (DHVs) along the study corridor as a result of the proposed SR 31 realignment to the east and the proposed access modifications.
- Traffic evaluation of the directional median openings located at NW Development Driveway N/RaceTrac Driveway N \& LJ's Lounge Driveway and the traffic evaluation of the proposed full median opening at Marina \& Restaurant Entrance. This full median opening was developed because of the proposed realignment of SR 31 study corridor to the east.

Screening of intersection alternatives for the SR 31 at SR 80 signalized intersection were performed utilizing FDOT's Intersection Control Evaluation (ICE) process and documented separately. Please refer to the "ICE Technical Analysis Memorandum - Traffic and Safety Analysis at SR 80 and SR 31, Lee County, FL, August 2022" for the intersection control strategies that were identified and evaluated as part of this PD\&E Study.

Based on the future year analysis results, the SR 31 study corridor in the No-Build condition is not expected to operate at acceptable LOS condition (LOS D) or better, under both Opening Year (2025) and Design Year (2045) conditions. In the Build condition, the proposed widening of SR 31 to a six-lane facility is expected to improve traffic operations within the study area.

### 1.1 SR 31 at SR 80 Intersection

Please refer to the ICE Memorandum prepared for this intersection as part of this study.

### 1.2 Directional Median Openings

Further, under Build (Option 1) w/ at-grade SR 31 at SR 80 intersection geometry, the proposed directional median openings along SR 31 located at the frontage roads of NW Development Driveway N/ RaceTrac Driveway N and LJ's Lounge are expected to perform at acceptable LOS conditions (LOS D) or better, for the Opening Year (2025). However, in the Design Year (2045) the left turns at the directional median openings are expected to experience excessive delays.

Under Build (Option 2) w/ grade-separated crossover SR 31 at SR 80 intersection geometry, the proposed directional median opening along LJ's Lounge is expected to perform at acceptable LOS conditions (LOS D) or better, for the Opening Year (2025). However, in the Design Year (2045) the left turns at the directional median opening are expected to experience excessive delays.

Based on the operational evaluation of directional median opening traffic conditions, Build (Option 2) w/ grade-separated crossover SR 31 at SR 80 intersection geometry will help in rerouting the LJ's Lounge directional median opening traffic to the Texas U-turn located SR 80 intersection and the Marina Drive (Dock Entrance)/Restaurant Driveway intersection, in the Design Year (2045). Therefore, it is recommended to consider Build (Option 2) based on traffic evaluation results.

### 1.3 SR 31 at Marina and Restaurant Entrance Intersection

The combined Marina Drive (Dock Entrance)/Restaurant Driveway intersection with the proposed realignment of SR 31 showed a need for signalization starting from the Opening Year (2025) conditions based on Synchro operational evaluation and warrants analysis, where warrants 1 and 2 were satisfied.

No change from the PTAR submitted in April 2020.

## Section 3.0 <br> INTRODUCTION

The Florida Department of Transportation (FDOT) District One is conducting a Project Development and Environmental (PD\&E) Study (Financial Project Number - 441942-1-22-01) for SR 31 from SR 80 (Palm Beach Boulevard) to SR 78 (Bayshore Road) in Lee County, Florida. This is an addendum to the Project Traffic Analysis Report (PTAR) which was submitted in April 2020. This addendum was prepared to document the following:

- The change of project analysis years to Opening Year (2025) and Design Year (2045) to be consistent with the "SR 31 PD\&E Study from SR 78 to Cook Brown Road", which is to the immediate north of this study. The PTAR submitted in April 2020 shows Opening Year (2026) and Design Year (2046).
- Revised safety evaluation of SR 31 study corridor (segment only) for a five-year period of 2017-2021.
- Revisions to Annual Average Daily Traffic (AADT) and Design Hour Volumes (DHVs) along the study corridor as a result of the proposed SR 31 realignment to the east and the proposed access modifications.
- Traffic evaluation of the directional median openings located at NW Development Driveway N/RaceTrac Driveway N \& LJ's Lounge Driveway and the traffic evaluation of the proposed full median opening at Marina \& Restaurant Entrance. This full median opening was developed because of the proposed realignment of SR 31 study corridor to the east.

Screening of intersection alternatives for the SR 31 at SR 80 signalized intersection were performed utilizing FDOT's Intersection Control Evaluation (ICE) process and documented separately. Please refer to the "ICE Technical Analysis Memorandum - Traffic and Safety Analysis at SR 80 and SR 31, Lee County, FL, August 2022" for the intersection control strategies that were identified and evaluated as part of this PD\&E Study.

### 3.1 Description of the Project

No change from the PTAR submitted in April 2020.

### 3.2 Objective

No change from the PTAR submitted in April 2020.

### 3.3 Methodology

No change from the PTAR submitted in April 2020.

### 3.4 Transportation Plan Consistency

No change from the PTAR submitted in April 2020.

## TRAFFIC ANALYSIS METHOD

No change from the PTAR submitted in April 2020.

# Section 5.0 <br> EXISTING CONDITIONS 

No change from the PTAR submitted in April 2020 except safety evaluation section.

### 5.1 Existing Roadway Characteristics

No change from the PTAR submitted in April 2020.

### 5.2 Multi-Modal Facilities

No change from the PTAR submitted in April 2020.

### 5.3 Traffic Data Collection

No change from the PTAR submitted in April 2020.

### 5.4 Existing Design Traffic Characteristics

No change from the PTAR submitted in April 2020.

### 5.4.1 K Factor

No change from the PTAR submitted in April 2020.

### 5.4.2 D Factor

No change from the PTAR submitted in April 2020.

### 5.4.3 $\quad T_{24}$ Factor

No change from the PTAR submitted in April 2020.

### 5.5 Existing Year (2019) LOS Analysis

No change from the PTAR submitted in April 2020.

### 5.5.1 Existing Roadway LOS Analysis

No change from the PTAR submitted in April 2020.

### 5.5.2 Existing Year HCM Capacity Analysis

No change from the PTAR submitted in April 2020.

### 5.5.3 Existing Intersection Analysis - Synchro

No change from the PTAR submitted in April 2020.

### 5.6 Safety Evaluation

In addition to the traffic operations, safety is an important consideration in evaluating intersection alternatives. Typically, historical crash data is reviewed to gain an understanding of the current crash patterns at study intersections. Crash records were reviewed, and various crash metrics are summarized to support identification and evaluation of alternatives.

### 5.6.1 Historic Crash Summary

Crash data for the SR 31 segment between SR 80 and SR 78 was obtained for the most recent fiveyear period (2017-2021). A total of 33 crashes were reported during the five-year analysis period. Number of crashes per year varied from one to thirteen. Figure 5-1 shows the crashes by year. Out of the 33 crashes reported, one (3\%) fatal crash, eight (24\%) of the crashes resulted in injuries and the remaining $24(73 \%)$ were property damage only crashes. A pedestrian was involved in the fatal crash which occurred during the daylight, clear weather, dry roadway surface condition and the event happened on the shoulder along SR 31. Based on the long report, the vehicle was traveling southbound on SR 31, north of Palm Beach Boulevard and the pedestrian was walking northbound on the west side paved shoulder. The front right of the vehicle collided with the pedestrian. Rearend crashes accounted for $34 \%$ (11) of the total crashes. Majority of crashes (64\%) occurred under daylight conditions. 3 ( $9 \%$ ) crashes occurred under wet road surface conditions. Figure 5-2 shows the summary of crashes by severity, crash type, lighting conditions and road surface conditions. Crash locations based on type of crashes and severity are depicted on Figure 5-3 and 5-4, respectively.

### 5.6.2 Intersection and Location Specific Crashes

Please refer to the ICE memorandum prepared for the SR 31 at SR 80 intersection for crash analysis related to this intersection.

A total seven crashes were reported at the West Marina Drive intersection. Major contributing factors are rear-ended (43\%), head-on (29\%), and angle crashes (14\%).

Over a period of five years (2017-2021), there were ten crashes that took place on the drawbridge. Out of these crashes, $60 \%$ (6) were rear-end collisions caused by failure to stop. This can most likely be attributed to the drawbridge operation.

Figure 5-1: SR 31 Segment Crash History


Figure 5-2: SR 31 Segment Crash Summary (2017-2021)


Figure 5-3: Location and Type of Crashes


Figure 5-4: Location and Severity of Crashes


### 5.6.3 Segment Crash Safety Ratio

Segment crash safety ratio was calculated to compare the annual crash rate of the midblock of SR 31 to the critical crash rate of similar segment throughout District One, Lee County. This method has historically been used by theFDOT and some local agencies to identify high crash locations. This method considers the traffic volumes at specific sites, considers the variance in crash data by including regional or statewide averages, and classifies roadway/intersection types into categories for more applicable comparisons. However, the safety crash ratio method includes the following limitations:

- Assumes a linear relationship between traffic volume and crashes
- Does not consider crash severity

The critical crash rate is based on the average crash rate for a similar facility adjusted by vehicle exposure and a probability constant. The safety ratio represents the actual crash rate divided by the critical crash rate. If a segment has an actual crash rate higher than the critical crash rate (i.e., safety ratio > 1.0), it may have a safety deficiency. Based on Table 5-1, the safety ratio for this segment is less than one.

Table 5-1: Segment Crash Safety Ratio

| Description | Total <br> Crashes | Actual <br> Crash Rate | Average Crash <br> Rate* | Critical <br> Crash Rate | Safety <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SR 31 Segment | 33 | 1.057 | 0.446 | 1.258 | 0.841 |

*FDOT CAR Lee County, 5-year Average Crash Rate(2015-2019). See AppencixA
Crash Rate Crashes per Million Vehicle Miles Travelled (MVMT)
Rural 2-3Ln 2Wy Undivided

### 5.6.4 Highway Safety Manual (HSM) - Predictive Crash Analysis

The ICE memorandum completed for the SR 31 at SR 80 intersection includes predictive safety analysis for segment of SR 31study corridor from SR 80 to LJ's Lounge Driveway. This addendum includes predictive safety analysis for the SR 31 study corridor from LJ's Lounge Driveway to south of SR 78, which is the northern section of the study corridor. The analysis was conducted using the predictive methods in Chapters 12 of the HSM, Urban and Suburban Arterials (750-02021c), which apply a combination of Safety Performance Functions (SPFs), crash modification factors (CMFs), and calibration factors to estimate crash frequency for each segment and intersection. The tool was adjusted based on the crash distribution for Florida based on Table 122.6.4 from the FDOT Design Manual 2022. The growth rates were estimated based on 2025 and 2045 AADTs for this study.

Note that the resulting predictions should be used with caution if the input AADTs (highlighted cell in the HSM tools) exceed the range of data used to develop one or more of the SPFs. The SPFs to local conditions were calibrated by applying calibration factors shown in Table 122.6.3 of the

FDOT Design Manual 2022. The Empirical Bayes method is used when the proposed modification does not create a major geometric modification; therefore, the analysis is performed starting from the existing year of the project. However, Empirical Bayes method is not applicable for this project due to major improvement along SR 31 project corridor.

It is important to note that the safety analysis tools available to date are deterministic in nature and estimate future crashes mainly based on AADT and roadway characteristics. These tools do not account for vehicle interactions (driver behaviors). No-Build is expected to have extensive congestion and queues that may potentially impact crashes. Consequently, crash frequency would be higher compared to Build. Nevertheless, the overall predicted crashes are lower by $44 \%$ for Build when compared to No-Build alternative due to added capacity along the SR 31. However, predictive crashes anticipated to increase under Build alternative at the intersection of Marina Drive (Dock Entrance)/ Restaurant Entrance and SR 31 intersection due to installation traffic signal. Traffic signal do not always prevent crashes. In many instances, the total number of crashes and injuries increase after installation of the traffic signal. However, most comment results showed that a reduction in right-angle collisions which is prone to severe crash injury. Detailed analyses are provided in Appendix B.

## Section 6.0 DEVELOPMENT OF FUTURE YEAR TRAFFIC FORECASTS

Future year traffic forecasts for the major roadways in the study area were developed by the Department as part of the PD\&E study conducted on SR 31 from SR 80 to Cook Brown Road. These major roadway traffic forecasts and local developments adjacent to the project corridor were used to develop study corridor specific AADTs and DHVs for the No-Build condition and were documented in the "Traffic Forecasts Memorandum" prepared as part of this study.

The No-Build traffic forecasts and the access plan prepared for the Build alternatives was used to develop the Build traffic forecasts for this study. The Build alternatives access management plan is documented in the "Access Management Memorandum" prepared for this study.

### 6.1 Description of Alternatives

Based on discussions with the Department, No-Build Alternative and a Build Alternative were evaluated for Opening Year and Design Year. All the alternatives considered are described in this section.

### 6.1.1 No-Build Alternative

Similar to existing conditions, the No-Build Alternative assumes that the SR 31 project corridor is a two-lane arterial facility. The intersection geometries and driveway access locations were also assumed to be the same as existing in the No-Build condition.

### 6.1.2 Build Alternatives

SR 31 is planned to be widened to a six-lane divided facility from SR 80 to Horseshoe Road and a four-lane divided facility from Horseshoe Road to Cook Brown Road. Therefore, within the project limits, SR 31 is assumed to be six-lane divided facility.

The proposed intersection geometries and median opening/ driveway access locations in the Build condition differ from the No-Build as the proposed corridor is a divided roadway. Also, in the proposed Build alternatives, the median opening/ driveway locations vary depending on whether SR 31 at SR 80 intersection is at-grade or grade-separated.

The location of median openings for Build (Option 1) w/ at-grade SR 31 at SR 80 intersection geometry are listed below:

- Directional Median Openings:
- SR 31 at Frontage Roads (NW Development Driveway N/ RaceTrac Driveway N)
- SR 31 at LJ's Lounge
- Full Median Opening
- SR 31 at Marina and Restaurant Entrance

The location of median openings for Build (Option 2) w/ grade-separated crossover SR 31 at SR 80 intersection geometry are listed below:

- Directional Median Openings:
- SR 31 at LJ's Lounge
- Full Median Opening
- SR 31 at Marina and Restaurant Entrance

The screening of alternatives for the SR 31 at SR 80 signalized intersection were performed utilizing FDOT's ICE process and documented separately. Please refer to the "ICE Technical Analysis Memorandum - Traffic and Safety Analysis at SR 80 and SR 31, Lee County, FL, August 2022" for the intersection control strategies that were identified and evaluated as part of this PD\&E Study.

Figure 6-1 shows the No-Build schematic diagram and the proposed Build configuration schematic diagrams with the revised alignment and access changes.

### 6.2 AADTs and DHVs

Figure 6-2 illustrates the No-Build and Build AADTs for the major road segments and driveways within the study area for Opening Year (2025) and Design Year (2045).

Figure 6-3 and 6-4 illustrates the No-Build DHVs for Opening Year (2025) and Design Year (2045), respectively.

Figure 6-5, 6-6, 6-7 and 6-8 illustrates the Build DHVs for Opening Year (2025) and Design Year (2045), respectively. The Build configuration assumes the proposed access changes along the project corridor to re-distribute the driveway traffic along the project corridor

### 6.3 Lane Geometry

Figure 6-9 and 6-10 illustrates the intersection geometry used for the Build analysis.

Figure 6-1: No-Build and Build Configuration Schematics


Figure 6-2: Annual Average Daily Traffic (AADT) Volumes


Figure 6-3: No-Build - Opening Year (2025) Design Hour Volumes


5


4


3


Figure 6-4: No-Build - Design Year (2045) Design Hour Volumes

$(5)$


4


Figure 6-5: Build (Option 1) - Opening Year (2025) Design Hour Volumes

## At-Grade: SR 31 at SR 80 Intersection



|  | Driveway |
| :---: | :---: |
|  | Roadway |
| "-": | Proposed Driveway |
|  | Proposed Realignment |
| XX(XX) | AM(PM) |
| ST0P | Stop Control |
| 吾 | Signal Control |
| 部 | Proposed Signal Control |

(4)

(3)


(2)
$\stackrel{\rightharpoonup}{-}$


Figure 6-6: Build (Option 1) - Design Year (2045) Design Hour Volumes
At-Grade: SR 31 at SR 80 Intersection


|  | Driveway |
| :---: | :---: |
|  | Roadway |
| "-": | Proposed Driveway |
|  | Proposed Realignment |
| $\mathrm{XX}(\mathrm{XX})$ | AM(PM) |
| STop | Stop Control |
| 否 | Signal Control |
| 部 | Proposed Signal Control |

4

(3)


(2)
(1)


Figure 6-7: Build (Option 2) - Opening Year (2025) Design Hour Volumes
Flyover Overpass with Crossover: SR 31 at SR 80 Intersection


|  | Driveway |
| :---: | :---: |
| - | Roadway |
|  | Proposed Bridge |
| ""*" | Proposed Driveway |
|  | Proposed Realignment |
| $\mathrm{xx}(\mathrm{XX})$ | AM(PM) |
| ST0\% | Stop Control |
| 产 | Signal Control |
| 害 | Proposed Signal Control |

4


3


Figure 6-8: Build (Option 2) - Design Year (2045) Design Hour Volumes
Flyover Overpass with Crossover: SR 31 at SR 80 Intersection


|  | Driveway |
| :---: | :---: |
|  | Roadway |
| --"." | Proposed Driveway |
|  | Proposed Realignment |
|  | Proposed Bridge |
| XX(XX) | AM(PM) |
| ST00 | Stop Control |
| 䂞 | Signal Control |
| 찰 | Proposed Signal Control |

4


3

2

1


Figure 6-9: Build Alternative (Option 1) - Lane Geometry
At-Grade: SR 31 at SR 80 Intersection

4

|  | Driveway |
| :---: | :---: |
|  | Roadway |
| ":- = | Proposed Driveway |
| $1 \times \square$ | Proposed Realignment |
| $\leftarrow$ | Existing Lanes |
| $4 . .$. | Proposed Lanes |
| S508 | Stop Control |
| 硈 | Signal Control |
| \% | Proposed Signal Control |


2


Figure 6-10: Build Alternative (Option 2) - Lane Geometry
FLyover Overpass with Crossover: SR 31 at SR 80 Intersection


|  | Driveway |
| :---: | :---: |
|  | Roadway |
| -*-"* | Proposed Driveway |
|  | Proposed Bridge |
| 1■■ | Proposed Realignment |
| $\leftarrow$ | Existing Lanes |
| $4 . .$. | Proposed Lanes |
| ST0P | Stop Control |
| 홉 | Signal Control |
| \# | Proposed Signal Control |



Utilizing the forecasted volumes, future year capacity analyses was performed for opening year (2025) and design year (2045). This section provides a summary of the traffic analysis conducted for No-Build and Build alternatives. Screening of intersection alternatives for the SR 31 at SR 80 signalized intersection were performed utilizing FDOT's ICE process and documented separately. Please refer to the "ICE Technical Analysis Memorandum - Traffic and Safety Analysis at SR 80 and SR 31, Lee County, FL, August 2022" for the intersection control strategies that were identified and evaluated as part of this PD\&E Study.

### 7.1 Future Year Roadway Analysis

No change from the PTAR submitted in April 2020. The analysis years changed to Opening Year (2025) and Design Year (2045). However, the traffic volumes used for the analysis remained the same.

### 7.1.1 No-Build Alternative HCM Capacity Analysis

No change from the PTAR submitted in April 2020.

### 7.1.2 Build Alternative HCM Capacity Analysis

No change from the PTAR submitted in April 2020.

### 7.2 Future Year Intersection Analysis

Intersection analysis was conducted using Synchro. The delay and LOS conditions at the signalized and unsignalized conditions were reported using the HCM $6^{\text {th }}$ Edition module in Synchro. The following intersections were evaluated under the Build conditions:

- Directional Median Openings:
- SR 31 at Frontage Roads (NW Development Driveway N/ RaceTrac Driveway N) - This directional median opening was proposed only with the at-grade (Option 1) SR 31 and SR 80 intersection geometry.
- SR 31 at LJ's Lounge - This directional median opening was proposed with both at-grade (Option 1) and grade-separated (Option 2) SR 31 and SR 80 intersection geometry
- Full Median Opening

SR 31 at Marina and Restaurant Entrance (Signal) - Preliminary evaluation conducted for this median opening by assuming bi-directional and full median openings (without a signal) has shown excessive delay conditions for the traffic entering and exiting the Marina and Restaurant Entrance driveway. This median opening will remain signalized under both at-grade (Option 1) and grade-separated (Option 2) SR 31 and SR 80 intersection geometry. Appendix C presents the preliminary synchro evaluation results for this median opening.

### 7.2.1 Warrants Analysis - SR 31 at Marina and Restaurant Entrance Intersection

In addition to the preliminary Synchro analysis conducted for the SR 31 at Marina and Restaurant Entrance intersection, a traffic signal warrants analysis as outlined in the Manual of -Uniform Traffic Control Devices (MUTCD), was also performed for the Opening Year (2025), Mid-Year (2035) and Design Year (2045) conditions using form 750-020-01. The eight-hour volumes required for future traffic evaluation were developed based on existing traffic counts collected at the Marina and Restaurant driveways and SR 31. The following warrants were applicable for this intersection and were evaluated:

Warrant 1 (eight-hour vehicular volume) - This warrant is applicable where a large volume of intersecting traffic is the principal reason to consider a traffic signal. To meet this warrant, specific traffic volumes on the major street and the higher volume minor street approach must be met or exceeded for at least eight hours on an average day. Because the traffic volume on major street (SR 31) is heavy and the traffic on the minor intersecting street suffers excessive delay, the Interruption of Continuous Traffic, Condition B, volume thresholds were used in Warrant 1. In addition, the $70 \%$ volume level was used as one of the volume level criteria in accordance with the MUTCD guidelines as the proposed posted speed limit along SR 31 in the Build condition is 45 mph . This warrant was satisfied as Warrant 1 - Condition B is $100 \%$ met for eight hours.

Warrant 2 (four-hour vehicular volume) - Four Hour Vehicular Volumes: This warrant is intended to be applied where the volume of the intersecting traffic is the principal reason to install a traffic signal. This warrant requires the volumes of any four hours to be plotted above the applicable curve, shown on analysis sheets for Warrant 2. This warrant was satisfied as four-hour volumes were plotted above the applicable curve.

A summary of the warrant analysis results is presented in Table 7-1. Appendix D presents the eight-hour peak volumes developed for warrants analysis and the signal warrants evaluation worksheets.

Table 7-1: Warrants Analysis - SR 31 at Marina and Restaurant Entrance

| Warrant \# | Warrant Name | Satisfied (Yes/No) |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Year 2025 | Year 2035 | Year 2045 |
| $\mathbf{1}$ | Eight-Hour Vehicular Volume | Yes | Yes | Yes |
| $\mathbf{2}$ | Four-Hour Vehicular Volume | Yes | Yes | Yes |

### 7.2.2 No-Build Alternative Intersection Analysis

Intersection analysis was not conducted for the No-Build alternative as the segment analysis from the PTAR submitted in April 2020 reported LOS F conditions.

### 7.2.3 Build Alternative Intersection Analysis

The Build condition intersection evaluation was conducted for the Opening Year (2025) and Design Year (2045). The delay and LOS conditions are presented in Table 7-2 and 7-3 when analyzed with at-grade SR 31 at SR 80 intersection geometry (Option 1) for the Opening Year (2025) and Design Year (2045), respectively. The delay and LOS conditions are presented in Table 7-4 and 7-5 when analyzed with grade-separated crossover SR 31 at SR 80 intersection geometry (Option 2) for the Opening Year (2025) and Design Year (2045), respectively.

## Build (Option 1): w/ At-Grade SR 31 at SR 80 Intersection Geometry

The directional median opening intersections located at the frontage roads of NW Development Driveway N/ RaceTrac Driveway N and LJ's Lounge are expected to perform under acceptable LOS conditions for the Opening Year (2025). However, under the Design Year (2045) conditions the directional median opening intersections are expected to experience excessive delays.

Traffic operational analysis conducted for the combined Marina Drive (Dock Entrance)/Restaurant Driveway with the proposed realignment of SR 31 and with signalization shows acceptable LOS conditions.

## Build (Option 2): w/ Grade-Separated crossover SR 31 at SR 80 Intersection Geometry

The directional median opening intersections located at LJ's Lounge is expected to perform under acceptable LOS conditions for the Opening Year (2025). However, under the Design Year (2045) conditions this directional median opening is expected to experience excessive delays.

Similar to Build Option 1, Traffic operational analysis conducted for the combined Marina Drive (Dock Entrance)/Restaurant Driveway with the proposed realignment of SR 31 and with signalization shows acceptable LOS conditions.
Appendix E presents the Synchro analysis outputs for the Opening Year (2025) and Design Year (2045) conditions.

Table 7-2: Build (Option 1) - Opening Year (2025) Intersection Delay/LOS

| AM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Cross-Street | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  | Overall |
|  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| SR 31 | SR 80** | Refer to ICE Memorandum |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Frontage Roads <br> NW Dev. Drwy N/RaceTrac Drwy N* | - | - | 16.8/C | - | - | 14.4/B | 19.5/C | - | - | 15.1/C | - | - | 19.5/C |
|  | LJs Lounge* | - | - | - | - | - | 0/A | 14.1/B | - | - | 12.2/B | - | - | 14.1/B |
|  | Marina Dr (Dock Ent)/ Restaurant Drwy** | 26.6/C | 0/A | 30.1/C | 27.3/C | 0/A | 0/A | 38.3/D | 6.6/A | 7/A | 36.8/D | 8.2/A | 6/A | 10/A |
| PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SR 31 | SR 80** | Refer to ICE Memorandum |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Frontage Roads <br> NW Dev. Drwy N/RaceTrac Drwy N* | - | - | 26.1/D | - | - | 24.1/C | 19.3/C | - | - | 32.6/D | - | - | 32.6/D |
|  | LJs Lounge* | - | - | - | - | - | 18.2/C | 14.2/B | - | - | 21.5/C | - | - | 21.5/C |
|  | Marina Dr (Dock Ent)/ Restaurant Drwy** | 24.8/C | 0/A | 30.2/C | 24.7/C | 0/A | 0/A | 38.1/D | 8.8/A | 9.4/A | 35.6/D | 9/A | 7.4/A | 11.6/B |

Note: 00.0/X - Delay/LOS. LOS E and LOS F movements are shown in yellow and orange, respectively. Delay is reported in sec/veh

* Unsignalized intersections with directional median openings/ ** Signalized intersections

Worst movement delay was reported as overall intersection delay for unsignalized intersections
Table 7-3: Build (Option 1) - Design Year (2045) Intersection Delay/LOS

| AM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Cross-Street | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  | Overall |
|  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| SR 31 | SR 80** | Refer to ICE Memorandum |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Frontage Roads <br> NW Dev. Drwy N/RaceTrac Drwy N* | - | - | 89.4/F | - | - | 38.7/E | 227.6/F | - | - | 130/F | - | - | 227.6/F |
|  | LJs Lounge* | - | - | - | - | - | 0/A | 131.9/F | - | - | 47.7/E | - | - | 131.9/F |
|  | Marina Dr (Dock Ent)/ Restaurant Drwy** | 45.1/D | 0/A | 51.2/D | 46.9/D | 0/A | 0/A | 65.3/E | 9.1/A | 10.2/B | 58.7/E | 16.1/B | 5.8/A | 15.4/B |
| PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SR 31 | SR 80** | Refer to ICE Memorandum |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Frontage Roads <br> NW Dev. Drwy N/RaceTrac Drwy N* | - | - | 520.9/F | - | - | 541/F | 300.8/F | - | - | - | - | - | 541/F |
|  | LJs Lounge* | - | - | - | - | - | 105.4/F | 141.7/F | - | - | 1574.1/F | - | - | 1574.1/F |
|  | Marina Dr (Dock Ent)/ Restaurant Drwy** | 37.7/D | 0/A | 46/D | 38.9/D | 0/A | 0/A | 51.8/D | 17/B | 20.8/C | 52.8/D | 14/B | 7.3/A | 18.3/B |

Note: 00.0/X - Delay/LOS. LOS E and LOS F movements are shown in yellow and orange, respectively. Delay is reported in sec/veh

* Unsignalized intersections with directional median openings/ ** Signalized intersections

Worst movement delay was reported as overall intersection delay for unsignalized intersections

Table 7-4: Build (Option 2) - Opening Year (2025) Intersection Delay/LOS

| AM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Cross-Street | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  | Overall |
|  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
|  | SR 80** | Refer to ICE Memorandum |  |  |  |  |  |  |  |  |  |  |  |  |
| SR 31 | Frontage Roads <br> NW Dev. Drwy N/RaceTrac Drwy N* | Not Applicable |  |  |  |  |  |  |  |  |  |  |  |  |
|  | LJs Lounge* | - | - | - | - | - | 0/A | 14.7/B | - | - | 12.2/B | - | - | 14.7/B |
|  | Marina Dr (Dock Ent)/ Restaurant Drwy** | 26.6/C | 0/A | 30.1/C | 27.3/C | 0/A | 0/A | 38.3/D | 6.6/A | 7/A | 36.8/D | 8.2/A | 6/A | 10/A |
| PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SR 31 | SR 80** | Refer to ICE Memorandum |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Frontage Roads <br> NW Dev. Drwy N/RaceTrac Drwy N* | Not Applicable |  |  |  |  |  |  |  |  |  |  |  |  |
|  | LJs Lounge* | - | - | - | - | - | 18.2/C | 16.3/C | - | - | 21.5/C | - | - | 21.5/C |
|  | Marina Dr (Dock Ent)/ Restaurant Drwy** | 24.8/C | 0/A | 30.2/C | 24.7/C | 0/A | 0/A | 38.1/D | 8.8/A | 9.4/A | 35.6/D | 9/A | 7.4/A | 11.6/B |

Note: 00.0/X - Delay/LOS. LOS E and LOS F movements are shown in yellow and orange, respectively. Delay is reported in sec/veh

* Unsignalized intersections with directional median openings/ ** Signalized intersections

Worst movement delay was reported as overall intersection delay for unsignalized intersections
Table 7-5: Build (Option 2) - Design Year (2045) Intersection Delay/LOS

| AM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Cross-Street | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  | Overall |
|  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| SR 31 | SR 80** | Refer to ICE Memorandum |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Frontage Roads <br> NW Dev. Drwy N/RaceTrac Drwy N* |  |  |  |  |  |  | t Applica |  |  |  |  |  |  |
|  | LJs Lounge* | - | - | - | - | - | 0/A | 231/F | - | - | 47.7/E | - | - | 231/F |
|  | Marina Dr (Dock Ent)/ Restaurant Drwy** | 45.1/D | 0/A | 51.2/D | 46.9/D | 0/A | 0/A | 65.3/E | 9.1/A | 10.2/B | 58.7/E | 16.1/B | 5.8/A | 15.4/B |
| PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SR 31 | SR 80** | Refer to ICE Memorandum |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Frontage Roads <br> NW Dev. Drwy N/RaceTrac Drwy N* | Not Applicable |  |  |  |  |  |  |  |  |  |  |  |  |
|  | LJs Lounge* | - | - | - | - | - | 105.4/F | 368.7/F | - | - | 1574.1/F | - | - | 1574.1/F |
|  | Marina Dr (Dock Ent)/ Restaurant Drwy** | 37.7/D | 0/A | 46/D | 38.9/D | 0/A | 0/A | 51.8/D | 17/B | 20.8/C | 52.8/D | 14/B | 7.3/A | 18.3/B |

Note: 00.0/X - Delay/LOS. LOS E and LOS F movements are shown in yellow and orange, respectively. Delay is reported in sec/veh

* Unsignalized intersections with directional median openings/ ** Signalized intersections

Worst movement delay was reported as overall intersection delay for unsignalized intersections

SUMMARY OF ANALYSIS RESULTS
Based on the future year analysis results, the SR 31 study corridor in the No-Build condition is not expected to operate at acceptable LOS condition (LOS D) or better, under both Opening Year (2025) and Design Year (2045) conditions. In the Build condition, the proposed widening of SR 31 to a six-lane facility is expected to improve traffic operations within the study area.

### 8.1 SR 31 at SR 80 Intersection

Please refer to the ICE Memorandum prepared for this intersection as part of this study.

### 8.2 Directional Median Openings

Further, under Build (Option 1) w/ at-grade SR 31 at SR 80 intersection geometry, the proposed directional median openings along SR 31 located at the frontage roads of NW Development Driveway N/ RaceTrac Driveway N and LJ's Lounge are expected to perform at acceptable LOS conditions (LOS D) or better, for the Opening Year (2025). However, in the Design Year (2045) the left turns at the directional median openings are expected to experience excessive delays.

Under Build (Option 2) w/ grade-separated crossover SR 31 at SR 80 intersection geometry, the proposed directional median opening along LJ's Lounge is expected to perform at acceptable LOS conditions (LOS D) or better, for the Opening Year (2025). However, in the Design Year (2045) the left turns at the directional median opening are expected to experience excessive delays.

Based on the operational evaluation of directional median opening traffic conditions, Build (Option 2) w/ grade-separated crossover SR 31 at SR 80 intersection geometry will help in rerouting the LJ's Lounge directional median opening traffic to the Texas U-turn located SR 80 intersection and the Marina Drive (Dock Entrance)/Restaurant Driveway intersection, in the Design Year (2045). Therefore, it is recommended to consider Build (Option 2) based on traffic evaluation results.

### 8.3 SR 31 at Marina and Restaurant Entrance Intersection

The combined Marina Drive (Dock Entrance)/Restaurant Driveway intersection with the proposed realignment of SR 31 showed a need for signalization starting from the Opening Year (2025) conditions based on Synchro operational evaluation and warrants analysis, where warrants 1 and 2 were satisfied.

## APPENDICES

## Appendix A <br> Lee County - Average Crash Rates Table

| District | County | Crash Rate Category Average C |  | Crash | 边 |  | Average | Average |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Lee | Interstate Urban 0.48592 | 1 | 2395 | 4931 | 142 | 202809 | 221380 |
| 1 | Lee | Interstate Rural 0.33573 | 0 | 163 | 486 | 29 | 208367 | 208169 |
| 1 | Lee | Toll Road Urban 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Toll Road Rural 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Urban Other Limited Acce 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Rural Other Limited Acces 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Ramp Urban 0 | 361 | 38 | 8 | 4 | 96430 | 97034 |
| 1 | Lee | Ramp Rural 0 | 995 | 735 | 258 | 90 | 141823 | 142651 |
| 1 | Lee | Urban 2-3Ln 2Wy Divd Ra: 21.67104 | 205 | 51 | 12 | 3 | 205869 | 194922 |
| 1 | Lee | Urban 2-3Ln 2Wy Divd Pa' 4.10853 | 82 | 363 | 108 | 18 | 94142 | 115001 |
| 1 | Lee | Urban 2-3Ln 2Wy Undivd 6.32592 | 47 | 41 | 14 | 5 | 40777 | 30346 |
| 1 | Lee | Suburban 2-3Ln 2Wy Divd 6.70918 | 39 | 265 | 45 | 6 | 115072 | 129724 |
| 1 | Lee | Suburban 2-3Ln 2Wy Divd 3.29995 | 158 | 685 | 255 | 43 | 257639 | 319875 |
| 1 | Lee | Suburban 2-3Ln 2Wy Und 0.97159 | 22 | 401 | 435 | 94 | 343441 | 428140 |
| 1 | Lee | Rural 2-3Ln 2Wy Divd Rasio | 0 | 0 | 4 | 0 | 0 | 0 |
| 1 | Lee | Rural 2-3Ln 2Wy Divd Pav 2.40905 | 1 | 29 | 12 | 4 | 880936 | 878176 |
| 1 | Lee | Rural 2-3Ln 2Wy Undivd 0.446 | 0 | 26 | 58 | 23 | 656424 | 1082453 |
| 1 | Lee | Urban 4-5Ln 2Wy Divd Ra: 3.12448 | 234 | 2503 | 876 | 83 | 208581 | 212512 |
| 1 | Lee | Urban 4-5Ln 2Wy Divd Pa' 1.80074 | 41 | 354 | 219 | 24 | 273200 | 318362 |
| 1 | Lee | Urban 4-5Ln 2Wy Undivd 5.05676 | 36 | 168 | 40 | 5 | 138064 | 157836 |
| 1 | Lee | Suburban 4-5Ln 2Wy Divd 2.21096 | 471 | 2399 | 1298 | 122 | 230904 | 259283 |
| 1 | Lee | Suburban 4-5Ln 2Wy Divd 1.52661 | 18 | 500 | 339 | 29 | 157394 | 169875 |
| 1 | Lee | Suburban 4-5Ln 2Wy Und 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Rural 4-5Ln 2Wy Divd Ras 0.73886 | 3 | 199 | 273 | 38 | 586538 | 637056 |
| 1 | Lee | Rural 4-5Ln 2Wy Divd Pav 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Rural 4-5Ln 2Wy Undivd 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Urban 6+Ln 2Wy Divd Ras 2.84582 | 324 | 3117 | 1209 | 81 | 155904 | 168539 |
| 1 | Lee | Urban 6+Ln 2Wy Divd Pav 5.1132 | 19 | 1332 | 264 | 17 | 170953 | 175876 |
| 1 | Lee | Urban 6+Ln 2Wy Undivd 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| 1 | Lee | Suburban 6+Ln 2Wy Divd 2.17622 | 276 | 4928 | 2391 | 134 | 172005 | 175905 |
| 1 | Lee | Suburban 6+Ln 2Wy Divd 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Suburban 6+Ln 2Wy Undii0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Rural 6+Ln 2Wy Divd Rasd 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Rural 6+Ln 2Wy Divd Pavc 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Rural 6+Ln 2Wy Undivd 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | Lee | Urban One Way 3.66094 | 127 | 244 | 101 | 23 | 165220 | 193438 |
| 1 | Lee | Suburban One Way 2.95697 | 50 | 48 | 33 | 7 | 453988 | 474594 |
| 1 | Lee | Rural One Way 0 | 2 | 0 | 0 | 15 | 95955 | 114450 |
| 1 | Lee | Undefined 0 | 98 | 158 | 0 | 0 | 220582 | 221619 |
| 1 | Lee | Not Coded 1.59981 | 733 | 21142 | 13673 | 1039 | 198783 | 215063 |


| District | County | Crash Rate Category Total Prow | 倍 | 倍 | , |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Lee | Interstate Urban 1616 | 359 | 293 | 98 |
| 1 | Lee | Interstate Rural 118 | 19 | 19 | 5 |
| 1 | Lee | Toll Road Urban 0 | 0 | 0 | 0 |
| 1 | Lee | Toll Road Rural 0 | 0 | 0 | 0 |
| 1 | Lee | Urban Other Limited Acce 0 | 0 | 0 | 0 |
| 1 | Lee | Rural Other Limited Acces 0 | 0 | 0 | 0 |
| 1 | Lee | Ramp Urban 261 | 82 | 45 | 10 |
| 1 | Lee | Ramp Rural 1097 | 368 | 196 | 57 |
| 1 | Lee | Urban 2-3Ln 2Wy Divd Ra: 154 | 67 | 28 | 4 |
| 1 | Lee | Urban 2-3Ln 2Wy Divd Pa' 257 | 102 | 61 | 25 |
| 1 | Lee | Urban 2-3Ln 2Wy Undivd 64 | 19 | 5 | 0 |
| 1 | Lee | Suburban 2-3Ln 2Wy Divd 182 | 74 | 38 | 9 |
| 1 | Lee | Suburban 2-3Ln 2Wy Divd 463 | 177 | 138 | 53 |
| 1 | Lee | Suburban 2-3Ln 2Wy Und 255 | 83 | 52 | 24 |
| 1 | Lee | Rural 2-3Ln 2Wy Divd Rasio | 0 | 0 | 0 |
| 1 | Lee | Rural 2-3Ln 2Wy Divd Pav 15 | 8 | 4 | 1 |
| 1 | Lee | Rural 2-3Ln 2Wy Undivd 13 | 3 | 3 | 6 |
| 1 | Lee | Urban 4-5Ln 2Wy Divd Ra: 1608 | 665 | 325 | 110 |
| 1 | Lee | Urban 4-5Ln 2Wy Divd Pa' 218 | 95 | 57 | 19 |
| 1 | Lee | Urban 4-5Ln 2Wy Undivd 103 | 72 | 24 | 4 |
| 1 | Lee | Suburban 4-5Ln 2Wy Divd 1574 | 708 | 432 | 121 |
| 1 | Lee | Suburban 4-5Ln 2Wy Divd 285 | 135 | 74 | 21 |
| 1 | Lee | Suburban 4-5Ln 2Wy Und 0 | 0 | 0 | 0 |
| 1 | Lee | Rural 4-5Ln 2Wy Divd Ras 107 | 39 | 31 | 17 |
| 1 | Lee | Rural 4-5Ln 2Wy Divd Pav 0 | 0 | 0 | 0 |
| 1 | Lee | Rural 4-5Ln 2Wy Undivd 0 | 0 | 0 | 0 |
| 1 | Lee | Urban 6+Ln 2Wy Divd Ras 2014 | 894 | 410 | 99 |
| 1 | Lee | Urban 6+Ln 2Wy Divd Pav 749 | 383 | 160 | 47 |
| 1 | Lee | Urban 6+Ln 2Wy Undivd 0 | 0 | 0 | 0 |
| 1 | Lee | Suburban 6+Ln 2Wy Divd 3056 | 1344 | 589 | 173 |
| 1 | Lee | Suburban 6+Ln 2Wy Divd 0 | 0 | 0 | 0 |
| 1 | Lee | Suburban 6+Ln 2Wy Undii0 | 0 | 0 | 0 |
| 1 | Lee | Rural 6+Ln 2Wy Divd Rasd 0 | 0 | 0 | 0 |
| 1 | Lee | Rural 6+Ln 2Wy Divd Pavc 0 | 0 | 0 | 0 |
| 1 | Lee | Rural 6+Ln 2Wy Undivd 0 | 0 | 0 | 0 |
| 1 | Lee | Urban One Way 207 | 120 | 32 | 6 |
| 1 | Lee | Suburban One Way 51 | 21 | 20 | 3 |
| 1 | Lee | Rural One Way 1 | 0 | 1 | 0 |
| 1 | Lee | Undefined 132 | 90 | 24 | 7 |
| 1 | Lee | Not Coded 12855 | 5226 | 2729 | 839 |




## Appendix B HSM Predictive Crash Analysis

In accordance with the Department's Highway Safety Manual Implementation Policy (Topic No. 000-500-001), "the transportation analyst is encouraged to use the Highway Safety Manual (HSM) methods, where applicable, to measure safety benefits from proposed improvements."

### 122.6.1 Historical Crash Method (HCM)

This method can be used for sites with a crash history. The historical crash analysis for Design Exceptions and Design Variations includes a review of crashes from within the FDOT Crash Analysis Reporting (CAR) system database and the SIGNAL FOUR ANALYTICS (SFA) system database. Department approval is required for access to the data within these systems and can be obtained through the district offices.

The FDOT CAR system database includes verified crash data for all fatal and serious injury (KA) crashes typically up to the current date and for all crash types (KABCO) up to 2018 (latest completed data set). These crashes should be included in all HCM analyses. The Signal Four database includes all crash types (KABCO) up to the current date and should be used to supplement the crashes reported from the FDOT CAR system database to establish a complete dataset of crashes over the analysis period. Due to the overlap of crash data within the two systems, proper vetting of the dataset is required to ensure that crashes are not duplicated within the analysis.

The $\mathrm{B} / \mathrm{C}$ (benefit/cost) ratio is the ratio of the estimated annual reduction in crash costs to the estimated annual increase in combined construction and maintenance costs. The annualized conversion will show whether the projected expenditure of funds for the crash benefit will exceed the direct cost for the improvement.

The HCM uses the Highway Safety Improvement Program Guideline (HSIPG) cost per crash by facility type in Table 122.6.1 to estimate benefit to society, while the cost to society is estimated by the expected cost of right of way, construction, and maintenance.

Table 122.6.1 FDOT Average Crash Costs by Facility Type

| Type <br> Facility | Divided Roadway |  |  | Undivided Roadway |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\$ 107,732$ | $\$ 201,527$ | $\$ 355,183$ | $\$ 124,618$ | $\$ 267,397$ | $\$ 523,727$ |
| $4-5$ Lanes | $\$ 123,406$ | $\$ 225,315$ | $\$ 473,637$ | $\$ 112,896$ | $\$ 190,276$ | $\mathrm{n} / \mathrm{a}$ |
| 6+ Lanes | $\$ 123,598$ | $\$ 166,258$ | $\$ 451,492$ | $\$ 41,650$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| Interstate | $\$ 153,130$ | $\mathrm{n} / \mathrm{a}$ | $\$ 327,385$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| Turnpike | $\$ 132,199$ | $\mathrm{n} / \mathrm{a}$ | $\$ 274,012$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |

Notes:
(1) Average Cost/Crash: \$159,093
(2) The above values were derived from 2014 through 2018 traffic crash and injury severity data for crashes on state roads in Florida using the formulation described in FHWA Technical Advisory "Motor Vehicle Accident Costs", T7570.2, dated October 31, 1994. Base costs derived from a memorandum from USDOT: "Guidance on Treatment of the Economic Value of a Statistical Life (VSL) in the U.S. Department of Transportation Analyses", dated August 8, 2016 updating the value of life saved from $\$ 9.4$ million to $\$ 9.6$ million for 2015 data with a growth factor applied to increase the base cost to $\$ 9.7$ million in the current analyses. Costs are computed for the actively state-maintained State Highway System (SHS) only.
(3) Link to Revised Departmental Guidance 2013

When utilizing predictive methods or crash severity distributions for analysis, the following crash severity level costs should be used:

Table 122.6.2 FDOT KABCO Crash Costs

| Crash Severity | Comprehensive Crash Cost |
| :--- | :--- |
| Fatal (K) | $\$ 10,890,000$ |
| Severe Injury (A) | $\$ 888,030$ |
| Moderate Injury (B) | $\$ 180,180$ |
| Minor Injury (C) | $\$ 103,950$ |
| Property Damage Only (O) | $\$ 7,700$ |
| Note: <br> (1) Source: Florida Department of Transportation State Safety Office's Crash Analysis Reporting <br> (CAR) System, analysis years 2014 through 2018. Published by FDOT State Safety Office on <br> 11/5/2020. |  |

### 122.6.2 Roadside Safety Analysis Program (RSAP)

This method complements the AASHTO Roadside Design Guide, dated June 2011. When hazards cannot be removed or relocated, designers need to determine if a safety device, such as a guardrail or a crash cushion, is warranted to protect motorists from the roadside obstacle. This method can be used to perform a benefit/cost analysis comparing a potential safety treatment with the existing or baseline conditions (i.e., the do-nothing option) or alternative safety treatments. Based on the input of information available to the user (e.g., offsets, traffic, slopes, crash history, traffic accident severity levels), the program will offer results which can be used in comparing design alternatives.

### 122.6.3 Highway Safety Manual

The AASHTO Highway Safety Manual (HSM) provides analytical tools and techniques for quantifying the potential effects on crashes as a result of decisions made in planning, design, operations, and maintenance. The new techniques and knowledge in the HSM reflect the evolution in safety analysis from descriptive (historical) methods to quantitative, predictive analyses. In the HSM, crash frequency is the fundamental basis for safety analysis and is used to reduce crashes and severities through the selection of alternative treatments.

The HSM includes Safety Performance Functions (SPFs) for many roadway segment and intersection applications. SPFs are equations used to estimate or predict the expected
average crash frequency per year at a location as a function of traffic volume and roadway characteristics. Adjust SPFs to local conditions by applying calibration factors shown in Table 122.6.3. The use of HSMSPF and Crash Modification Factors (CMF), with an Empirical Bayes (EB) adjustment, provides research-based solutions for use in Benefit/Cost comparisons. Crash distributions presented in Table 122.6.4 and KABCO costs as specified in Table 122.6.2 should be used in determining benefits from an HSM analysis.

Table 122.6.3 HSM Calibration Factors for Florida

|  | Type Facility | Abbreviation | Calibration <br> Factor (Cx) |
| :---: | :---: | :---: | :---: |
| FDOT Roadway Calibration Factors |  |  |  |
| Rural | 2-lane Undivided | R2U | 1.00 |
|  | 4-lane Divided | R4D | 0.68 |
| Urban | 2-lane Undivided | U2U | 1.02 |
|  | 3-lane with a Center Two-Way Left Turn Lane | U32LT | 1.04 |
|  | 4-lane Undivided | U4U | 0.73 |
|  | 4-lane Divided | U4D | 1.63 |
|  | 5-lane with a Center Two-Way Left Turn Lane | U52LT | 0.70 |
| FDOT Intersection Calibration Factors |  |  |  |
| Rural | 2-lane 3-Leg Stop-Controlled | RTL3ST | 1.27 |
|  | 2-lane 4-Leg Stop-Controlled | RTL4ST | 0.74 |
|  | 2-lane 4-Leg Signalized | RTL4SG | 0.92 |
|  | Multilane 3-Leg Stop-Controlled | RML3ST | 2.20 |
|  | Multilane 4-Leg Stop-Controlled | RML4ST | 1.64 |
|  | Multilane 4-Leg Signalized | RML4SG | 0.45 |
| Urban | 3-Leg Stop-Controlled Intersection | USA3ST | 1.14 |
|  | 4-Leg Stop-Controlled Intersection | USA4ST | 1.87 |
|  | 3-Leg Signalized w/o Ped. CMFs | USA3SG w/o Ped. | 2.58 |
|  | 3-Leg Signalized w/ Ped. CMFs | USA3SG w/ Ped. | 2.50 |
|  | 4-Leg Signalized | USA4SG | 2.27 |

Table 122.6.4 HSM Crash Distribution for Florida

| Type Facility |  | Abbreviation | K | A | B | C | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rural Roadways | 2-lane Undivided | R2U | 0.028 | 0.094 | 0.181 | 0.187 | 0.509 |
|  | 4-lane Undivided | R4U | 0.033 | 0.093 | 0.164 | 0.186 | 0.524 |
|  | 4-lane Divided | R4D | 0.028 | 0.090 | 0.187 | 0.196 | 0.499 |
| Urban \& Suburban Arterials | 2-lane Undivided | U2U | 0.009 | 0.050 | 0.150 | 0.224 | 0.567 |
|  | 3-lane TWLTL | U32LT | N/A |  |  |  |  |
|  | 4-lane Undivided | U4U | 0.004 | 0.031 | 0.110 | 0.204 | 0.650 |
|  | 4-lane Divided | U4D | 0.008 | 0.046 | 0.142 | 0.234 | 0.571 |
|  | 5-lane TWLTL | U52LT | N/A |  |  |  |  |
| Freeways | Rural |  | 0.017 | 0.065 | 0.143 | 0.163 | 0.612 |
|  | Urban |  | 0.006 | 0.035 | 0.113 | 0.206 | 0.641 |
|  | Ramps |  | 0.004 | 0.032 | 0.107 | 0.210 | 0.647 |
| All | All Roadways and Ramps |  | 0.007 | 0.041 | 0.124 | 0.217 | 0.611 |
| Notes: | A - Incapacitating Injury <br> K - Fatality <br> B - Non-incapacitating Inju |  |  |  | - Possible (or minor) Injury <br> - Property Damage Only |  |  |
| Data Source: Florida Department of Transportation, State Safety Office's Crash Analysis Reporting (CAR) database, analysis years 2014 through 2018. Publishing by FDOT State Safety Office on 11/5/2020. |  |  |  |  |  |  |  |

Tools and spreadsheets for use with these analytical methods have been developed and are available on the following websites:

## https://safety.fhwa.dot.gov/rsdp/hsm.aspx

## https://www.fdot.gov/roadway/QA/Tools.shtm

### 122.7 Design Approval Request

### 122.7.1 Submittal Package

The submittal package for a Design Exception or a Design Variation will include the same items. However, the required documentation and necessary level of detail will vary depending on the design element being evaluated (as described in FDM 122.4). The Design Exception or Design Variation submittal package is to include the following items:
(1) Submittal/Approval Letter (cover letter): Form 122-A (see FDM 103).
(2) Signed and Sealed Report: The signed and sealed documents including all required documentation and justification (see FDM 122.4 for documentation requirements). Multiple design elements and signed and sealed reports may be included in one submittal package.
(3) Appendices (as needed): Include any support documentation to facilitate an understanding of the report. Supplemental documents do not alter the sealed analysis or design.

Sign and seal the report in accordance with FDM 130. A Submittal/Approval Letter (Form 122-A, see FDM 103) is to be attached to the Signed and Sealed Report and submitted to the District or Turnpike Design Engineer. The District or Turnpike Design Engineer then approves or denies the request and notifies the Responsible Engineer. When further approvals are required, the District or Turnpike Design Engineer will forward the Submittal/Approval Letter and Sealed Report to the State Roadway Design Office.

### 122.7.2 Design Exception Approval

The request will be reviewed by the State Roadway Design Engineer and may be forwarded for approval to the Chief Engineer, the State Structures Design Engineer, the Planning Office, and FHWA, as appropriate.

Each request will be reviewed on a case-by-case basis and approved on its merits. When approval is obtained, the State Roadway Design Office will email the disposition to the District or Turnpike Design Engineer along with the signed Submittal/Approval Letter. The State Roadway Design Office will keep an electronic copy filed under the assigned reference number.

When a request is denied, the State Roadway Design Office will notify the District or Turnpike Design Engineer of the disposition. Denied requests can be resubmitted when all deficiencies, noted in the denial notification, have been addressed. This may require
only a new Submittal/Approval Letter if the Sealed Report does not need to be amended; however, if the Sealed Report requires revision, a new Sealed Report and attached Submittal/Approval Letter must be submitted.

Documentation requirements for Design Exceptions are in FDM 122.4.

### 122.7.3 Design Variation Approval

Design Variations are typically approved at the District level; however, there are specific elements requiring Central Office approval noted in FDM 122.7.4 (see Table 122.7.1). Design Variations requiring Central Office approval must follow the processes in FDM 122.7.2.

Design Variations approved at the District level may be submitted as either a Formal Design Variation or a Design Variation Memorandum for approval by the District or Turnpike Enterprise Design Engineer.

Documentation requirements for Design Variations (both Formal and Memorandums) are in FDM 122.4.

### 122.7.4 Signature Requirements

Obtain all required approvals as described in this section. Approvals from multiple individuals may be required for certain issues. The Director of Design must resolve any approval authority issues if conflicting objectives arise. Approval signatures are required by the following Department and FHWA personnel as specified:

## Chief Engineer:

(1) Design Exceptions for Design Speed on SIS facilities, following review by the Chief Planner.
(2) Design Variations for Design Speed on SIS facilities, following review by the Chief Planner.
(3) Design Variations for omission of Emergency Shoulder Use (ESU) evacuation requirements for any phase of construction.
(4) Design Variation for Shared Use Paths in LA R/W not meeting the criteria in FDM 224.1.1, following review by the Chief Planner.
(5) Design Exceptions or Variations involving lateral offsets or vertical clearances for railroads not meeting the requirements of Rule 14-57 F.A.C. or the clearance
criteria for the South Florida Rail Corridor (Topic No. 000-725-003 - South Florida Rail Corridor Clearance Policy for 25 KV service).
(6) Design Variations for Non-Standard Use of Shoulders. (e.g., Bus on Shoulder Projects, Part-Time Shoulder Use, Hard Shoulder Running, etc.)
(7) Design Exceptions for Paved Shoulder Width on Interstate and Turnpike Facilities.
(8) Design Variations to not install a Railroad Dynamic Envelope (RDE).

## FHWA Division Administrator:

(1) Design Exceptions on Projects of Division Interest (PoDIs).

## District (or Turnpike) Design Engineer:

(1) Design Exceptions
(2) Design Variations

## State Roadway Design Engineer:

(1) Design Exceptions for elements other than Design Loading Structural Capacity.
(2) Design Variations involving the use of fencing around stormwater management facilities.
(3) Design Exceptions or Variations involving lateral offsets or vertical clearances for railroads not meeting the requirements of Rule 14-57 F.A.C. or the clearance criteria for the South Florida Rail Corridor (Topic No. 000-725-003 - South Florida Rail Corridor Clearance Policy for 25 KV service).

## State Structures Design Engineer:

(1) Design Exceptions for Design Loading Structural Capacity of bridges and Vertical Clearance impacting Category 1 and 2 bridge structures.
(2) Design Variations for Design Loading Structural Capacity of bridges and Vertical Clearance impacting Category 2 structures.
(3) Design Variations for Design Loading Structural Capacity due to deficient load ratings impacting both Category 1 and 2 bridge structures.
(4) Design Variations for Traffic Railing impacting Category 1 and 2 bridge structures.
(5) Design Exceptions or Variations involving lateral offsets or vertical clearances for railroads not meeting the requirements of Rule 14-57 F.A.C. or the clearance criteria for the South Florida Rail Corridor (Topic No. 000-725-003 - South Florida Rail Corridor Clearance Policy for 25 KV service).

## District (or Turnpike) Structures Design Engineer:

(1) Design Exceptions for Design Loading Structural Capacity of all structural items and Vertical Clearance impacting Category 1 and 2 bridge structures.
(2) Design Variations for Design Loading Structural Capacity of all structural items and Vertical Clearance impacting Category 1 bridge structures.

Table 122.7.1 Central Office Approvals

| Design Element | State <br> Roadway Design Engineer | State Structures Design Engineer | Chief Planner | Chief Engineer |
| :---: | :---: | :---: | :---: | :---: |
|  | Approval | Approval | Review | Approval |
| Design Speed Exception | X |  |  |  |
| Design Speed Exception-SIS | X |  | X | X |
| Design Speed Variation-SIS |  |  | X | X |
| Design Variation: ESU Omission during Construction |  |  |  | X |
| Design Variation: Shared Use Path in LA R/W |  |  | X | X |
| Design Variation: Non-Standard Shoulder Use |  |  |  | X |
| Design Variations to not install an RDE |  |  |  | X |
| Lane Width Exception | X |  |  |  |
| Shoulder Width Exception | X |  |  |  |
| Paved Shoulder Width Exception (Interstate and Turnpike) | X |  |  | X |
| Maximum Grade Exception | X |  |  |  |
| Cross Slope Exception | X |  |  |  |
| Superelevation Rate Exception | X |  |  |  |
| Horizontal Curve Radius Exception | X |  |  |  |
| Stopping Sight Distance Exception | X |  |  |  |
| Design Variation: Traffic Railing (Category 1 and 2 Structures) |  | X |  |  |
| Design Variation: Fencing on Traffic Railing between pedestrians and travel lanes on LA Facilities |  | X |  |  |
| Design Variation: Crossovers on Limited Access Facilities | X |  |  |  |
| Design Variation: Patterned Pavement Technical Special Provisions | X |  |  |  |
| Design Variation: Use of fencing around stormwater management facilities | X |  |  |  |

Table 122.7.1 Central Office Approvals (Cont.)

| Design Element | State <br> Roadway Design Engineer | State Structures Design Engineer | Chief Planner | Chief Engineer |
| :---: | :---: | :---: | :---: | :---: |
|  | Approval | Approval | Review | Approval |
| Design Loading Structural Capacity |  |  |  |  |
| -Design Exception for Bridges |  | X |  |  |
| -Design Variation: Category 2 Structures |  | X |  |  |
| -Design Variation: Deficient Load Ratings (Category 1 and 2 Structures) |  | X |  |  |
| Vertical Clearance Exception |  |  |  |  |
| - Non-Bridge Items | X |  |  |  |
| - Bridge Structures (Category 1 and 2) | X | X |  |  |
| -RR-South Fla Rail Corridor | X | X |  | X |
| Vertical Clearance Variation |  |  |  |  |
| -Category 2 Structures |  | X |  |  |
| -RR-South Fla Rail Corridor | X | X |  | X |
| Lateral Offset Variation |  |  |  |  |
| -Category 1 and 2 Structures | X |  |  |  |
| -RR-South Fla Rail Corridor | X | X |  | X |



| Worksheet 1B -- Crash Modification Factors for Urban and Suburban Roadway Segments |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for On-Street Parking | CMF for Roadside Fixed Objects | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF comb |
| from Equation 12-32 | from Equation 12-33 | from Table 12-22 | from Equation 12-34 | from Section 12.7.1 | $(1)^{*}(2)^{*}(3)^{*}(4)^{*}(5)$ |
| 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| Worksheet 1C -- Multiple-Vehicle Nondriveway Collisions by Severity Level for Urban and Suburban Roadway Segments |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) |  | (3) | (4) | (5) | (6) | (7) |  | (9) |
| Crash Severity Level | SPF Coefficients |  | Overdispersion Parameter, k | Initial $\mathrm{N}_{\text {brmv }}$ | Proportion of Total Crashes | $\begin{gathered} \hline \text { Adjusted } \\ \mathbf{N}_{\text {brmv }} \\ \hline \end{gathered}$ | Combined CMFs | Calibration Factor, $\mathbf{C r}$ | $\begin{gathered} \hline \text { Predicted } \\ \mathbf{N}_{\text {brmv }} \\ \hline \end{gathered}$ |
|  | from Table 12-3 |  | from Table 12-3 | from Equation 12-10 |  | (4) total $^{*}{ }^{\text {( }}$ ) | (6) from Worksheet 1B |  | (6)* 7$)^{*}$ (8) |
|  | a | b |  |  |  |  |  |  | (6) (7) ${ }^{\text {( }}$ ) |
| Total | -15.22 | 1.68 | 0.84 | 5.707 | 1.000 | 5.707 | 1.00 | 1.02 | 5.821 |
| Fatal and Injury (FI) | -16.22 | 1.66 | 0.65 | 1.712 | $\frac{(4)_{\mathrm{FI}} /\left((4)_{\mathrm{FI}}+(4)_{\mathrm{PDO}}\right)}{0.288}$ | 1.642 | 1.00 | 1.02 | 1.675 |
| Property Damage Only (PDO) | -15.62 | 1.69 | 0.87 | 4.237 | $\frac{(5)_{\text {TOTAL }}-(5)_{\mathrm{FI}}}{0.712}$ | 4.065 | 1.00 | 1.02 | 4.146 |


| (1) | (2) | (3) | (4) | (5) | (6) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Collision Type | Proportion of Collision Type(FI) | Predicted $\mathbf{N}$ brmv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted $\mathbf{N}$ brmv (PDO) (crashes/year) | Predicted $\mathbf{N}_{\text {brmv (total }}$ (crashes/year) |
|  | from Table 12-4 | (9)fl from Worksheet 1 C | from Table 12-4 | (9)poo from Worksheet 1C | (9)total from Worksheet 1C |
| Total | 1.000 | 1.675 | 1.000 | 4.146 | 5.821 |
|  |  | (2)* $(3)_{\text {F1 }}$ |  | (4)* ${ }^{*}()_{\text {PDo }}$ | (3)+(5) |
| Rear-end collision | 0.730 | 1.223 | 0.778 | 3.226 | 4.449 |
| Head-on collision | 0.068 | 0.114 | 0.004 | 0.017 | 0.131 |
| Angle collision | 0.085 | 0.142 | 0.079 | 0.328 | 0.470 |
| Sideswipe, same direction | 0.015 | 0.025 | 0.031 | 0.129 | 0.154 |
| Sideswipe, opposite direction | 0.073 | 0.122 | 0.055 | 0.228 | 0.350 |
| Other multiple-vehicle collision | 0.029 | 0.049 | 0.053 | 0.220 | 0.268 |


| (1) | (2) |  | (3) | (4) | (5) <br> Proportion of Total <br> Crashes | (6)Adjusted <br> $\mathbf{N}_{\text {brsv }}$ | $\begin{gathered} \hline(7) \\ \hline \begin{array}{c} \text { Combined } \\ \text { CMFs } \end{array} \\ \hline \end{gathered}$ |  | $(9)$ <br> Predicted <br> $\mathbf{N}_{\text {brsv }}$ <br> $(6)^{*}(8)(8)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SPF Coefficients |  | Overdispersion Parameter, $\mathbf{k}$ | Initial $\mathrm{N}_{\text {brsv }}$ |  |  |  |  |  |
| rash Severity Level | from | 12-5 | from Table 12-5 | from Equation 12-13 |  | (4) тотаL $^{*}{ }^{*}(5)$ | (6) from Worksheet 1B |  | $(6)^{*}(7)^{*}(8)$ |
| Total | -5.47 | 0.56 | 0.81 | 1.066 | 1.000 | 1.066 | 1.00 | 1.02 | 1.087 |
| Fatal and Injury (FI) | -3.96 | 0.23 | 0.50 | 0.166 | $\frac{(4)_{\mathrm{Fl}} /\left((4)_{\mathrm{F}+}(4)_{\mathrm{PDO}}\right)}{0.163}$ | 0.174 | 1.00 | 1.02 | 0.178 |
| Property Damage Only (PDO) | -6.51 | 0.64 | 0.87 | 0.852 | $\frac{(5)_{\text {TOTAL }}-(5)_{\text {FI }}}{0.837}$ | 0.892 | 1.00 | 1.02 | 0.909 |


| (1) | (2) | (3) | (4) | (5) | (6) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Proportion of Collision Type(f) | Predicted $\mathbf{N}_{\text {brsv ( }}$ (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted $\mathbf{N}$ brsv (PDO) (crashes/year) | Predicted $\mathrm{N}_{\text {brss (total) }}$ (crashes/year) |
|  | from Table 12-6 | (9)fl from Worksheet 1E | from Table 12-6 | (9)poo from Worksheet 1E | (9)total from Worksheet 1E |
| Total | 1.000 | 0.178 | 1.000 | 0.909 | 1.087 |
|  |  | (2)* ${ }^{*}$ ) ${ }_{\text {F1 }}$ |  | (4)** ${ }^{*}$ PDo | (3)+(5) |
| Collision with animal | 0.026 | 0.005 | 0.066 | 0.060 | 0.065 |
| Collision with fixed object | 0.723 | 0.128 | 0.759 | 0.690 | 0.819 |
| Collision with other object | 0.010 | 0.002 | 0.013 | 0.012 | 0.014 |
| Other single-vehicle collision | 0.241 | 0.043 | 0.162 | 0.147 | 0.190 |


| Driveway Type | Number of driveways, $\mathbf{n}_{\mathrm{j}}$ | Crashes per driveway per year, $\mathrm{N}_{\mathrm{j}}$ | Coefficient for traffic adjustment, t | Initial $\mathrm{N}_{\text {brdwy }}$ | Overdispersion parameter, k |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | from Table 12-7 | from Table 12-7 | Equation 12-16 | from Table 12-7 |
|  |  |  |  | $\mathrm{n}_{\mathrm{j}}{ }^{*} \mathrm{~N}_{\mathrm{j}}{ }^{*}(\text { AADT } / 15,000)^{\mathrm{t}}$ |  |
| Major commercial | 0 | 0.158 | 1.000 | 0.000 | -- |
| Minor commercial | 0 | 0.050 | 1.000 | 0.000 |  |
| Major industrial/institutional | 0 | 0.172 | 1.000 | 0.000 |  |
| Minor industrial/institutional | 0 | 0.023 | 1.000 | 0.000 |  |
| Major residential | 0 | 0.083 | 1.000 | 0.000 |  |
| Minor residential | 0 | 0.016 | 1.000 | 0.000 |  |
| Other | 2 | 0.025 | 1.000 | 0.090 |  |
| Total | -- | -- | -- | 0.090 | 0.81 |


| Worksheet 1H -- Multiple-Vehicle Driveway-Related Collisions by Severity Level for Urban and Suburban Roadway Segments |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Crash Severity | Initial $\mathrm{N}_{\text {brdwy }}$ | Proportion of total crashes ( $\mathrm{f}_{\mathrm{dwy}}$ ) | Adjusted $\mathrm{N}_{\text {brdwy }}$ | Combined CMFs | Calibration factor, $\mathrm{Cr}_{\mathrm{r}}$ | Predicted $\mathrm{N}_{\text {brdwy }}$ |
| Crash | (5) Total from Worksheet 1G | from Table 12-7 | (2) TOTAL ${ }^{\text {* }}$ (3) | (6) from Worksheet 1B |  | $(4)^{\star}(5)^{*}(6)$ |
| Total | 0.090 | 1.000 | 0.090 | 1.00 | 1.02 | 0.092 |
| Fatal and injury (FI) | -- | 0.323 | 0.029 | 1.00 | 1.02 | 0.030 |
| Property damage only (PDO) | -- | 0.677 | 0.061 | 1.00 | 1.02 | 0.062 |


| Worksheet 1I-- Vehicle-Pedestrian Collisions for Urban and Suburban Roadway Segments |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
| Crash Severity Level | Predicted $\mathrm{N}_{\text {brmv }}$ | Predicted $\mathrm{N}_{\text {brsv }}$ | Predicted $\mathrm{N}_{\text {brdwy }}$ | Predicted $\mathrm{N}_{\mathrm{br}}$ | $\mathrm{f}_{\text {pedr }}$ | Calibration factor, $\mathrm{C}_{\mathrm{r}}$ | Predicted $\mathrm{N}_{\text {pedr }}$ |
|  | (9) from Worksheet 1C | (9) from Worksheet 1E | (7) from Worksheet 1H | $(2)+(3)+(4)$ | $\begin{gathered} \text { from Table } \\ 12-8 \end{gathered}$ |  | $(5)^{*}(6)^{\star}(7)$ |
| Total | 5.821 | 1.087 | 0.092 | 7.000 | 0.005 | 1.02 | 0.035 |
| Fatal and injury (FI) | -- | -- | -- | -- | -- | 1.02 | 0.035 |


| Worksheet 1J -- Vehicle-Bicycle Collisions for Urban and Suburban Roadway Segments |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Crash Severity Level | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|  | Predicted $\mathrm{N}_{\text {brmv }}$ | Predicted $\mathrm{N}_{\text {brsv }}$ | Predicted $\mathrm{N}_{\text {brdwy }}$ | Predicted $\mathrm{N}_{\text {br }}$ | $\mathrm{f}_{\text {biker }}$ | Calibration factor, $\mathrm{C}_{\mathrm{r}}$ | Predicted $\mathrm{N}_{\text {biker }}$ |
|  | (9) from Worksheet 1 C | (9) from Worksheet 1E | (7) from Worksheet 1H | (2)+(3)+(4) | $\begin{gathered} \hline \text { from Table } \\ 12-9 \\ \hline \end{gathered}$ |  | $(5)^{*}(6)^{*}(7)$ |
| Total | 5.821 | 1.087 | 0.092 | 7.000 | 0.004 | 1.02 | 0.028 |
| Fatal and injury (FI) | -- | -- | -- | -- | -- | 1.02 | 0.028 |


| Worksheet 1K -- Crash Severity Distribution for Urban and Suburban Roadway Segments |  |  |  |
| :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) |
|  | Fatal and injury (FI) | Property damage only (PDO) | Total |
| Collision type | (3) from Worksheet 1D and 1F; <br> (7) from Worksheet 1H; and <br> (8) from Worksheet 1 I and 1 J | (5) from Worksheet 1D and 1F; and (7) from Worksheet 1H | (6) from Worksheet 1D and 1F; <br> (7) from Worksheet 1H; and <br> (8) from Worksheet 1 I and 1 J |
| MULTIPLE-VEHICLE |  |  |  |
| Rear-end collisions (from Worksheet 1D) | 1.223 | 3.226 | 4.449 |
| Head-on collisions (from Worksheet 1D) | 0.114 | 0.017 | 0.131 |
| Angle collisions (from Worksheet 1D) | 0.142 | 0.328 | 0.470 |
| Sideswipe, same direction (from Worksheet 1D) | 0.025 | 0.129 | 0.154 |
| Sideswipe, opposite direction (from Worksheet 1D) | 0.122 | 0.228 | 0.350 |
| Driveway-related collisions (from Worksheet 1H) | 0.030 | 0.062 | 0.092 |
| Other multiple-vehicle collision (from Worksheet 1D) | 0.049 | 0.220 | 0.268 |
| Subtotal | 1.705 | 4.208 | 5.913 |
| SINGLE-VEHICLE |  |  |  |
| Collision with animal (from Worksheet 1F) | 0.005 | 0.060 | 0.065 |
| Collision with fixed object (from Worksheet 1F) | 0.128 | 0.690 | 0.819 |
| Collision with other object (from Worksheet 1F) | 0.002 | 0.012 | 0.014 |
| Other single-vehicle collision (from Worksheet 1F) | 0.043 | 0.147 | 0.190 |
| Collision with pedestrian (from Worksheet 11) | 0.035 | 0.000 | 0.035 |
| Collision with bicycle (from Worksheet 1J) | 0.028 | 0.000 | 0.028 |
| Subtotal | 0.241 | 0.909 | 1.150 |
| Total | 1.946 | 5.118 | 7.063 |


| Worksheet 1L -- Summary Results for Urban and Suburban Roadway Segments |  |  |  |
| :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) |
| Crash Severity Level | Predicted average crash frequency, $\mathrm{N}_{\text {predicted rs }}$ (crashes/year) | Roadway segment length, L (mi) | Crash rate (crashes/mi/year) |
|  | (Total) from Worksheet 1K |  | (2) / (3) |
| Total | 7.1 | 0.84 | 8.5 |
| Fatal and injury (FI) | 1.9 | 0.84 | 2.3 |
| Property damage only (PDO) | 5.1 | 0.84 | 6.1 |

Urban/Suburban Arterial - 2 Lane Undivided


> NOTES:
> 1. Present Value $=$ Future Cash Flow $/(1+\text { Required Rate of Return })^{\text {Number of Years You Have To Wat For The Cash Flow }}$
> 2. Traffic Growth Rate $=\left[\left(\left(A D T_{f} / A D T_{i}\right)^{(1 /(-1))}\right)-1\right] \times 100$
> where $A D T_{f}=$ Average Daily Traffic for Future Year

> $$
> \begin{array}{l}A D T_{i}=\text { Average Daily Traffic for Initial Year } \\ \text { I } \\ \text { F Initial Year for ADT } \\ \text { F }\end{array}
>
$$

3. Column E(Site Specific (Npredicted / expected)) is updated based on manually updating AADT within the copy of the spreadsheet and get copy the crash rate for each year here

| Worksheet 2A -- General Information and Input Data for Urban and Suburban Arterial Intersections |  |  |
| :---: | :---: | :---: |
| General Information | Location Information |  |
| Analyst  <br> Agency or Company AECOM <br> Date Performed $10 / 27 / 22$ | Roadway Intersection Jurisdiction Analysis Year | SR 31 <br> Marina Dr and SR 31 <br> Lee County 2025 |
| Input Data | Base Conditions | Site Conditions |
| Intersection type (3ST, 3SG, 4ST, 4SG) | -- | 3ST |
|  | -- | 27,000 |
| $\mathrm{AADT}_{\text {minor }}$ (veh/day) $\mathrm{AADT}_{\text {MAX }}=\quad 9,300$ (veh/day) | -- | 1,900 |
| Intersection lighting (present/not present) | Not Present | Not Present |
| Calibration factor, $\mathrm{C}_{\mathrm{i}}$ | 1.00 | 1.14 |
| Data for unsignalized intersections only: | -- |  |
| Number of major-road approaches with left-turn lanes (0,1,2) | 0 | 1 |
| Number of major-road approaches with right-turn lanes (0,1,2) | 0 | 1 |
| Data for signalized intersections only: | -- |  |
| Number of approaches with left-turn lanes (0,1,2,3,4) [for 3SG, use maximum value of 3] | 0 | 0 |
| Number of approaches with right-turn lanes ( $0,1,2,3,4$ ) [for 3SG, use maximum value of 3] | 0 | 0 |
| Number of approaches with left-turn signal phasing [for 3SG, use maximum value of 3] | -- | 0 |
| Type of left-turn signal phasing for Leg \#1 | Permissive | Not Applicable |
| Type of left-turn signal phasing for Leg \#2 | -- | Not Applicable |
| Type of left-turn signal phasing for Leg \#3 | -- | Not Applicable |
| Type of left-turn signal phasing for Leg \#4 (if applicable) | -- | Not Applicable |
| Number of approaches with right-turn-on-red prohibited [for 3SG, use maximum value of 3] | 0 | 0 |
| Intersection red light cameras (present/not present) | Not Present | Not Present |
| Sum of all pedestrian crossing volumes (PedVol) -- Signalized intersections only |  |  |
| Maximum number of lanes crossed by a pedestrian ( $\mathrm{n}_{\text {lanesx }}$ ) | -- | 3 |
| Number of bus stops within $300 \mathrm{~m}(1,000 \mathrm{ft}$.) of the intersection | 0 | 0 |
| Schools within 300 m (1,000 ft.) of the intersection (present/not present) | Not Present | Not Present |
| Number of alcohol sales establishments within 300 m (1,000 ft.) of the intersection | 0 | 0 |


| Worksheet 2B -- Crash Modification Factors for Urban and Suburban Arterial Intersections |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| CMF for Left-Turn Lanes | CMF for Left-Turn Signal Phasing | CMF for Right-Turn Lanes | CMF for Right Turn on Red | CMF for Lighting | CMF for Red Light Cameras | Combined CMF |
| CMF 1i | CMF 2i | CMF 3i | CMF 4i | CMF $5 i$ | CMF 6i | CMF сомв |
| from Table 12-24 | from Table 12-25 | from Table 12-26 | from Equation 12-35 | from Equation 12-36 | from Equation 12-37 | $(1)^{*}(2)^{*}(3)^{*}(4)^{*}(5)^{*}(6)$ |
| 0.67 | 1.00 | 0.86 | 1.00 | 1.00 | 1.00 | 0.58 |


| Worksheet 2C -- Multiple-Vehicle Collisions by Severity Level for Urban and Suburban Arterial Intersections |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) |  |  | (3) | (4) | (5)Proportion of TotalCrashes | (6) | (7) | (8) | (9) |
| Crash Severity Level | SPF Coefficients |  |  | Overdispersion Parameter, $k$ | Initial $\mathrm{N}_{\text {bimv }}$ |  | $\begin{gathered} \text { Adjusted } \\ \mathbf{N}_{\text {bimv }} \end{gathered}$ | Combined CMFs | Calibration Factor, C | $\begin{gathered} \hline \text { Predicted } \\ \mathbf{N}_{\text {bimv }} \end{gathered}$ |
|  | from Table 12-10 |  |  | from Table 12-10 | $\begin{gathered} \text { from Equation 12- } \\ 21 \\ \hline \end{gathered}$ |  | (4) TOTAL $^{*}$ (5) | (7) from Worksheet 2B |  | (6)* 7 )* ${ }^{(8)}$ |
|  | a | b | c |  |  |  |  |  |  |  |
| Total | -13.36 | 1.11 | 0.41 | 0.80 | 2.890 | 1.000 | 2.890 | 0.58 | 1.14 | 1.898 |
| Fatal and Injury (FI) | -14.01 | 1.16 | 0.30 | 0.69 | 1.095 | (4) ${ }_{\text {FI }} /\left((4)_{\text {FIF }}+(4)_{\text {PDO }}\right)$ | 1.009 | 0.58 | 1.14 | 0.663 |
|  |  |  |  |  |  | 0.349 |  |  |  |  |
| Property Damage Only (PDO) | -15.38 | 1.20 | 0.51 | 0.77 | 2.043 | (5) TOTAL $^{-(5)_{\text {FI }}}$ | 1.882 | 0.58 | 1.14 | 1.236 |
|  |  |  |  |  |  | 0.651 |  |  |  |  |


| Worksheet 2D -- Multiple-Vehicle Collisions by Collision Type for Urban and Suburban Arterial Intersections |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) |
| Collision Type | Proportion of Collision Type(f) | Predicted $\mathbf{N}$ bimv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted $\mathbf{N}$ bimv (PDo) (crashes/year) | Predicted $\mathbf{N}_{\text {bimv (total }}$ (crashes/year) |
|  | from Table 12-11 | (9)FI from Worksheet 2C | from Table 12-11 | (9)ppo from Worksheet 2C | (9)pdo from Worksheet 2C |
| Total | 1.000 | 0.663 | 1.000 | 1.236 | 1.898 |
|  |  | (2)* 3$)_{\text {Fl }}$ |  | (4)* 5$)_{\text {PDO }}$ | (3)+(5) |
| Rear-end collision | 0.421 | 0.279 | 0.440 | 0.544 | 0.823 |
| Head-on collision | 0.045 | 0.030 | 0.023 | 0.028 | 0.058 |
| Angle collision | 0.343 | 0.227 | 0.262 | 0.324 | 0.551 |
| Sideswipe | 0.126 | 0.083 | 0.040 | 0.049 | 0.133 |
| Other multiple-vehicle collision | 0.065 | 0.043 | 0.235 | 0.290 | 0.334 |


| Worksheet 2E -- Single-Vehicle Collisions by Severity Level for Urban and Suburban Arterial Intersections |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) |  |  | (3) | (4) | $(5)$Proportion of TotalCrashes | $(6)$ <br> Adjusted <br> $\mathbf{N}_{\text {bimv }}$ <br> $(4)_{\text {TOTAL }}{ }^{*}(5)$ | (7) <br> Combined <br> CMFs <br> (7) from <br> Worksheet 2B | $\begin{array}{\|c\|} \hline(8) \\ \hline \text { Calibration } \\ \text { Factor, } \boldsymbol{C}_{\mathbf{i}} \\ \hline \end{array}$ | $\begin{gathered} \hline \text { (9) } \\ \hline \text { Predicted } \\ \mathbf{N}_{\text {bisv }} \end{gathered}$ |
| Crash Severity Level | SPF Coefficients |  |  | Overdispersion Parameter, $k$ | Initial $\mathrm{N}_{\text {bisv }}$ |  |  |  |  |  |
|  | from Table 12-12 |  |  | from Table 12-12 | from Eqn. 12-24; <br> (FI) from Eqn. 12- <br> 24 or 12-27 |  |  |  |  | $(6)^{*}(7)^{\star}(8)$ |
|  | a | b | c |  |  |  | (4) ${ }_{\text {total }}(5)$ |  |  |  |
| Total | -6.81 | 0.16 | 0.51 | 1.14 | 0.265 | 1.000 | 0.265 | 0.58 | 1.14 | 0.174 |
| Fatal and Injury (FI) | -- | -- | -- | -- | 0.082 | $\frac{(4)_{\mathrm{FI}} /\left((4)_{\mathrm{F} \cdot}+(4)_{\mathrm{PDO}}\right)}{0.301}$ | 0.080 | 0.58 | 1.14 | 0.052 |
| Property Damage Only (PDO) | -8.36 | 0.25 | 0.55 | 1.29 | 0.191 | $\begin{gathered} (5)_{\text {TOTAL }}-(5)_{\text {FI }} \\ 0.699 \end{gathered}$ | 0.185 | 0.58 | 1.14 | 0.122 |


| Worksheet 2F -- Single-Vehicle Collisions by Collision Type for Urban and Suburban Arterial Intersections |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) |
| Collision Type | Proportion of Collision Type(FI) | Predicted $\mathbf{N}$ bisv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted $\mathbf{N}$ bisv (PDo) (crashes/year) | Predicted $\mathbf{N}_{\text {bisv (total }}$ (crashes/year) |
|  | from Table 12-13 | (9)fl from Worksheet 2E | from Table 12-13 | (9)poo from Worksheet 2E | (9)poo from Worksheet 2E |
| Total | 1.000 | 0.052 | 1.000 | 0.122 | 0.174 |
|  |  | (2)* ${ }^{\text {(3) }}$ F1 |  | (4)**(5) ${ }_{\text {PDo }}$ | (3)+(5) |
| Collision with parked vehicle | 0.001 | 0.000 | 0.003 | 0.000 | 0.000 |
| Collision with animal | 0.003 | 0.000 | 0.018 | 0.002 | 0.002 |
| Collision with fixed object | 0.762 | 0.040 | 0.834 | 0.102 | 0.142 |
| Collision with other object | 0.090 | 0.005 | 0.092 | 0.011 | 0.016 |
| Other single-vehicle collision | 0.039 | 0.002 | 0.023 | 0.003 | 0.005 |
| Single-vehicle noncollision | 0.105 | 0.006 | 0.030 | 0.004 | 0.009 |


| Worksheet 2G -- Vehicle-Pedestrian Collisions for Urban and Suburban Arterial Stop-Controlled Intersections |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | Predicted $\mathrm{N}_{\text {bimv }}$ | Predicted $\mathrm{N}_{\text {bisv }}$ | Predicted $\mathrm{N}_{\mathrm{bi}}$ | $\mathrm{f}_{\text {pedi }}$ | Calibration factor, $\mathrm{C}_{\mathbf{i}}$ | Predicted $\mathrm{N}_{\text {pedi }}$ |
|  | (9) from Worksheet 2 C | (9) from Worksheet 2E | (2) + (3) | from Table 12-16 |  | $(4)^{*}(5)^{*}(6)$ |
| Total | 1.898 | 0.174 | 2.073 | 0.021 | 1.14 | 0.050 |
| Fatal and injury (FI) | -- | -- | -- | -- | 1.14 | 0.050 |


| (1) | (2) | (3) | (4) |
| :---: | :---: | :---: | :---: |
| CMF for Bus Stops | CMF for Schools | CMF for Alcohol Sales Establishments | Combined CMF |
| $\mathrm{CMF}_{1 \mathrm{p}}$ | $\mathrm{CMF}_{2 \mathrm{p}}$ | $\mathrm{CMF}_{3 \mathrm{p}}$ |  |
| from Table 12-28 | from Table 12-29 | from Table 12-30 | $(1) *(2) *$ (3) |
| -- | -- | -- | -- |


| Worksheet 21-- Vehicle-Pedestrian Collisions for Urban and Suburban Arterial Signalized Intersections |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) |  |  |  |  | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients |  |  |  |  | Overdispersion Parameter, k | $\mathbf{N}_{\text {pedbase }}$ | Combined CMF | Calibration factor, $\mathrm{C}_{\mathrm{i}}$ | Predicted $\mathbf{N}_{\text {pedi }}$ |
|  | from Table 12-14 |  |  |  |  |  | from Equation 12-29 | (4) from Worksheet 2H |  | $(4)^{*}(5)^{*}(6)$ |
|  | a | b | c | d | e |  |  |  |  |  |
| Total | -- | -- | -- | -- | -- | -- | -- | -- | 1.14 | 1.140 |
| Fatal and Injury (FI) | -- | -- | -- | -- | -- | -- | -- | -- | 1.14 | 1.140 |


| Worksheet 2J -- Vehicle-Bicycle Collisions for Urban and Suburban Arterial Intersections |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | Predicted $\mathrm{N}_{\text {bimv }}$ | Predicted $\mathrm{N}_{\text {bisv }}$ | Predicted $\mathrm{N}_{\mathrm{bi}}$ | $\mathrm{f}_{\text {bikei }}$ | Calibration factor, $\mathrm{C}_{\mathrm{i}}$ | Predicted $\mathrm{N}_{\text {bikei }}$ |
|  | (9) from Worksheet 2C | (9) from Worksheet 2E | (2) $+(3)$ | from Table 12-17 |  | $(4)^{\star}(5){ }^{\star}(6)$ |
| Total | 1.898 | 0.174 | 2.073 | 0.016 | 1.14 | 0.033 |
| Fatal and injury (FI) | -- | -- | -- | -- | 1.14 | 0.033 |


| Worksheet 2K -- Crash Severity Distribution for Urban and Suburban Arterial Intersections |  |  |  |
| :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) |
|  | Fatal and injury (FI) | Property damage only (PDO) | Total |
| Collision type | (3) from Worksheet 2D and 2F; <br> (7) from 2G or 2 I and 2 J | (5) from Worksheet 2D and 2F | (6) from Worksheet 2D and 2F; <br> (7) from 2G or 2 I and 2 J |
| MULTIPLE-VEHICLE |  |  |  |
| Rear-end collisions (from Worksheet 2D) | 0.279 | 0.544 | 0.823 |
| Head-on collisions (from Worksheet 2D) | 0.030 | 0.028 | 0.058 |
| Angle collisions (from Worksheet 2D) | 0.227 | 0.324 | 0.551 |
| Sideswipe (from Worksheet 2D) | 0.083 | 0.049 | 0.133 |
| Other multiple-vehicle collision (from Worksheet 2D) | 0.043 | 0.290 | 0.334 |
| Subtotal | 0.663 | 1.236 | 1.898 |
| SINGLE-VEHICLE |  |  |  |
| Collision with parked vehicle (from Worksheet 2F) | 0.000 | 0.000 | 0.000 |
| Collision with animal (from Worksheet 2F) | 0.000 | 0.002 | 0.002 |
| Collision with fixed object (from Worksheet 2F) | 0.040 | 0.102 | 0.142 |
| Collision with other object (from Worksheet 2F) | 0.005 | 0.011 | 0.016 |
| Other single-vehicle collision (from Worksheet 2F) | 0.002 | 0.003 | 0.005 |
| Single-vehicle noncollision (from Worksheet 2F) | 0.006 | 0.004 | 0.009 |
| Collision with pedestrian (from Worksheet 2G or 2I) | 0.050 | 0.000 | 0.050 |
| Collision with bicycle (from Worksheet 2J) | 0.033 | 0.000 | 0.033 |
| Subtotal | 0.135 | 0.122 | 0.257 |
| Total | 0.798 | 1.358 | 2.156 |


| Worksheet 2L -- Summary Results for Urban and Suburban Arterial Intersections |  |
| :--- | :---: |
| $(1)$ | $(2)$ |
| Crash severity level | Predicted average crash frequency, $\mathrm{N}_{\text {predicted int }}$ |
|  |  |

# Present Worth Analysis 

Urban/Suburban Arterial - Unsignalised 3 Leg Intersection
No-Build Alternative

| General Information |  |  |  |  | Site Information |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Analyst: |  | $\begin{array}{r} \text { Date: } \\ \text { AECOM } \end{array}$ | 10/27/2022 |  | Location ID: $\qquad$ City: | arina Dr and SR 31 | County: Lee County |  |  |
| Agency or Company: |  |  |  |  |  | Fort Mayers | M.P. - M.P. |  |  |
| Manual Input from Analysis |  |  |  |  |  |  |  |  |  |
| Major Growth Rate = | 3.9\% | Current Year = | 2025 roject Opening Year = | 2025 | Default Distribution for | rash Severity | 0-2014 Florida H | Crash Di | bution) |
| Minor Growth Rate = | 1.0\% | Rate of Return = | 4.0\% Analysis Period = | 21 | Fatality = | 0.9\% | Poss | Injury = | 22.4\% |
| Current Year Major AADT $=$ | 27,000 | Intersection Type $=$ | 3ST |  | Incapacitating = | 5.0\% | Property Da | Only = | 56.7\% |
| Current Year Minor AADT = | 1,900 | Intersection = Crash Data Used = | Intersection1 No | Analyze | Non-Incapacitating = | 15.0\% | Segment Type $=$ | 2 U | 100.0\% |


|  |  |  |  | Annual Number of Crashes |  |  |  |  |  | Annual Cost |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Year | AADT | AADT |  | Fatality | Incap. | Non-Inc. | Possible Injury | PDO | Fatality | Incap. | Non-Inc. | Possible Injury | PDO | Total Cost | Present Value |
| 1 | 2025 | 27,000 | 1,900 | 2.2 | 0.019 | 0.108 | 0.324 | 0.484 | 1.225 | \$211,732 | \$95,921 | \$58,387 | \$50,302 | \$9,432 | \$425,774 | \$409,398 |
| 2 | 2026 | 28,053 | 1,919 | 2.3 | 0.020 | 0.113 | 0.338 | 0.505 | 1.279 | \$221,159 | \$100,192 | \$60,986 | \$52,542 | \$9,852 | \$444,731 | \$411,178 |
| 3 | 2027 | 29,147 | 1,938 | 2.4 | 0.021 | 0.118 | 0.354 | 0.528 | 1.337 | \$231,028 | \$104,663 | \$63,708 | \$54,887 | \$10,291 | \$464,576 | \$413,006 |
| 4 | 2028 | 30,284 | 1,958 | 2.5 | 0.022 | 0.123 | 0.369 | 0.552 | 1.396 | \$241,359 | \$109,343 | \$66,557 | \$57,341 | \$10,751 | \$485,351 | \$414,880 |
| 5 | 2029 | 31,465 | 1,977 | 2.6 | 0.023 | 0.129 | 0.386 | 0.576 | 1.459 | \$252,175 | \$114,243 | \$69,539 | \$59,911 | \$11,233 | \$507,102 | \$416,801 |
| 6 | 2030 | 32,692 | 1,997 | 2.7 | 0.024 | 0.134 | 0.403 | 0.602 | 1.524 | \$263,499 | \$119,373 | \$72,662 | \$62,601 | \$11,738 | \$529,873 | \$418,766 |
| 7 | 2031 | 33,967 | 2,017 | 2.8 | 0.025 | 0.140 | 0.421 | 0.629 | 1.593 | \$275,355 | \$124,744 | \$75,931 | \$65,418 | \$12,266 | \$553,713 | \$420,776 |
| 8 | 2032 | 35,292 | 2,037 | 2.9 | 0.026 | 0.147 | 0.440 | 0.658 | 1.665 | \$287,767 | \$130,367 | \$79,354 | \$68,366 | \$12,819 | \$578,674 | \$422,831 |
| 9 | 2033 | 36,668 | 2,057 | 3.1 | 0.028 | 0.153 | 0.460 | 0.687 | 1.740 | \$300,763 | \$136,255 | \$82,938 | \$71,454 | \$13,398 | \$604,807 | \$424,930 |
| 10 | 2034 | 38,098 | 2,078 | 3.2 | 0.029 | 0.160 | 0.481 | 0.718 | 1.819 | \$314,370 | \$142,419 | \$86,690 | \$74,687 | \$14,004 | \$632,170 | \$427,071 |
| 11 | 2035 | 39,584 | 2,099 | 3.4 | 0.030 | 0.168 | 0.503 | 0.751 | 1.901 | \$328,618 | \$148,874 | \$90,619 | \$78,072 | \$14,638 | \$660,820 | \$429,256 |
| 12 | 2036 | 41,128 | 2,120 | 3.5 | 0.032 | 0.175 | 0.526 | 0.785 | 1.987 | \$343,536 | \$155,632 | \$94,733 | \$81,616 | \$15,303 | \$690,819 | \$431,483 |
| 13 | 2037 | 42,732 | 2,141 | 3.7 | 0.033 | 0.183 | 0.550 | 0.821 | 2.078 | \$359,156 | \$162,709 | \$99,040 | \$85,327 | \$15,999 | \$722,230 | \$433,753 |
| 14 | 2038 | 44,398 | 2,162 | 3.8 | 0.034 | 0.192 | 0.575 | 0.858 | 2.172 | \$375,512 | \$170,118 | \$103,550 | \$89,213 | \$16,727 | \$755,121 | \$436,064 |
| 15 | 2039 | 46,130 | 2,184 | 4.0 | 0.036 | 0.200 | 0.601 | 0.897 | 2.271 | \$392,639 | \$177,878 | \$108,273 | \$93,282 | \$17,490 | \$789,562 | \$438,416 |
| 16 | 2040 | 47,929 | 2,206 | 4.2 | 0.038 | 0.209 | 0.628 | 0.938 | 2.375 | \$410,574 | \$186,002 | \$113,219 | \$97,542 | \$18,289 | \$825,627 | \$440,809 |
| 17 | 2041 | 49,798 | 2,228 | 4.4 | 0.039 | 0.219 | 0.657 | 0.981 | 2.484 | \$429,354 | \$194,510 | \$118,398 | \$102,004 | \$19,126 | \$863,392 | \$443,243 |
| 18 | 2042 | 51,740 | 2,250 | 4.6 | 0.041 | 0.229 | 0.687 | 1.026 | 2.598 | \$449,021 | \$203,420 | \$123,821 | \$106,676 | \$20,002 | \$902,940 | \$445,716 |
| 19 | 2043 | 53,758 | 2,273 | 4.8 | 0.043 | 0.240 | 0.719 | 1.073 | 2.717 | \$469,615 | \$212,750 | \$129,500 | \$111,569 | \$20,919 | \$944,353 | \$448,230 |
| 20 | 2044 | 55,855 | 2,295 | 5.0 | 0.045 | 0.251 | 0.752 | 1.123 | 2.842 | \$491,182 | \$222,520 | \$135,447 | \$116,693 | \$21,880 | \$987,722 | \$450,783 |
| 21 | 2045 | 58,033 | 2,318 | 5.2 | 0.047 | 0.262 | 0.786 | 1.174 | 2.972 | \$513,767 | \$232,752 | \$141,675 | \$122,059 | \$22,886 | \$1,033,139 | \$453,376 |
|  | 2046 | 60,296 | 2,342 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2047 | 62,648 | 2,365 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2048 | 65,091 | 2,389 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2049 | 67,630 | 2,412 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2050 | 70,267 | 2,437 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2051 | 73,008 | 2,461 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |

NOTES:

1. Present Value $=$ Future Cash Flow $/(1+\text { Required Rate of Return })^{\text {Number of Years You Have To Watit For The Cash Flow }}$
2. Traffic Growth Rate $=\left[\left(\left(A D T_{f} / A D T_{i}\right)^{(1 /(F-1))}\right)-1\right] \times 100$
where $A D T_{f}=$ Average Daily Traffic for Future Year
$A D T_{i}=$ Average Daily Traffic for Initial Year
I = Initial Year for ADT
$I=$ Initial Year for ADT
F F Future Year for ADT
3. Column F(Site Specific (Npredicted / expected)) is updated based on manually updating AADT within the copy of the spreadsheet and get copy the crash rate for each year here

Worksheet 1A -- General Information and Input Data for Urban and Suburban Roadway Segments


| Worksheet 1B -- Crash Modification Factors for Urban and Suburban Roadway Segments |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for On-Street Parking | CMF for Roadside Fixed Objects | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF comb |
| from Equation 12-32 | from Equation 12-33 | from Table 12-22 | from Equation 12-34 | from Section 12.7.1 | $(1)^{*}(2)^{*}(3)^{*}(4)^{*}(5)$ |
| 1.00 | 1.00 | 0.99 | 0.91 | 1.00 | 0.90 |


| Worksheet 1C -- Multiple-Vehicle Nondriveway Collisions by Severity Level for Urban and Suburban Roadway Segments |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) |  | (3) | (4) | (5)Proportion of Total <br> Crashes | (6) | (7) | (8) | (9) <br> Predicted <br> $\mathbf{N}_{\text {brmv }}$ |
| Crash Severity Level | SPF Coefficients |  | Overdispersion Parameter, $\mathbf{k}$ | Initial $\mathrm{N}_{\text {brmv }}$ |  | $\begin{gathered} \hline \text { Adjusted } \\ \mathbf{N}_{\text {brmv }} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Combined } \\ \text { CMFs } \end{gathered}$ | Calibration Factor, Cr |  |
|  | from Table 12-3 |  | from Table 12-3 | from Equation 12-10 |  | (4) TOTAL $^{*}$ (5) | (6) from Worksheet 1B |  | $(6)^{*}(7){ }^{*}(8)$ |
|  | a | b |  |  |  |  |  |  | (6) ${ }^{(7)}$ (8) |
| Total | -12.34 | 1.36 | 1.32 | 2.529 | 1.000 | 2.529 | 0.90 | 1.63 | 3.730 |
| Fatal and Injury (FI) | -12.76 | 1.28 | 1.31 | 0.753 | $\frac{(4)_{\mathrm{FI}} /\left((4)_{\mathrm{FI}}+(4)_{\mathrm{PDO}}\right)}{0.281}$ | 0.711 | 0.90 | 1.63 | 1.049 |
| Property Damage Only (PDO) | -12.81 | 1.38 | 1.34 | 1.926 | $\frac{(5)_{\text {TOTAL }}-(5)_{\text {FI }}}{0.719}$ | 1.818 | 0.90 | 1.63 | 2.681 |


| $\begin{gathered} \hline \frac{(1)}{\text { Collision Type }} \end{gathered}$ | (2) | (3) | (4) | (5) | (6) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Proportion of Collision Type(f) | Predicted $\mathbf{N}_{\text {brmv ( }}$ (F) (crashes/year) | Proportion of Collision Type (PDO) | Predicted $\mathbf{N}_{\text {brmu ( }}$ (PDO) (crashes/year) | Predicted $\mathbf{N}_{\text {brmv (total) }}$ (crashes/year) |
|  | from Table 12-4 | (9)FIf from Worksheet 1C | from Table 12-4 | (9)poo from Worksheet 1 C | (9)total from Worksheet 1C |
| Total | 1.000 | 1.049 | 1.000 | 2.681 | 3.730 |
|  |  | (2)* $\left.{ }^{*}\right)_{\text {F1 }}$ |  | (4)** 5$)_{\text {PDO }}$ | (3)+(5) |
| Rear-end collision | 0.832 | 0.872 | 0.662 | 1.775 | 2.647 |
| Head-on collision | 0.020 | 0.021 | 0.007 | 0.019 | 0.040 |
| Angle collision | 0.040 | 0.042 | 0.036 | 0.097 | 0.138 |
| Sideswipe, same direction | 0.050 | 0.052 | 0.223 | 0.598 | 0.650 |
| Sideswipe, opposite direction | 0.010 | 0.010 | 0.001 | 0.003 | 0.013 |
| Other multiple-vehicle collision | 0.048 | 0.050 | 0.071 | 0.190 | 0.241 |


| Worksheet 1E -- Single-Vehicle Collisions by Severity Level for Urban and Suburban Roadway Segments |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) |  | (3) | (4) | $(5)$Proportion of Total <br> Crashes | (6) <br> Adjusted <br> $\mathbf{N}_{\text {brsv }}$ | $(7)$ <br> Combined <br> CMFs <br> $(6)$ mra | (8) <br> Calibration <br> Factor, Cr | $\frac{(9)}{\text { Predicted }}$ |
| Crash Severity Level | SPF Coefficients |  | Overdispersion Parameter, $\mathbf{k}$ | Initial $\mathrm{N}_{\text {brsv }}$ |  |  |  |  |  |
| Crash Severity Level | from | 12-5 | from Table 12-5 | from Equation 12-13 |  | (4) total $^{*}$ (5) | (6) from Worksheet 1 B |  | $(6)^{*}(7)^{*}(8)$ |
| Total | -5.05 | 0.47 | 0.86 | 0.558 | 1.000 | 0.558 | 0.90 | 1.63 | 0.823 |
| Fatal and Injury (FI) | -8.71 | 0.66 | 0.28 | 0.094 | $\frac{\left.(4)_{\mathrm{F} /} /(4)_{\mathrm{F}}+(4)_{\mathrm{PDO}}\right)}{0.169}$ | 0.094 | 0.90 | 1.63 | 0.139 |
| Property Damage Only (PDO) | -5.04 | 0.45 | 1.06 | 0.463 | $\frac{(5)_{\text {TOTAL }}-(5)_{\text {FI }}}{0.831}$ | 0.464 | 0.90 | 1.63 | 0.684 |


| (1) | (2) | (3) | (4) | (5) | (6) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Proportion of Collision Type(F) | Predicted $\mathbf{N}$ brsv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted $\mathbf{N}$ brsv (PDO) (crashes/year) | Predicted $\mathrm{N}_{\text {brss (total }}$ ( crashes/year) |
|  | from Table 12-6 | (9) FI from Worksheet 1E | from Table 12-6 | (9)poo from Worksheet 1E | (9)total from Worksheet 1E |
| Total | 1.000 | 0.139 | 1.000 | 0.684 | 0.823 |
|  |  | (2)* $(3)_{\text {F1 }}$ |  | (4)* ${ }^{*}$ (5poo | (3)+(5) |
| Collision with animal | 0.001 | 0.000 | 0.063 | 0.043 | 0.043 |
| Collision with fixed object | 0.500 | 0.070 | 0.813 | 0.556 | 0.626 |
| Collision with other object | 0.028 | 0.004 | 0.016 | 0.011 | 0.015 |
| Other single-vehicle collision | 0.471 | 0.066 | 0.108 | 0.074 | 0.139 |


| (1) | (2) | (3) (4) |  | (5) | (6) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Number of driveways, $n_{j}$ | Crashes per driveway per year, $\mathrm{N}_{\mathrm{j}}$ | Coefficient for traffic adjustment, t | Initial $\mathrm{N}_{\text {brdwy }}$ | Overdispersion parameter, $k$ |
| Driveway Type |  | from Table 12-7 | from Table 12-7 | Equation 12-16 | from Table 12-7 |
|  |  |  |  | $\mathrm{n}_{\mathrm{j}}{ }^{*} \mathrm{~N}_{\mathrm{j}}{ }^{*}(\text { AADT } / 15,000)^{\text {t }}$ |  |
| Major commercial | 0 | 0.033 | 1.106 | 0.000 | -- |
| Minor commercial | 0 | 0.011 | 1.106 | 0.000 |  |
| Major industrial/institutional | 0 | 0.036 | 1.106 | 0.000 |  |
| Minor industrial/institutional | 0 | 0.005 | 1.106 | 0.000 |  |
| Major residential | 0 | 0.018 | 1.106 | 0.000 |  |
| Minor residential | 4 | 0.003 | 1.106 | 0.016 |  |
| Other | 0 | 0.005 | 1.106 | 0.000 |  |
| Total | -- | -- | -- | 0.016 | 1.39 |


| Worksheet 1H -- Multiple-Vehicle Driveway-Related Collisions by Severity Level for Urban and Suburban Roadway Segments |  |  |  |  | (6) | (7) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Initial $\mathrm{N}_{\text {brdwy }}$ | Proportion of total crashes ( $\mathrm{f}_{\mathrm{dwy}}$ ) | Adjusted $\mathrm{N}_{\text {brdwy }}$ | Combined CMFs | Calibration factor, $\mathrm{C}_{\mathrm{r}}$ | Predicted $\mathrm{N}_{\text {brdwy }}$ |
| Crash Severity Level | (5) Total from Worksheet 1 G | from Table 12-7 | (2) ${ }_{\text {total }}$ * (3) | (6) from Worksheet 1B |  | $(4)^{*}(5)^{\star}(6)$ |
| Total | 0.016 | 1.000 | 0.016 | 0.90 | 1.63 | 0.024 |
| Fatal and injury (FI) | -- | 0.284 | 0.005 | 0.90 | 1.63 | 0.007 |
| Property damage only (PDO) | -- | 0.716 | 0.012 | 0.90 | 1.63 | 0.017 |


| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Crash Severity Level | Predicted $\mathrm{N}_{\text {brmv }}$ | Predicted $\mathrm{N}_{\text {brsv }}$ | Predicted $\mathrm{N}_{\text {brdwy }}$ | Predicted $\mathrm{N}_{\mathrm{br}}$ | $\mathrm{f}_{\text {pear }}$ | Calibration factor, $\mathrm{C}_{\mathrm{r}}$ | Predicted $\mathrm{N}_{\text {pedr }}$ |
|  | (9) from Worksheet 1C | (9) from Worksheet 1E | (7) from Worksheet 1 1 H | (2)+(3)+(4) | $\begin{gathered} \text { from Table } \\ 12-8 \end{gathered}$ |  | $(5)^{*}(6)^{\star}(7)$ |
| Total | 3.730 | 0.823 | 0.024 | 4.577 | 0.019 | 1.63 | 0.087 |
| Fatal and injury (FI) | -- | -- | -- | -- | -- | 1.63 | 0.087 |


| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Predicted $\mathrm{N}_{\text {brmv }}$ | Predicted $\mathrm{N}_{\text {brsv }}$ | Predicted $\mathrm{N}_{\text {brdwy }}$ | Predicted $\mathrm{N}_{\text {br }}$ | $\mathrm{f}_{\text {biker }}$ |  | Predicted $\mathrm{N}_{\text {biker }}$ |
| Crash Severity Level | (9) from Worksheet 1C | (9) from Worksheet 1E | (7) from Worksheet 1 1 H | $(2)+(3)+(4)$ | $\begin{gathered} \text { from Table } \\ 12-9 \end{gathered}$ | factor, $\mathrm{C}_{\mathrm{r}}$ | $(5)^{*}(6)^{*}(7)$ |
| Total | 3.730 | 0.823 | 0.024 | 4.577 | 0.005 | 1.63 | 0.023 |
| Fatal and injury (FI) | -- | -- | -- | -- | -- | 1.63 | 0.023 |


| Worksheet 1K -- Crash Severity Distribution for Urban and Suburban Roadway Segments |  |  |  |
| :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) |
|  | Fatal and injury (FI) | Property damage only (PDO) | Total |
| Collision type | (3) from Worksheet 1D and 1F; <br> (7) from Worksheet 1H; and <br> (8) from Worksheet 1 I and 1 J | (5) from Worksheet 1D and 1F; and (7) from Worksheet 1H | (6) from Worksheet 1D and 1F; <br> (7) from Worksheet 1 H ; and <br> (8) from Worksheet 1 I and 1 J |
| MULTIPLE-VEHICLE |  |  |  |
| Rear-end collisions (from Worksheet 1D) | 0.872 | 1.775 | 2.647 |
| Head-on collisions (from Worksheet 1D) | 0.021 | 0.019 | 0.040 |
| Angle collisions (from Worksheet 1D) | 0.042 | 0.097 | 0.138 |
| Sideswipe, same direction (from Worksheet 1D) | 0.052 | 0.598 | 0.650 |
| Sideswipe, opposite direction (from Worksheet 1D) | 0.010 | 0.003 | 0.013 |
| Driveway-related collisions (from Worksheet 1H) | 0.007 | 0.017 | 0.024 |
| Other multiple-vehicle collision (from Worksheet 1D) | 0.050 | 0.190 | 0.241 |
| Subtotal | 1.055 | 2.698 | 3.754 |
| SINGLE-VEHICLE |  |  |  |
| Collision with animal (from Worksheet 1F) | 0.000 | 0.043 | 0.043 |
| Collision with fixed object (from Worksheet 1F) | 0.070 | 0.556 | 0.626 |
| Collision with other object (from Worksheet 1F) | 0.004 | 0.011 | 0.015 |
| Other single-vehicle collision (from Worksheet 1F) | 0.066 | 0.074 | 0.139 |
| Collision with pedestrian (from Worksheet 1I) | 0.087 | 0.000 | 0.087 |
| Collision with bicycle (from Worksheet 1 J ) | 0.023 | 0.000 | 0.023 |
| Subtotal | 0.249 | 0.684 | 0.933 |
| Total | 1.304 | 3.383 | 4.687 |


| Worksheet 1L -- Summary Results for Urban and Suburban Roadway Segments |  |  |  |
| :--- | :---: | :---: | :---: |
| $(1)$ |  |  |  |
| Crash Severity Level | $(2)$ | $(3)$ | $(4)$ |

Urban/Suburban Arterial - 4 Lane Divided
Build Alternative

| General Information |  |  |  |  |  | Site Information |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Analyst: |  | Date: | 10/27/2022 |  |  | Location ID: City | SR 31 LJ's Lounge Driveway to south of SR 78 |  | County:_ Lee County |  |
| Agency or Company: AECOM |  |  |  |  |  |  |  |  | M.P. - M.P. |  |
| Manual Input from Analysis |  |  |  |  |  |  |  |  |  |  |
| Growth Rate = | 3.6\% |  | Current Year = | 2025 | Project Opening Year = | 2025 | Default D | bution for | S Se | 014 Florida HSM Crash Dis | bution) |
| Current Year AADT $=$ | 19,700 | Rate of Return = | 4.0\% | Analysis Period = | 21 |  | Fatality $=$ | 0.8\% | Possible Injury = | 23.4\% |
| Segment Length $=$ | 0.835 | Segment Type $=$ | 4D |  | Analyze |  | acitating = | 4.6\% | Property Damage Only = | 57.1\% |
| Crash Data Used = | No | Segment $=$ | Segment1 |  |  | Non-In | acitating = | 14.2\% |  | 100.1\% |


|  | Year | AADT | Annual Number of Crashes |  |  |  |  |  | Annual Cost |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Site Specific ( $\mathrm{N}_{\text {predicted } / \text { expected }}$ ) | Fatality | Incap. | Non-Inc. | Possible Injury | PDO | Fatality | Incap. | Non-Inc. | Possible Injury | PDO | Total Cost | Present Value |
| 1 | 2025 | 19,700 | 4.7 | 0.037 | 0.216 | 0.666 | 1.097 | 2.676 | \$408,325 | \$191,458 | \$119,918 | \$114,006 | \$20,607 | \$854,315 | \$821,456 |
| 2 | 2026 | 20,411 | 4.9 | 0.039 | 0.225 | 0.694 | 1.144 | 2.793 | \$426,087 | \$199,786 | \$125,134 | \$118,965 | \$21,503 | \$891,476 | \$824,219 |
| 3 | 2027 | 21,148 | 5.1 | 0.041 | 0.235 | 0.725 | 1.194 | 2.915 | \$444,685 | \$208,507 | \$130,596 | \$124,158 | \$22,442 | \$930,387 | \$827,110 |
| 4 | 2028 | 21,911 | 5.3 | 0.043 | 0.245 | 0.757 | 1.247 | 3.042 | \$464,160 | \$217,638 | \$136,315 | \$129,595 | \$23,425 | \$971,133 | \$830,129 |
| 5 | 2029 | 22,702 | 5.6 | 0.044 | 0.256 | 0.790 | 1.301 | 3.176 | \$484,555 | \$227,201 | \$142,305 | \$135,290 | \$24,454 | \$1,013,804 | \$833,273 |
| 6 | 2030 | 23,522 | 5.8 | 0.046 | 0.267 | 0.825 | 1.359 | 3.316 | \$505,914 | \$237,216 | \$148,578 | \$141,253 | \$25,532 | \$1,058,493 | \$836,543 |
| 7 | 2031 | 24,371 | 6.1 | 0.049 | 0.279 | 0.861 | 1.419 | 3.462 | \$528,285 | \$247,706 | \$155,148 | \$147,500 | \$26,661 | \$1,105,299 | \$839,936 |
| 8 | 2032 | 25,251 | 6.3 | 0.051 | 0.291 | 0.899 | 1.482 | 3.616 | \$551,716 | \$258,692 | \$162,029 | \$154,042 | \$27,844 | \$1,154,323 | \$843,453 |
| 9 | 2033 | 26,163 | 6.6 | 0.053 | 0.304 | 0.939 | 1.548 | 3.777 | \$576,260 | \$270,201 | \$169,237 | \$160,894 | \$29,082 | \$1,205,675 | \$847,091 |
| 10 | 2034 | 27,107 | 6.9 | 0.055 | 0.318 | 0.981 | 1.617 | 3.945 | \$601,971 | \$282,256 | \$176,788 | \$168,073 | \$30,380 | \$1,259,467 | \$850,851 |
| 11 | 2035 | 28,086 | 7.2 | 0.058 | 0.332 | 1.025 | 1.689 | 4.122 | \$628,904 | \$294,885 | \$184,698 | \$175,593 | \$31,739 | \$1,315,819 | \$854,731 |
| 12 | 2036 | 29,099 | 7.5 | 0.060 | 0.347 | 1.071 | 1.765 | 4.307 | \$657,121 | \$308,115 | \$192,984 | \$183,471 | \$33,163 | \$1,374,855 | \$858,730 |
| 13 | 2037 | 30,150 | 7.9 | 0.063 | 0.363 | 1.119 | 1.844 | 4.501 | \$686,683 | \$321,976 | \$201,666 | \$191,725 | \$34,655 | \$1,436,706 | \$862,848 |
| 14 | 2038 | 31,238 | 8.2 | 0.066 | 0.379 | 1.170 | 1.928 | 4.704 | \$717,656 | \$336,499 | \$210,763 | \$200,373 | \$36,218 | \$1,501,509 | \$867,084 |
| 15 | 2039 | 32,366 | 8.6 | 0.069 | 0.396 | 1.223 | 2.015 | 4.916 | \$750,110 | \$351,716 | \$220,294 | \$209,434 | \$37,856 | \$1,569,409 | \$871,437 |
| 16 | 2040 | 33,534 | 9.0 | 0.072 | 0.414 | 1.278 | 2.106 | 5.139 | \$784,115 | \$367,661 | \$230,280 | \$218,929 | \$39,572 | \$1,640,557 | \$875,907 |
| 17 | 2041 | 34,745 | 9.4 | 0.075 | 0.433 | 1.336 | 2.202 | 5.373 | \$819,749 | \$384,369 | \$240,745 | \$228,878 | \$41,370 | \$1,715,111 | \$880,492 |
| 18 | 2042 | 35,999 | 9.8 | 0.079 | 0.453 | 1.397 | 2.302 | 5.618 | \$857,090 | \$401,878 | \$251,712 | \$239,303 | \$43,255 | \$1,793,238 | \$885,193 |
| 19 | 2043 | 37,299 | 10.3 | 0.082 | 0.473 | 1.461 | 2.407 | 5.874 | \$896,222 | \$420,226 | \$263,204 | \$250,229 | \$45,230 | \$1,875,112 | \$890,008 |
| 20 | 2044 | 38,645 | 10.8 | 0.086 | 0.495 | 1.528 | 2.517 | 6.143 | \$937,233 | \$439,456 | \$275,248 | \$261,680 | \$47,300 | \$1,960,917 | \$894,937 |
| 21 | 2045 | 40,041 | 11.3 | 0.090 | 0.518 | 1.598 | 2.633 | 6.425 | \$980,215 | \$459,609 | \$287,871 | \$273,680 | \$49,469 | \$2,050,844 | \$899,979 |
|  | 2046 | 41,486 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2047 | 42,984 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2048 | 44,535 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2049 | 46,143 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2050 | 47,809 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2051 | 49,535 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |

## NOTES:

1. Present Value $=$ Future Cash Flow $/(1+\text { Required Rate of Return })^{\text {Number of Years You Have To Wait For The Cash Flow }}$
2. Traffic Growth Rate $=\left[\left(\left(\mathrm{ADT}_{f} / A D T_{i}\right)^{(1 /(F-1)}\right)-1\right] \times 100$
where $A D T_{f}=$ Average Daily Traffic for Future Year
$A D T_{i}=$ Average Daily Traffic for Initial Year
I = Initial Year for ADT
F = Future Year for ADT
3. Column E (Site Specific (Npredicted / expected)) is updated based on manually updating AADT within the copy of the spreadsheet and get copy the crash rate for each year here

| Worksheet 2A -- General Information and Input Data for Urban and Suburban Arterial Intersections |  |  |
| :---: | :---: | :---: |
| General Information | Location Information |  |
| Analyst  <br> Agency or Company AECOM <br> Date Performed $10 / 27 / 22$ | Roadway Intersection Jurisdiction Analysis Year | SR 31 Marina Dr and SR 31 Lee County 2025 |
| Input Data | Base Conditions | Site Conditions |
| Intersection type (3ST, 3SG, 4ST, 4SG) | -- | 4SG |
| $\mathrm{AADT}_{\text {major }}$ (veh/day) ${ }^{\text {a }}$ ( $\mathrm{AADT}_{\text {MAX }}=667,700$ (veh/day) | -- | 19,700 |
| $\mathrm{AADT}_{\text {minor }}$ (veh/day) $\mathrm{AADT}_{\text {MAX }}=333,400$ (veh/day) | -- | 1,900 |
| Intersection lighting (present/not present) | Not Present | Present |
| Calibration factor, $\mathrm{C}_{\mathrm{i}}$ | 1.00 | 2.27 |
| Data for unsignalized intersections only: | -- |  |
| Number of major-road approaches with left-turn lanes (0,1,2) | 0 | 0 |
| Number of major-road approaches with right-turn lanes (0,1,2) | 0 | 0 |
| Data for signalized intersections only: | -- |  |
| Number of approaches with left-turn lanes (0,1,2,3,4) [for 3SG, use maximum value of 3] | 0 | 2 |
| Number of approaches with right-turn lanes ( $0,1,2,3,4$ ) [for 3SG, use maximum value of 3] | 0 | 0 |
| Number of approaches with left-turn signal phasing [for 3SG, use maximum value of 3] | -- | 2 |
| Type of left-turn signal phasing for Leg \#1 | Permissive | Protected |
| Type of left-turn signal phasing for Leg \#2 | -- | Protected |
| Type of left-turn signal phasing for Leg \#3 | -- | Protected / Permissive |
| Type of left-turn signal phasing for Leg \#4 (if applicable) | -- | Protected / Permissive |
| Number of approaches with right-turn-on-red prohibited [for 3SG, use maximum value of 3] | 0 | 0 |
| Intersection red light cameras (present/not present) | Not Present | Not Present |
| Sum of all pedestrian crossing volumes (PedVol) -- Signalized intersections only |  | 10 |
| Maximum number of lanes crossed by a pedestrian ( $\mathrm{l}_{\text {lanesx }}$ ) | -- | 7 |
| Number of bus stops within 300 m ( $1,000 \mathrm{ft}$.) of the intersection | 0 | 0 |
| Schools within 300 m (1,000 ft.) of the intersection (present/not present) | Not Present | Not Present |
| Number of alcohol sales establishments within 300 m (1,000 ft.) of the intersection | 0 | 0 |


| Worksheet 2B -- Crash Modification Factors for Urban and Suburban Arterial Intersections |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| CMF for Left-Turn Lanes | CMF for Left-Turn Signal Phasing | CMF for Right-Turn Lanes | CMF for Right Turn on Red | CMF for Lighting | CMF for Red Light Cameras | Combined CMF |
| CMF 1i | CMF 2i | CMF 3i | CMF 4i | CMF 5i | CMF 6i | CMF сомв |
| from Table 12-24 | from Table 12-25 | from Table 12-26 | from Equation 12-35 | from Equation 12-36 | from Equation 12-37 | $(1)^{*}(2)^{*}(3)^{*}(4)^{*}(5)^{*}(6)$ |
| 0.81 | 0.87 | 1.00 | 1.00 | 0.91 | 1.00 | 0.65 |


| Worksheet 2C -- Multiple-Vehicle Collisions by Severity Level for Urban and Suburban Arterial Intersections |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) |  |  | (3) | (4) | (5)Proportion of TotalCrashes | (6) | (7) | (8) | (9) |
| Crash Severity Level | SPF Coefficients |  |  | Overdispersion Parameter, k |  |  | $\begin{gathered} \hline \text { Adjusted } \\ \mathbf{N}_{\text {bimv }} \end{gathered}$ | $\begin{gathered} \text { Combined } \\ \text { CMFs } \end{gathered}$ | Calibration Factor, $\mathrm{C}_{\mathrm{i}}$ | $\begin{gathered} \hline \text { Predicted } \\ \mathbf{N}_{\text {bimv }} \\ \hline \end{gathered}$ |
|  | from Table 12-10 |  |  | from Table 12-10 | from Equation 1221 |  | (4) TOTAL ${ }^{*}$ (5) | (7) from |  | $(6)^{*}(7)^{*}(8)$ |
|  | a | b | c |  |  |  | (4) Total ${ }^{\text {( }}$ ) | Worksheet 2B |  | (6) ${ }^{(7)}$ (8) |
| Total | -10.99 | 1.07 | 0.23 | 0.39 | 3.770 | 1.000 | 3.770 | 0.65 | 2.27 | 5.522 |
| Fatal and Injury (FI) | -13.14 | 1.18 | 0.22 | 0.33 | 1.208 | $\frac{(4)_{\text {Fl }} /\left((4)_{\text {FI }}+(4)_{\text {PDO }}\right)}{0.334}$ | 1.260 | 0.65 | 2.27 | 1.846 |
| Property Damage Only (PDO) | -11.02 | 1.02 | 0.24 | 0.44 | 2.406 | $\frac{(5)_{\text {TOTAL }}-(5)_{\text {FI }}}{0.666}$ | 2.509 | 0.65 | 2.27 | 3.676 |


| Worksheet 2D -- Multiple-Vehicle Collisions by Collision Type for Urban and Suburban Arterial Intersections |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) |
| Collision Type | Proportion of Collision Type(FI) | Predicted $\mathbf{N}$ bimv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted $\mathbf{N}$ bimv (PDo) (crashes/year) | Predicted $\mathbf{N}_{\text {bimv (total) }}$ (crashes/year) |
|  | from Table 12-11 | (9)Fl from Worksheet 2C | from Table 12-11 | (9)pDo from Worksheet 2C | (9)pdo from Worksheet 2C |
| Total | 1.000 | 1.846 | 1.000 | 3.676 | 5.522 |
|  |  | $(2) *$ (3) ${ }_{\text {FI }}$ |  | (4)* 5$)_{\text {PDO }}$ | (3)+(5) |
| Rear-end collision | 0.450 | 0.831 | 0.483 | 1.775 | 2.606 |
| Head-on collision | 0.049 | 0.090 | 0.030 | 0.110 | 0.201 |
| Angle collision | 0.347 | 0.641 | 0.244 | 0.897 | 1.537 |
| Sideswipe | 0.099 | 0.183 | 0.032 | 0.118 | 0.300 |
| Other multiple-vehicle collision | 0.055 | 0.102 | 0.211 | 0.776 | 0.877 |


| Worksheet 2E -- Single-Vehicle Collisions by Severity Level for Urban and Suburban Arterial Intersections |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) |  |  | (3) | (4) | (5) | (6) | (7) | (8)CalibrationFactor, $\mathrm{C}_{\mathrm{i}}$ | (9) |
| Crash Severity Level | SPF Coefficients |  |  | Overdispersion Parameter, k | Initial $\mathbf{N}_{\text {bisv }}$ | Proportion of Total Crashes | $\begin{gathered} \hline \text { Adjusted } \\ \mathbf{N}_{\text {bimv }} \end{gathered}$ | $\begin{gathered} \text { Combined } \\ \text { CMFs } \end{gathered}$ |  | $\begin{gathered} \text { Predicted } \\ \mathbf{N}_{\text {bisv }} \end{gathered}$ |
|  | from Table 12-12 |  |  | from Table 12-12 | from Eqn. 12-24; (FI) from Eqn. 1224 or 12-27 |  | (4) TOTAL ${ }^{*}(5)$ | (7) from Worksheet 2B |  | $(6)^{*}(7)^{*}(8)$ |
|  | a | b | c |  |  |  |  |  |  |  |
| Total | -10.21 | 0.68 | 0.27 | 0.36 | 0.235 | 1.000 | 0.235 | 0.65 | 2.27 | 0.344 |
| Fatal and Injury (FI) | -9.25 | 0.43 | 0.29 | 0.09 | 0.060 | $\frac{(4)_{\mathrm{FI}} /\left((4)_{\mathrm{FI}}+(4)_{\mathrm{PDO}}\right)}{0.256}$ | 0.060 | 0.65 | 2.27 | 0.088 |
| Property Damage Only (PDO) | -11.34 | 0.78 | 0.25 | 0.44 | 0.176 | $\frac{(5)_{\text {TOTAL }}-(5)_{\mathrm{FI}}}{0.744}$ | 0.175 | 0.65 | 2.27 | 0.256 |


| Worksheet 2F -- Single-Vehicle Collisions by Collision Type for Urban and Suburban Arterial Intersections |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) |
| Collision Type | Proportion of Collision Type(FI) | Predicted $\mathbf{N}$ bisv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted $\mathbf{N}$ bisv (PDo) (crashes/year) | Predicted $\mathbf{N}_{\text {bisv (total }}$ (crashes/year) |
|  | from Table 12-13 | (9)Fl from Worksheet 2E | from Table 12-13 | (9)pdo from Worksheet 2E | (9)pdo from Worksheet 2E |
| Total | 1.000 | 0.088 | 1.000 | 0.256 | 0.344 |
|  |  | (2)* ${ }^{*}(3)_{\text {Fl }}$ |  | (4)* ${ }^{*}$ ) ${ }_{\text {PDO }}$ | (3)+(5) |
| Collision with parked vehicle | 0.001 | 0.000 | 0.001 | 0.000 | 0.000 |
| Collision with animal | 0.002 | 0.000 | 0.002 | 0.001 | 0.001 |
| Collision with fixed object | 0.744 | 0.066 | 0.870 | 0.223 | 0.289 |
| Collision with other object | 0.072 | 0.006 | 0.070 | 0.018 | 0.024 |
| Other single-vehicle collision | 0.040 | 0.004 | 0.023 | 0.006 | 0.009 |
| Single-vehicle noncollision | 0.141 | 0.012 | 0.034 | 0.009 | 0.021 |


| Worksheet 2G -- Vehicle-Pedestrian Collisions for Urban and Suburban Arterial Stop-Controlled Intersections |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | Predicted $\mathrm{N}_{\text {bimv }}$ | Predicted $\mathrm{N}_{\text {bisv }}$ | Predicted $\mathrm{N}_{\mathrm{bi}}$ | $\mathbf{f}_{\text {pedi }}$ | Calibration factor, $\mathrm{C}_{\mathrm{i}}$ | Predicted $\mathbf{N}_{\text {pedi }}$ |
|  | (9) from Worksheet 2C | (9) from Worksheet 2E | (2) + (3) | from Table 12-16 |  | $(4)^{\star}(5)^{\star}(6)$ |
| Total | -- | -- | -- | -- | 2.27 | -- |
| Fatal and injury (FI) | -- | -- | -- | -- | 2.27 | -- |


| (1) | (2) | (3) | (4) |
| :---: | :---: | :---: | :---: |
| CMF for Bus Stops | CMF for Schools | CMF for Alcohol Sales Establishments | Combined CMF |
| $\mathrm{CMF}_{1 \mathrm{p}}$ | $\mathrm{CMF}_{2 \mathrm{p}}$ | $\mathrm{CMF}_{3 \mathrm{p}}$ |  |
| from Table 12-28 | from Table 12-29 | from Table 12-30 | $(1)^{*}(2) *$ (3) |
| 1.00 | 1.00 | 1.00 | 1.00 |


| Worksheet 2I -- Vehicle-Pedestrian Collisions for Urban and Suburban Arterial Signalized Intersections |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) |  |  |  |  | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients |  |  |  |  | Overdispersion Parameter, k | $\mathbf{N}_{\text {pedbase }}$ | Combined CMF | Calibration factor, $\mathrm{C}_{\mathrm{i}}$ | Predicted $\mathbf{N}_{\text {pedi }}$ |
|  | from Table 12-14 |  |  |  |  |  | from Equation 12-29 | (4) from Worksheet 2H |  | $(4)^{*}(5)^{*}(6)$ |
|  | a | b | c | d | e |  |  |  |  |  |
| Total | -9.53 | 0.40 | 0.26 | 0.45 | 0.04 | 0.24 | 0.008 | 1.00 | 2.27 | 0.008 |
| Fatal and Injury (FI) | -- | -- | -- | -- | -- | -- | -- | -- | 2.27 | 0.008 |


| Worksheet 2J -- Vehicle-Bicycle Collisions for Urban and Suburban Arterial Intersections |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | Predicted $\mathrm{N}_{\text {bimv }}$ | Predicted $\mathrm{N}_{\text {bisv }}$ | Predicted $\mathrm{N}_{\mathrm{bi}}$ | $\mathrm{f}_{\text {bikei }}$ | Calibration factor, $\mathbf{C}_{\mathbf{i}}$ | Predicted $\mathrm{N}_{\text {bikei }}$ |
|  | (9) from Worksheet 2C | (9) from Worksheet 2E | (2) + (3) | from Table 12-17 |  | $(4)^{*}(5)^{\star}(6)$ |
| Total | 5.522 | 0.344 | 5.866 | 0.015 | 2.27 | 0.088 |
| Fatal and injury (FI) | -- | -- | -- | -- | 2.27 | 0.088 |


| Worksheet 2K -- Crash Severity Distribution for Urban and Suburban Arterial Intersections |  |  |  |
| :---: | :---: | :---: | :---: |
| (1) | (2) | (3) | (4) |
|  | Fatal and injury (FI) | Property damage only (PDO) | Total |
| Collision type | (3) from Worksheet 2D and 2F; (7) from 2 G or 2 I and 2 J | (5) from Worksheet 2D and 2F | (6) from Worksheet 2D and 2F; (7) from 2 G or 2 I and 2 J |
| MULTIPLE-VEHICLE |  |  |  |
| Rear-end collisions (from Worksheet 2D) | 0.831 | 1.775 | 2.606 |
| Head-on collisions (from Worksheet 2D) | 0.090 | 0.110 | 0.201 |
| Angle collisions (from Worksheet 2D) | 0.641 | 0.897 | 1.537 |
| Sideswipe (from Worksheet 2D) | 0.183 | 0.118 | 0.300 |
| Other multiple-vehicle collision (from Worksheet 2D) | 0.102 | 0.776 | 0.877 |
| Subtotal | 1.846 | 3.676 | 5.522 |
| SINGLE-VEHICLE |  |  |  |
| Collision with parked vehicle (from Worksheet 2F) | 0.000 | 0.000 | 0.000 |
| Collision with animal (from Worksheet 2F) | 0.000 | 0.001 | 0.001 |
| Collision with fixed object (from Worksheet 2F) | 0.066 | 0.223 | 0.289 |
| Collision with other object (from Worksheet 2F) | 0.006 | 0.018 | 0.024 |
| Other single-vehicle collision (from Worksheet 2F) | 0.004 | 0.006 | 0.009 |
| Single-vehicle noncollision (from Worksheet 2F) | 0.012 | 0.009 | 0.021 |
| Collision with pedestrian (from Worksheet 2G or 2I) | 0.008 | 0.000 | 0.008 |
| Collision with bicycle (from Worksheet 2J) | 0.088 | 0.000 | 0.088 |
| Subtotal | 0.184 | 0.256 | 0.440 |
| Total | 2.030 | 3.932 | 5.962 |


| (1) | (2) |
| :---: | :---: |
| Crash severity level | Predicted average crash frequency, $\mathbf{N}_{\text {predicted int }}$ (crashes/year) |
|  | (Total) from Worksheet 2K |
| Total | 6.0 |
| Fatal and injury (FI) | 2.0 |
| Property damage only (PDO) | 3.9 |

Urban/Suburban Arterial - Signalized 4 Leg Intersection


|  | Year | Major AADT | Minor AADT | Annual Number of Crashes |  |  |  |  |  | Annual Cost |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Fatality | Incap. | Non-Inc. | Possible Injury | PDO | Fatality | Incap. | Non-Inc. | Possible Injury | PDO | Total Cost | Present Value |
| 1 | 2025 | 19,700 | 1,900 | 6.0 | 0.048 | 0.274 | 0.847 | 1.395 | 3.404 | \$519,421 | \$243,550 | \$152,545 | \$145,025 | \$26,214 | \$1,086,754 | \$1,044,956 |
| 2 | 2026 | 20,409 | 1,919 | 6.2 | 0.050 | 0.285 | 0.881 | 1.451 | 3.541 | \$540,245 | \$253,313 | \$158,660 | \$150,839 | \$27,265 | \$1,130,321 | \$1,045,046 |
| 3 | 2027 | 21,144 | 1,938 | 6.4 | 0.052 | 0.297 | 0.916 | 1.509 | 3.683 | \$561,909 | \$263,471 | \$165,022 | \$156,888 | \$28,358 | \$1,175,649 | \$1,045,147 |
| 4 | 2028 | 21,905 | 1,958 | 6.7 | 0.054 | 0.309 | 0.953 | 1.570 | 3.831 | \$584,449 | \$274,040 | \$171,642 | \$163,181 | \$29,495 | \$1,222,807 | \$1,045,260 |
| 5 | 2029 | 22,694 | 1,977 | 7.0 | 0.056 | 0.321 | 0.991 | 1.633 | 3.984 | \$607,899 | \$285,036 | \$118,529 | \$169,728 | \$30,679 | \$1,271,871 | \$1,045,385 |
| 6 | 2030 | 23,511 | 1,997 | 7.3 | 0.058 | 0.334 | 1.031 | 1.698 | 4.144 | \$632,297 | \$296,475 | \$185,694 | \$176,540 | \$31,910 | \$1,322,917 | \$1,045,521 |
| 7 | 2031 | 24,357 | 2,017 | 7.5 | 0.060 | 0.347 | 1.072 | 1.766 | 4.311 | \$657,681 | \$308,378 | \$193,149 | \$183,628 | \$33,191 | \$1,376,027 | \$1,045,667 |
| 8 | 2032 | 25,234 | 2,037 | 7.9 | 0.063 | 0.361 | 1.115 | 1.837 | 4.484 | \$684,092 | \$320,761 | \$200,905 | \$191,002 | \$34,524 | \$1,431,284 | \$1,045,825 |
| 9 | 2033 | 26,142 | 2,057 | 8.2 | 0.065 | 0.376 | 1.160 | 1.911 | 4.664 | \$711,570 | \$333,645 | \$208,975 | \$198,674 | \$35,911 | \$1,488,775 | \$1,045,994 |
| 10 | 2034 | 27,083 | 2,078 | 8.5 | 0.068 | 0.391 | 1.206 | 1.988 | 4.851 | \$740,159 | \$347,051 | \$217,371 | \$206,656 | \$37,354 | \$1,548,591 | \$1,046,173 |
| 11 | 2035 | 28,058 | 2,099 | 8.8 | 0.071 | 0.407 | 1.255 | 2.068 | 5.046 | \$769,905 | \$360,998 | \$226,107 | \$214,961 | \$38,855 | \$1,610,827 | \$1,046,362 |
| 12 | 2036 | 29,069 | 2,120 | 9.2 | 0.074 | 0.423 | 1.305 | 2.151 | 5.249 | \$800,855 | \$375,510 | \$235,196 | \$223,602 | \$40,417 | \$1,675,580 | \$1,046,562 |
| 13 | 2037 | 30,115 | 2,141 | 9.6 | 0.076 | 0.440 | 1.358 | 2.238 | 5.460 | \$833,056 | \$390,609 | \$244,653 | \$232,593 | \$42,042 | \$1,742,953 | \$1,046,772 |
| 14 | 2038 | 31,199 | 2,162 | 9.9 | 0.080 | 0.458 | 1.412 | 2.328 | 5.680 | \$866,560 | \$406,318 | \$254,493 | \$241,948 | \$43,733 | \$1,813,052 | \$1,046,992 |
| 15 | 2039 | 32,322 | 2,184 | 10.3 | 0.083 | 0.476 | 1.469 | 2.421 | 5.908 | \$901,421 | \$422,664 | \$264,731 | \$251,681 | \$45,492 | \$1,885,989 | \$1,047,223 |
| 16 | 2040 | 33,486 | 2,206 | 10.8 | 0.086 | 0.495 | 1.528 | 2.519 | 6.146 | \$937,692 | \$439,671 | \$275,383 | \$261,808 | \$47,323 | \$1,961,877 | \$1,047,462 |
| 17 | 2041 | 34,691 | 2,228 | 11.2 | 0.090 | 0.515 | 1.590 | 2.620 | 6.393 | \$975,432 | \$457,367 | \$286,467 | \$272,345 | \$49,227 | \$2,040,838 | \$1,047,712 |
| 18 | 2042 | 35,940 | 2,250 | 11.6 | 0.093 | 0.536 | 1.654 | 2.725 | 6.651 | \$1,014,700 | \$475,779 | \$297,999 | \$283,309 | \$51,209 | \$2,122,997 | \$1,047,971 |
| 19 | 2043 | 37,234 | 2,273 | 12.1 | 0.097 | 0.557 | 1.720 | 2.835 | 6.918 | \$1,055,559 | \$494,937 | \$309,998 | \$294,717 | \$53,271 | \$2,208,482 | \$1,048,239 |
| 20 | 2044 | 38,575 | 2,295 | 12.6 | 0.101 | 0.580 | 1.790 | 2.949 | 7.197 | \$1,098,072 | \$514,871 | \$322,484 | \$306,587 | \$55,417 | \$2,297,430 | \$1,048,517 |
| 21 | 2045 | 39,963 | 2,318 | 13.1 | 0.105 | 0.603 | 1.862 | 3.068 | 7.487 | \$1,142,307 | \$535,612 | \$335,475 | \$318,937 | \$57,649 | \$2,389,981 | \$1,048,804 |
|  | 2046 | 41,402 | 2,342 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2047 | 42,892 | 2,365 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2048 | 44,437 | 2,389 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2049 | 46,036 | 2,412 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2050 | 47,694 | 2,437 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | 2051 | 49,411 | 2,461 |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 | \$0 |
|  | d cel | es the | T is ou | 190.9 |  |  |  |  |  |  |  |  |  |  | Present Valu | \$21,977,591 |

NOTES:

1. Present Value $=$ Future Cash Flow $/(1+\text { Required Rate of Return })^{\text {Number of Years You Have To Wait For The Cash Flow }}$
2. Traffic Growth Rate $=\left[\left(\left(A D T_{f} / A D T_{i}\right)^{(1 /(F-1)}\right)-1\right] \times 100$
where $\mathrm{ADT}_{\mathrm{f}}=$ Average Daily Traffic for Future Year
$A D T_{i}=$ Average Daily Traffic for Initial Year
I = Initial Year for ADT
3. Column F(Site Specific (Npredicted / expected)) is updated based on manually updating AADT within the copy of the spreadsheet and get copy the crash rate for each year here

# Appendix C 

Preliminary Synchro Analysis SR 31 at Marina and Restaurant Entrance







## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 s \quad+$ : Computation Not Defined $\quad$ : All major volume in platoon



Platoon blocked, \%


Mov Cap-2 Maneuver
Stage 1
Stage 2

| Approach | EB | WB | NB |
| :--- | ---: | ---: | :--- |
| HCM Control Delay, S\$ 313.3 | 49.2 |  | SB |
| HCM LOS | F | E | 3.4 |


| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | + | - | - | 161 | 98 | 40 | - |
| HCM Lane V/C Ratio | - | - | -1.517 | 0.172 | 0.842 | - | - |
| HCM Control Delay (s) | - | - | $-\$ 313.3$ | 49.2 | 247.5 | - | - |
| HCM Lane LOS | - | - | - | F | E | F | - |
| HCM 95th \%tile Q(veh) | - | - | - | 16.1 | 0.6 | 3.2 | - |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 s \quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 10.2 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | ＊ |  |  | H | 虾 |  | ${ }^{7}$ | 444 | 「 |
| Traffic Vol，veh／h | 44 | 0 | 59 | 20 | 0 | 28 | 56 | 77 | 967 | 20 | 20 | 1174 | 38 |
| Future Vol，veh／h | 44 | 0 | 59 | 20 | 0 | 28 | 56 | 77 | 967 | 20 | 20 | 1174 | 38 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free | Free |
| RT Channelized | － | － | None | － | － | None | － | － | － | None | － | － | None |
| Storage Length | － | － | 100 | － | － | － | － | 400 | － | － | 150 | － | 220 |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles，\％ | 6 | 2 | 6 | 2 | 2 | 2 | 2 | 6 | 6 | 2 | 2 | 6 | 6 |
| Mvmt Flow | 46 | 0 | 62 | 21 | 0 | 29 | 59 | 81 | 1018 | 21 | 21 | 1236 | 40 |



| Minor Lane／Major Mvmt | NBL | NBT | NBR EBLn1 | EBLn2W | VBLn1 | SBL | SBT | SBR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity（veh／h） | 323 | － | 38 | 363 | 89 | 375 | － |  | － |
| HCM Lane V／C Ratio | 0.433 | － | － 1.219 | 0.171 | 0.568 | 0.056 | － |  | － |
| HCM Control Delay（s） | 24.4 | － | \＄ 382.2 | 17 | 88.9 | 15.2 | － |  | － |
| HCM Lane LOS | C | － | F | C | F | C | － |  | － |
| HCM 95th \％tile Q（veh） | 2.1 | － | 4.7 | 0.6 | 2.6 | 0.2 | － |  | － |
| Notes |  |  |  |  |  |  |  |  |  |
| $\sim$ ：Volume exceeds capacity | \＄：D | ay exc | eds 300s | ＋：Comp | putation | Not D | fined | ＊：All | Ill major volume in platoon |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 23 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 | F＇ |  | $\leftrightarrow$ |  |  | \＃ | 种中 |  | ${ }^{7}$ | 來乐 | 「 |
| Traffic Vol，veh／h | 58 | 0 | 112 | 27 | 0 | 16 | 103 | 76 | 1204 | 27 | 27 | 989 | 83 |
| Future Vol，veh／h | 58 | 0 | 112 | 27 | 0 | 16 | 103 | 76 | 1204 | 27 | 27 | 989 | 83 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free | Free |
| RT Channelized | － | － | None | － | － | None | － | － | － | None | － | － | None |
| Storage Length | － | － | 100 | － | － | － | － | 400 | － | － | 150 | － | 220 |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles，\％ | 6 | 2 | 6 | 2 | 2 | 2 | 2 | 6 | 6 | 2 | 2 | 6 | 6 |
| Mvmt Flow | 61 | 0 | 118 | 28 | 0 | 17 | 108 | 80 | 1267 | 28 | 28 | 1041 | 87 |



| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay，s | 227 | $\$ 448.1$ | 2.9 | 0.5 |
| HCM LOS | F | F |  |  |


| Minor Lane／Major Mvmt | NBL | NBT | NBR EBLn1 EBLn2WBLn1 | SBL | SBT | SBR |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity（veh／h） | 383 | - | - | 34 | 420 | 34 | 281 | - | - |
| HCM Lane V／C Ratio | 0.492 | - | - | 1.796 | 0.281 | 1.331 | 0.101 | - | - |
| HCM Control Delay（s） | 23.1 | - | $-\$ 632.8$ | $16.9 \$ 448.1$ | 19.2 | - | - |  |  |
| HCM Lane LOS | C | - | - | F | C | F | C | - | - |
| HCM 95th \％tile Q（veh） | 2.6 | - | - | 6.8 | 1.1 | 4.9 | 0.3 | - | - |
| Notes |  |  |  |  |  |  |  |  |  |
| ～：Volume exceeds capacity | \＄：Delay exceeds 300s | $+:$ Computation Not Defined | ＊：All major volume in platoon |  |  |  |  |  |  |




| Approach | EB | WB | NB |
| :--- | :---: | ---: | :--- |
| HCM Control Delay, s | 162.4 | SB |  |

HCM LOS


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 79.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | ＊ |  |  | \＃ | 虾 |  | ${ }^{1}$ | 444 | 「 |
| Traffic Vol，veh／h | 68 | 0 | 132 | 32 | 0 | 16 | 122 | 89 | 2710 | 32 | 32 | 2183 | 98 |
| Future Vol，veh／h | 68 | 0 | 132 | 32 | 0 | 16 | 122 | 89 | 2710 | 32 | 32 | 2183 | 98 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free | Free |
| RT Channelized | － | － | None | － | － | None | － | － | － | None | － | － | None |
| Storage Length | － | － | 100 | － | － | － | － | 400 | － | － | 150 | － | 220 |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles，\％ | 5 | 2 | 5 | 2 | 2 | 2 | 2 | 5 | 5 | 2 | 2 | 5 | 5 |
| Mvmt Flow | 72 | 0 | 139 | 34 | 0 | 17 | 128 | 94 | 2853 | 34 | 34 | 2298 | 103 |



| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |

HCM LOS


# Appendix D Warrants Analysis SR 31 at Marina and Restaurant Entrance 



| Marina/Restaurant/Babcock Ranch Road at SR 31 Signal Warrant Volumes (Year 2025) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | EB | WB | NB | SB | Major St. <br> Approaches | Highest <br> Minor St. <br> Approach | Total Volume | Rank by <br> Minor <br> Approach |
| 12:00 AM | 1 | 2 | 55 | 75 | 131 | 2 | 133 | 22 |
| 1:00 AM | 1 | 1 | 41 | 51 | 92 | 1 | 93 | 24 |
| 2:00 AM | 1 | 1 | 26 | 54 | 80 | 1 | 82 | 23 |
| 3:00 AM | 2 | 1 | 51 | 71 | 122 | 2 | 125 | 21 |
| 4:00 AM | 3 | 3 | 81 | 103 | 184 | 3 | 190 | 20 |
| 5:00 AM | 1 | 9 | 306 | 221 | 527 | 9 | 537 | 19 |
| 6:00 AM | 6 | 10 | 745 | 702 | 1,447 | 10 | 1,463 | 18 |
| 7:00 AM | 8 | 18 | 990 | 829 | 1,818 | 18 | 1,844 | 15 |
| 8:00 AM | 9 | 16 | 817 | 937 | 1,754 | 16 | 1,779 | 17 |
| 9:00 AM | 19 | 12 | 838 | 703 | 1,541 | 19 | 1,572 | 14 |
| 10:00 AM | 21 | 14 | 806 | 680 | 1,486 | 21 | 1,522 | 13 |
| 11:00 AM | 31 | 16 | 880 | 698 | 1,578 | 31 | 1,625 | 12 |
| 12:00 PM | 49 | 27 | 926 | 810 | 1,736 | 49 | 1,812 | 10 |
| 1:00 PM | 64 | 38 | 985 | 871 | 1,856 | 64 | 1,957 | 7 |
| 2:00 PM | 63 | 37 | 978 | 874 | 1,852 | 63 | 1,952 | 8 |
| 3:00 PM | 80 | 43 | 1,104 | 1,030 | 2,134 | 80 | 2,257 | 4 |
| 4:00 PM | 103 | 48 | 1,120 | 1,232 | 2,352 | 103 | 2,503 | 2 |
| 5:00 PM | 170 | 43 | 1,410 | 1,099 | 2,509 | 170 | 2,722 | 1 |
| 6:00 PM | 81 | 27 | 956 | 823 | 1,779 | 81 | 1,887 | 3 |
| 7:00 PM | 80 | 22 | 686 | 598 | 1,285 | 80 | 1,387 | 5 |
| 8:00 PM | 75 | 17 | 498 | 498 | 996 | 75 | 1,088 | 6 |
| 9:00 PM | 55 | 12 | 352 | 369 | 721 | 55 | 788 | 9 |
| 10:00 PM | 35 | 8 | 209 | 240 | 450 | 35 | 492 | 11 |
| 11:00 PM | 17 | 4 | 101 | 122 | 223 | 17 | 244 | 16 |


| Marina/Restaurant/Babcock Ranch Road at SR 31 Signal Warrant Volumes (Year 2035) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | EB | WB | NB | SB | Major St. <br> Approaches | Highest Minor St. Approach | Total Volume | Rank by <br> Minor <br> Approach |
| 12:00 AM | 1 | 1 | 97 | 137 | 234 | 1 | 236 | 23 |
| 1:00 AM | 1 | 1 | 71 | 93 | 164 | 1 | 166 | 24 |
| 2:00 AM | 1 | 1 | 46 | 98 | 144 | 1 | 145 | 22 |
| 3:00 AM | 2 | 1 | 89 | 129 | 218 | 2 | 222 | 21 |
| 4:00 AM | 3 | 3 | 142 | 188 | 330 | 3 | 336 | 20 |
| 5:00 AM | 1 | 7 | 536 | 402 | 937 | 7 | 946 | 19 |
| 6:00 AM | 6 | 8 | 1,303 | 1,279 | 2,582 | 8 | 2,596 | 18 |
| 7:00 AM | 10 | 16 | 1,731 | 1,509 | 3,240 | 16 | 3,265 | 16 |
| 8:00 AM | 10 | 14 | 1,429 | 1,707 | 3,135 | 14 | 3,159 | 17 |
| 9:00 AM | 22 | 13 | 1,465 | 1,280 | 2,745 | 22 | 2,781 | 14 |
| 10:00 AM | 24 | 15 | 1,410 | 1,238 | 2,648 | 24 | 2,688 | 13 |
| 11:00 AM | 35 | 17 | 1,540 | 1,270 | 2,810 | 35 | 2,863 | 12 |
| 12:00 PM | 53 | 26 | 1,620 | 1,475 | 3,095 | 53 | 3,174 | 10 |
| 1:00 PM | 69 | 40 | 1,724 | 1,585 | 3,309 | 69 | 3,418 | 7 |
| 2:00 PM | 68 | 39 | 1,711 | 1,592 | 3,303 | 68 | 3,410 | 8 |
| 3:00 PM | 87 | 46 | 1,932 | 1,874 | 3,806 | 87 | 3,938 | 4 |
| 4:00 PM | 112 | 51 | 1,621 | 1,787 | 3,408 | 112 | 3,571 | 2 |
| 5:00 PM | 184 | 45 | 2,041 | 1,594 | 3,635 | 184 | 3,865 | 1 |
| 6:00 PM | 88 | 28 | 1,673 | 1,497 | 3,170 | 88 | 3,287 | 3 |
| 7:00 PM | 87 | 23 | 1,201 | 1,089 | 2,290 | 87 | 2,400 | 5 |
| 8:00 PM | 81 | 18 | 871 | 906 | 1,777 | 81 | 1,877 | 6 |
| 9:00 PM | 60 | 13 | 616 | 671 | 1,287 | 60 | 1,360 | 9 |
| 10:00 PM | 38 | 8 | 366 | 438 | 804 | 38 | 850 | 11 |
| 11:00 PM | 19 | 4 | 177 | 222 | 399 | 19 | 422 | 15 |


| Marina/Restaurant/Babcock Ranch Road at SR 31 Signal Warrant Volumes (Year 2045) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | EB | WB | NB | SB | Major St. <br> Approaches | Highest <br> Minor St. <br> Approach | Total Volume | Rank by Minor Approach |
| 12:00 AM | 2 | 2 | 106 | 160 | 266 | 2 | 270 | 21 |
| 1:00 AM | 1 | 2 | 78 | 108 | 186 | 2 | 189 | 23 |
| 2:00 AM | 1 | 1 | 50 | 114 | 164 | 1 | 166 | 24 |
| 3:00 AM | 1 | 2 | 98 | 150 | 248 | 2 | 252 | 22 |
| 4:00 AM | 2 | 3 | 156 | 219 | 375 | 3 | 380 | 20 |
| 5:00 AM | 1 | 4 | 588 | 468 | 1,055 | 4 | 1,061 | 19 |
| 6:00 AM | 4 | 6 | 1,429 | 1,489 | 2,918 | 6 | 2,928 | 18 |
| 7:00 AM | 6 | 12 | 1,899 | 1,757 | 3,656 | 12 | 3,674 | 16 |
| 8:00 AM | 8 | 11 | 1,567 | 1,987 | 3,554 | 11 | 3,574 | 17 |
| 9:00 AM | 15 | 17 | 1,607 | 1,491 | 3,098 | 17 | 3,131 | 14 |
| 10:00 AM | 17 | 16 | 1,547 | 1,441 | 2,989 | 17 | 3,022 | 15 |
| 11:00 AM | 32 | 28 | 1,689 | 1,479 | 3,169 | 32 | 3,228 | 12 |
| 12:00 PM | 76 | 31 | 1,777 | 1,717 | 3,494 | 76 | 3,601 | 8 |
| 1:00 PM | 99 | 41 | 1,891 | 1,812 | 3,703 | 99 | 3,844 | 5 |
| 2:00 PM | 87 | 43 | 1,877 | 1,820 | 3,697 | 87 | 3,828 | 6 |
| 3:00 PM | 108 | 48 | 2,119 | 2,143 | 4,262 | 108 | 4,418 | 3 |
| 4:00 PM | 136 | 59 | 2,432 | 2,790 | 5,222 | 136 | 5,417 | 2 |
| 5:00 PM | 200 | 48 | 2,953 | 2,313 | 5,266 | 200 | 5,514 | 1 |
| 6:00 PM | 102 | 32 | 1,835 | 1,744 | 3,579 | 102 | 3,713 | 4 |
| 7:00 PM | 80 | 23 | 1,317 | 1,268 | 2,586 | 80 | 2,689 | 7 |
| 8:00 PM | 66 | 18 | 956 | 1,055 | 2,011 | 66 | 2,095 | 9 |
| 9:00 PM | 65 | 13 | 676 | 782 | 1,457 | 65 | 1,536 | 10 |
| 10:00 PM | 41 | 8 | 402 | 510 | 911 | 41 | 961 | 11 |
| 11:00 PM | 21 | 4 | 194 | 259 | 453 | 21 | 477 | 13 |

## SIGNAL WARRANT ANALYSIS

## Introduction

- The Signal Warrant Analysis Spreadsheets are a tool for assisting traffic engineers when evaluating the need for a traffic signal installation
- The filled spreadsheets can be used as part of the supporting documents for the signal warrant evaluation

Note: This templates are a useful resource, but it remains necessary to apply engineering judgment and to consider specific environmental, traffic, geometric, and operational conditions

```
Instructions
Fill in "Orange" areas only
Automated cells based on in Input
Data in "orange" cells
General Information
Enter Eight Hour Volumes
Enter Four Hour Volumes
Enter Pedestrian Volumes (4-hr)
Enter Peak Hour Volumes
Fill in below the general information including:
District, County (drop-down menu)
City, Engineer, Date
Major and Minor Street with corresponding number of lanes and speed limits
Any 8 hours of an average day. Major-street and minor-street volumes shall be for the same 8 hours; however, the 8 hours satisfied in Condition A shall not be required to be the same 8 hours satisfied in Condition B for \(80 \%\) columns only. On the minor street, the higher volume shall not be required to be on the same approach during each of the 8 hours.
Any 4 hours of an average day. Vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor-street approach (one direction only, not required to be on the same approach during each of the 4 hours)
Pedestrians per hour crossing the major street (total of all crossings)
Enter Peak Hour Volumes
Vehicular: Any four consecutive 15-minute periods of an average day
Pedestrian: Any four consecutive 15-minute periods of an average day representing the vehicles per hour on the major street (total of both approaches) and the corresponding pedestrians per hour crossing the major street (total of all crossings)
```



## TRAFFIC SIGNAL WARRANT SUMMARY



Engineer: $\qquad$
Date:

| Lanes: $\quad \mathbf{6}$ |
| :--- |
| Lanes: $\quad \mathbf{2}$ |

Major Approach Speed:
Minor Approach Speed: $\qquad$ 45 30

## TRAFFIC SIGNAL WARRANT SUMMARY

## Condition B - Interruption of Continuous Traffic

Condition B is intended for application where Condition A is not satisfied and the traffic volume on a major street is so heavy that traffic on the minor intersecting street suffers excessive delay or conflict in entering or crossing the major street.

| Applicable: | $\square$ Yes | $\square$ No |
| ---: | :--- | :--- |
| 100\% Satisfied: | $\square$ Yes | $\square$ No |
| 80\% Satisfied: | $\square$ Yes | $\square$ No |
| 70\% Satisfied: | $\square$ Yes | $\square$ No |


| Number of traffic on | for moving approach | Vehicles per hour on majorstreet (total of both approaches) |  |  | Vehicles per hour on minorstreet (one direction only) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major | Minor | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ |
| 1 | 1 | 750 | 600 | 525 | 75 | 60 | 53 |
| 2 or more | 1 | 900 | 720 | 630 | 75 | 60 | 53 |
| 2 or more | 2 or more | 900 | 720 | 630 | 100 | 80 | 70 |
| 1 | 2 or more | 750 | 600 | 525 | 100 | 80 | 70 |

${ }^{\text {a }}$ Basic Minimum hourly volume
${ }^{\mathrm{b}}$ Used for combination of Conditions $A$ and $B$ after adequate trial of other remedial measures
${ }^{\text {c }}$ May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

Record 8 highest hours and the corresponding major-street and minor-street volumes in the Instructions Sheet.

| Eight Highest Hours |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Street |  | $\begin{aligned} & \sum_{0} \\ & 0 \\ & \stackrel{\rightharpoonup}{\dot{\theta}} \end{aligned}$ | $\sum_{0}$ <br> 0 <br> 0 <br> 0 | $\begin{aligned} & \sum_{0} \\ & \stackrel{\rightharpoonup}{\mathrm{O}} \end{aligned}$ |  | $\begin{aligned} & \Sigma \Sigma_{0} \\ & \text { ọi } \\ & \dot{\phi} \end{aligned}$ | $\begin{aligned} & \Sigma \\ & \\ & \hline \mathbf{O} \end{aligned}$ | $\begin{aligned} & \underset{0}{\boldsymbol{N}} \\ & \stackrel{\rightharpoonup}{\mathrm{~N}} \\ & \dot{\mathrm{~N}} \end{aligned}$ |
| Major | 2,509 | 2,352 | 1,779 | 2,134 | 1,285 | 996 | 1,856 | 1,852 |
| Minor | 170 | 103 | 81 | 80 | 80 | 75 | 64 | 63 |

## Existing Volumes



## SIGNAL WARRANT ANALYSIS

## Introduction

- The Signal Warrant Analysis Spreadsheets are a tool for assisting traffic engineers when evaluating the need for a traffic signal installation
- The filled spreadsheets can be used as part of the supporting documents for the signal warrant evaluation

Note: This templates are a useful resource, but it remains necessary to apply engineering judgment and to consider specific environmental, traffic, geometric, and operational conditions

```
Instructions
Fill in "Orange" areas only
Automated cells based on in Input
Data in "orange" cells
General Information
Enter Eight Hour Volumes
Enter Four Hour Volumes
Enter Pedestrian Volumes (4-hr)
Enter Peak Hour Volumes
Fill in below the general information including:
District, County (drop-down menu)
City, Engineer, Date
Major and Minor Street with corresponding number of lanes and speed limits
Any 8 hours of an average day. Major-street and minor-street volumes shall be for the same 8 hours; however, the 8 hours satisfied in Condition A shall not be required to be the same 8 hours satisfied in Condition B for \(80 \%\) columns only. On the minor street, the higher volume shall not be required to be on the same approach during each of the 8 hours.
Any 4 hours of an average day. Vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor-street approach (one direction only, not required to be on the same approach during each of the 4 hours)
Pedestrians per hour crossing the major street (total of all crossings)
Enter Peak Hour Volumes
Vehicular: Any four consecutive 15-minute periods of an average day
Pedestrian: Any four consecutive 15-minute periods of an average day representing the vehicles per hour on the major street (total of both approaches) and the corresponding pedestrians per hour crossing the major street (total of all crossings)
```

| Input Data |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Engineer: |  | Major Approach Speed: Minor Approach Speed: |  |  | Form 750-020-01 TRAFFIC ENGINEERING 10/15 |
|  | 12 - Lee |  | AECOM |  |  |  |  |
|  | One | Date: | March 8th, 2023 |  |  |  |  |
| Major Street: Minor Street: | SR 31 | \# Lanes: | 6 |  | 45 |  |  |
|  | Restaurant | \# Lanes: | 2 |  | 30 |  |  |
|  | Eight Hour Volumes (Condition A) |  |  |  | Eight Hour Volumes (Condition B) |  |  |
|  | Hours | Major Street <br> (total of both approaches) | Minor Street (one direction only) |  | Hours | Major Street <br> (total of both approaches) | Minor Street (one direction only) |
|  | 5:00 PM | 3635 | 184 |  | 5:00 PM | 3635 | 184 |
|  | 4:00 PM | 3408 | 112 |  | 4:00 PM | 3408 | 112 |
|  | 6:00 PM | 3170 | 88 |  | 6:00 PM | 3170 | 88 |
|  | 3:00 PM | 3806 | 87 |  | 3:00 PM | 3806 | 87 |
|  | 7:00 PM | 2290 | 87 |  | 7:00 PM | 2290 | 87 |
|  | 8:00 PM | 1777 | 81 |  | 8:00 PM | 1777 | 81 |
|  | 7:00 PM | 3309 | 69 |  | 7:00 PM | 3309 | 69 |
|  | 2:00 PM | 3303 | 68 |  | 2:00 PM | 3303 | 68 |
|  | Highest Four Hour Vehicular Volumes |  |  |  | Highest Four Hour Pedestrian Volumes |  |  |
|  | Hours | Major Street <br> (total of both approaches) | Minor Street (one direction only) |  | Hours | Major Street <br> (total of both approaches) | Pedestrian Crossings on Major Street |
|  | 5:00 PM | 3635 | 184 |  |  |  |  |
|  | 4:00 PM | 3408 | 112 |  |  |  |  |
|  | 6:00 PM | 3170 | 88 |  |  |  |  |
|  | 3:00 PM | 3806 | 87 |  |  |  |  |
|  | Vehicular Peak Hour Volumes |  |  |  |  |  |  |
|  | Peak Hour | Major Street (total of both approaches) | Minor Street (one direction only) | Total Entering Volume |  |  |  |
|  | 5:00 PM | 3635 | 184 | 3865 |  |  |  |
|  | Pedestrian Peak Hour Volumes |  |  |  |  |  |  |
|  | Peak Hour | Major Street (total of both approaches) | Pedestrian Crossing Volumes on Major Street |  |  |  |  |
|  |  |  |  |  |  |  |  |

# State of Florida Department of Transportation 

# TRAFFIC SIGNAL WARRANT SUMMARY 



Major Street: $\qquad$

Engineer: $\qquad$
Date: March 8th, 2023

| Lanes: $\quad \mathbf{6}$ |
| :--- |
| Lanes: |

Major Approach Speed: $\qquad$ 45 Minor Approach Speed: $\qquad$

MUTCD Electronic Reference to Chapter 4: http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf

## Volume Level Criteria

1. Is the posted speed or 85 th-percentile of major street $>40 \mathrm{mph}(70 \mathrm{~km} / \mathrm{h})$ ?
2. Is the intersection in a built-up area of an isolated community with a population < 10,000?

" $70 \%$ " volume level may be used if Question 1 or 2 above is answered "Yes"
V 70\%

- 100\%


## WARRANT 1 - EIGHT-HOUR VEHICULAR VOLUME

Warrant 1 is satisfied if Condition A or Condition B is "100\%" satisfied for eight hours. Warrant 1 is also satisfied if both Condition A and Condition B are " $80 \%$ " satisfied (should only be applied after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems).

## Condition A - Minimum Vehicular Volume

| Condition A is intended for application at locations where a large volume of | 100\% Satisfied: | $\square$ Yes |
| :--- | :--- | :--- |
| intersecting traffic is the principal reason to consider installing a traffic control |  |  |
| signal. | $80 \%$ Satisfied: | $\square$ Yes |


| Number of traffic on | for moving approach | Vehicles per hour on majorstreet (total of both approaches) |  |  | Vehicles per hour on minorstreet (one direction only) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major | Minor | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ |
| 1 | 1 | 500 | 400 | 350 | 150 | 120 | 105 |
| 2 or more | 1 | 600 | 480 | 420 | 150 | 120 | 105 |
| 2 or more | 2 or more | 600 | 480 | 420 | 200 | 160 | 140 |
| 1 | 2 or more | 500 | 400 | 350 | 200 | 160 | 140 |

${ }^{\text {a }}$ Basic Minimum hourly volume
${ }^{\mathrm{b}}$ Used for combination of Conditions A and B after adequate trial of other remedial measures
${ }^{\text {c }}$ May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000
Record 8 highest hours and the corresponding major-street and minor-street volumes in the Instructions Sheet.

|  | Eight Highest Hours |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Street | $\begin{aligned} & \sum_{0}^{n} \\ & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \sum \\ & \underset{0}{0} \\ & \stackrel{O}{\dot{\gamma}} \end{aligned}$ | $\begin{aligned} & \sum \\ & \mathbf{N} \\ & \hline \mathbf{O} \\ & \ddot{0} \end{aligned}$ | $$ |  | $\begin{aligned} & \sum_{0}^{n} \\ & \text { O} \\ & \stackrel{\infty}{\infty} \end{aligned}$ |  |  |
| Major | 3,635 | 3,408 | 3,170 | 3,806 | 2,290 | 1,777 | 3,309 | 3,303 |
| Minor | 184 | 112 | 88 | 87 | 87 | 81 | 69 | 68 |

## Existing Volumes

## TRAFFIC SIGNAL WARRANT SUMMARY

## Condition B - Interruption of Continuous Traffic

Condition B is intended for application where Condition A is not satisfied and the traffic volume on a major street is so heavy that traffic on the minor intersecting street suffers excessive delay or conflict in entering or crossing the major street.

| Applicable: | $\square$ Yes | $\square$ No |
| ---: | :---: | :---: |
| 100\% Satisfied: | $\square$ Yes | $\square$ No |
| 80\% Satisfied: | $\square$ Yes | $\square$ No |
| 70\% Satisfied: | $\square$ Yes | $\square$ No |


| Number of traffic on | for moving approach | Vehicles per hour on majorstreet (total of both approaches) |  |  | Vehicles per hour on minorstreet (one direction only) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major | Minor | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ |
| 1 | 1 | 750 | 600 | 525 | 75 | 60 | 53 |
| 2 or more | 1 | 900 | 720 | 630 | 75 | 60 | 53 |
| 2 or more | 2 or more | 900 | 720 | 630 | 100 | 80 | 70 |
| 1 | 2 or more | 750 | 600 | 525 | 100 | 80 | 70 |

${ }^{\text {a }}$ Basic Minimum hourly volume
${ }^{\mathrm{b}}$ Used for combination of Conditions $A$ and $B$ after adequate trial of other remedial measures
${ }^{\text {c }}$ May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

Record 8 highest hours and the corresponding major-street and minor-street volumes in the Instructions Sheet.

| Eight Highest Hours |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Street | $\begin{aligned} & \sum_{0} \\ & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \sum \underset{0}{\sum} \\ & \stackrel{O}{\dot{j}} \end{aligned}$ |  |  |  | $\begin{aligned} & \sum_{0} \\ & \stackrel{O}{\circ} \\ & \ddot{\infty} \end{aligned}$ |  |  |
| Major | 3,635 | 3,408 | 3,170 | 3,806 | 2,290 | 1,777 | 3,309 | 3,303 |
| Minor | 184 | 112 | 88 | 87 | 87 | 81 | 69 | 68 |

## Existing Volumes



## SIGNAL WARRANT ANALYSIS

## Introduction

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Automated cells based on in Input
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Enter Four Hour Volumes
Enter Pedestrian Volumes (4-hr)
Enter Peak Hour Volumes
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City, Engineer, Date
Major and Minor Street with corresponding number of lanes and speed limits
Any 8 hours of an average day. Major-street and minor-street volumes shall be for the same 8 hours; however, the 8 hours satisfied in Condition A shall not be required to be the same 8 hours satisfied in Condition B for \(80 \%\) columns only. On the minor street, the higher volume shall not be required to be on the same approach during each of the 8 hours.
Any 4 hours of an average day. Vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor-street approach (one direction only, not required to be on the same approach during each of the 4 hours)
Pedestrians per hour crossing the major street (total of all crossings)
Enter Peak Hour Volumes
Vehicular: Any four consecutive 15-minute periods of an average day
Pedestrian: Any four consecutive 15-minute periods of an average day representing the vehicles per hour on the major street (total of both approaches) and the corresponding pedestrians per hour crossing the major street (total of all crossings)
```



## TRAFFIC SIGNAL WARRANT SUMMARY



Engineer: $\qquad$
Date:

| Lanes: $\quad \mathbf{6}$ |
| :--- |
| Lanes: $\quad \mathbf{2}$ |

Major Approach Speed:
Minor Approach Speed: $\qquad$ 45 30

## TRAFFIC SIGNAL WARRANT SUMMARY

## Condition B - Interruption of Continuous Traffic

Condition B is intended for application where Condition A is not satisfied and the traffic volume on a major street is so heavy that traffic on the minor intersecting street suffers excessive delay or conflict in entering or crossing the major street.
100\% Satisfied: $\square$ Yes $\square$
80\% Satisfied: $\square$ Yes $\square$ No
70\% Satisfied: $\square$ Yes $\square$ N No

| Number of traffic on | for moving approach | Vehicles per hour on majorstreet (total of both approaches) |  |  | Vehicles per hour on minorstreet (one direction only) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major | Minor | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ |
| 1 | 1 | 750 | 600 | 525 | 75 | 60 | 53 |
| 2 or more | 1 | 900 | 720 | 630 | 75 | 60 | 53 |
| 2 or more | 2 or more | 900 | 720 | 630 | 100 | 80 | 70 |
| 1 | 2 or more | 750 | 600 | 525 | 100 | 80 | 70 |

${ }^{\text {a }}$ Basic Minimum hourly volume
${ }^{b}$ Used for combination of Conditions $A$ and $B$ after adequate trial of other remedial measures
${ }^{\text {c }}$ May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

Record 8 highest hours and the corresponding major-street and minor-street volumes in the Instructions Sheet.

| Eight Highest Hours |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Street |  |  | $\begin{aligned} & \sum_{0} \\ & \text { O} \\ & \text { è } \end{aligned}$ |  |  | $\begin{aligned} & \sum_{0} \\ & \stackrel{\rightharpoonup}{\circ} \\ & \text { in } \end{aligned}$ |  | $\begin{aligned} & \sum_{0} \\ & \text { 을 } \\ & \underset{\sim}{n} \end{aligned}$ |
| Major | 5,266 | 5,222 | 4,262 | 3,579 | 3,703 | 3,697 | 2,586 | 3,494 |
| Minor | 200 | 136 | 108 | 102 | 99 | 87 | 80 | 76 |

## Existing Volumes



## Appendix E <br> Design Year (2045) - Build Synchro Outputs






|  | $\dagger$ |  |  | $\dagger$ |  | 4 | $\dagger$ | 4 | $\dagger$ | $p$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\uparrow$ | 「 |  | \＄ |  |  | \％ | 快 |  | ${ }^{7}$ | 4舟 |
| Trafic Volume（veh／h） | 44 | 0 | 59 | 20 | 0 | 28 | 56 | 77 | 967 | 20 | 20 | 1174 |
| Future Volume（veh／h） | 44 | 0 | 59 | 20 | 0 | 28 | 56 | 77 | 967 | 20 | 20 | 1174 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  | No |  |  | No |
| Adj Sat Flow，veh／h／ln | 1811 | 1870 | 1811 | 1870 | 1870 | 1870 |  | 1811 | 1811 | 1870 | 1870 | 1811 |
| Adj Flow Rate，veh／h | 46 | 0 | 62 | 21 | 0 | 29 |  | 81 | 1018 | 21 | 21 | 1236 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh，\％ | 6 | 2 | 6 | 2 | 2 | 2 |  | ， | 6 | 2 | 2 | 6 |
| Cap，veh／h | 242 | 0 | 119 | 118 | 12 | 61 |  | 106 | 2982 | 61 | 44 | 2773 |
| Arrive On Green | 0.08 | 0.00 | 0.08 | 0.08 | 0.00 | 0.08 |  | 0.06 | 0.60 | 0.60 | 0.02 | 0.56 |
| Sat Flow，veh／h | 1580 | 0 | 1535 | 423 | 150 | 790 |  | 1725 | 4986 | 103 | 1781 | 4944 |
| Grp Volume（v），veh／h | 46 | 0 | 62 | 50 | 0 | 0 |  | 81 | 673 | 366 | 21 | 1236 |
| Grp Sat Flow（s），veh／h／ln | 1580 | 0 | 1535 | 1363 | 0 | 0 |  | 1725 | 1648 | 1793 | 1781 | 1648 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 2.3 | 0.8 | 0.0 | 0.0 |  | 2.8 | 6.2 | 6.2 | 0.7 | 8.8 |
| Cycle Q Clear（g＿c），s | 1.5 | 0.0 | 2.3 | 2.3 | 0.0 | 0.0 |  | 2.8 | 6.2 | 6.2 | 0.7 | 8.8 |
| Prop In Lane | 1.00 |  | 1.00 | 0.42 |  | 0.58 |  | 1.00 |  | 0.06 | 1.00 |  |
| Lane Grp Cap（c），veh／h | 242 | 0 | 119 | 191 | 0 | 0 |  | 106 | 1971 | 1072 | 44 | 2773 |
| V／C Ratio（X） | 0.19 | 0.00 | 0.52 | 0.26 | 0.00 | 0.00 |  | 0.76 | 0.34 | 0.34 | 0.48 | 0.45 |
| Avail Cap（c＿a），veh／h | 550 | 0 | 460 | 518 | 0 | 0 |  | 172 | 1971 | 1072 | 148 | 2773 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 26.2 | 0.0 | 26.6 | 26.5 | 0.0 | 0.0 |  | 27.7 | 6.1 | 6.1 | 28.9 | 7.7 |
| Incr Delay（d2），s／veh | 0.4 | 0.0 | 3.5 | 0.7 | 0.0 | 0.0 |  | 10.6 | 0.5 | 0.9 | 7.9 | 0.5 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 0.6 | 0.0 | 0.9 | 0.7 | 0.0 | 0.0 |  | 1.4 | 1.6 | 1.8 | 0.4 | 2.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 26.6 | 0.0 | 30.1 | 27.3 | 0.0 | 0.0 |  | 38.3 | 6.6 | 7.0 | 36.8 | 8.2 |
| LnGrp LOS | C | A | C | C | A | A |  | D | A | A | D | A |
| Approach Vol，veh／h |  | 108 |  |  | 50 |  |  |  | 1120 |  |  | 1297 |
| Approach Delay，s／veh |  | 28.6 |  |  | 27.3 |  |  |  | 9.0 |  |  | 8.6 |
| Approach LOS |  | C |  |  | C |  |  |  | A |  |  | A |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 7.5 | 41.9 | 10.6 | 9.7 | 39.7 | 10.6 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Max Green Setting（Gmax），s | 5.0 | 19.0 | 18.0 | 6.0 | 18.0 | 18.0 |
| Max Q Clear Time（g＿c +11 ），s | 2.7 | 8.2 | 4.3 | 4.8 | 10.8 | 4.3 |
| Green Ext Time（p＿c），s | 0.0 | 4.7 | 0.3 | 0.0 | 4.4 | 0.1 |

Intersection Summary

| HCM 6th Ctrl Delay | 10.0 |
| :--- | ---: |
| HCM 6th LOS | A |

Notes
User approved ignoring U－Turning movement．

| Movement | SBR |
| :---: | :---: |
|  | 「 |
| Traffic Volume (veh/h) | 38 |
| Future Volume (veh/h) | 38 |
| Initial Q (Qb), veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1811 |
| Adj Flow Rate, veh/h | 40 |
| Peak Hour Factor | 0.95 |
| Percent Heavy Veh, \% | 6 |
| Cap, veh/h | 861 |
| Arrive On Green | 0.56 |
| Sat Flow, veh/h | 1535 |
| Grp Volume(v), veh/h | 40 |
| Grp Sat Flow(s),veh/h/ln | 1535 |
| Q Serve(g_s), s | 0.7 |
| Cycle Q Clear(g_c), s | 0.7 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 861 |
| V/C Ratio(X) | 0.05 |
| Avail Cap(c_a), veh/h | 861 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(I) | 1.00 |
| Uniform Delay (d), s/veh | 5.9 |
| Incr Delay (d2), s/veh | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.2 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d), s/veh | 6.0 |
| LnGrp LOS | A |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |






|  | $\stackrel{ }{*}$ |  |  | $\dagger$ |  | 4 | $\dagger$ | 4 | $\uparrow$ | $p$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\uparrow$ | \％ |  | $\dagger$ |  |  | \％ | 㔼 |  | \％ | 个个4 |
| Traffic Volume（veh／h） | 58 | 0 | 112 | 27 | 0 | 16 | 103 | 76 | 1204 | 27 | 27 | 989 |
| Future Volume（veh／h） | 58 | 0 | 112 | 27 | 0 | 16 | 103 | 76 | 1204 | 27 | 27 | 989 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  | No |  |  | No |
| Adj Sat Flow，veh／h／ln | 1811 | 1870 | 1811 | 1870 | 1870 | 1870 |  | 1811 | 1811 | 1870 | 1870 | 1811 |
| Adj Flow Rate，veh／h | 61 | 0 | 118 | 28 | 0 | 17 |  | 80 | 1267 | 28 | 28 | 1041 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh，\％ | 6 | 2 | 6 | 2 | 2 | 2 |  | 6 | 6 | 2 | 2 | 6 |
| Cap，veh／h | 292 | 0 | 173 | 167 | 21 | 55 |  | 106 | 2768 | 61 | 55 | 2600 |
| Arrive On Green | 0.11 | 0.00 | 0.11 | 0.11 | 0.00 | 0.11 |  | 0.06 | 0.56 | 0.56 | 0.03 | 0.53 |
| Sat Flow，veh／h | 1522 | 0 | 1535 | 617 | 188 | 489 |  | 1725 | 4977 | 110 | 1781 | 4944 |
| Grp Volume（v），veh／h | 61 | 0 | 118 | 45 | 0 | 0 |  | 80 | 839 | 456 | 28 | 1041 |
| Grp Sat Flow（s），veh／h／ln | 1522 | 0 | 1535 | 1295 | 0 | 0 |  | 1725 | 1648 | 1791 | 1781 | 1648 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 4.4 | 0.3 | 0.0 | 0.0 |  | 2.7 | 9.1 | 9.1 | 0.9 | 7.6 |
| Cycle Q Clear（g＿c），s | 1.9 | 0.0 | 4.4 | 2.2 | 0.0 | 0.0 |  | 2.7 | 9.1 | 9.1 | 0.9 | 7.6 |
| Prop In Lane | 1.00 |  | 1.00 | 0.62 |  | 0.38 |  | 1.00 |  | 0.06 | 1.00 |  |
| Lane Grp Cap（c），veh／h | 292 | 0 | 173 | 243 | 0 | 0 |  | 106 | 1833 | 996 | 55 | 2600 |
| V／C Ratio（X） | 0.21 | 0.00 | 0.68 | 0.18 | 0.00 | 0.00 |  | 0.76 | 0.46 | 0.46 | 0.51 | 0.40 |
| Avail Cap（c＿a），veh／h | 553 | 0 | 460 | 501 | 0 | 0 |  | 172 | 1833 | 996 | 148 | 2600 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 24.4 | 0.0 | 25.6 | 24.4 | 0.0 | 0.0 |  | 27.7 | 7.9 | 7.9 | 28.6 | 8.5 |
| Incr Delay（d2），s／veh | 0.4 | 0.0 | 4.7 | 0.4 | 0.0 | 0.0 |  | 10.4 | 0.8 | 1.5 | 7.0 | 0.5 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 0.8 | 0.0 | 1.7 | 0.6 | 0.0 | 0.0 |  | 1.3 | 2.5 | 2.9 | 0.5 | 2.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 24.8 | 0.0 | 30.2 | 24.7 | 0.0 | 0.0 |  | 38.1 | 8.8 | 9.4 | 35.6 | 9.0 |
| LnGrp LOS | C | A | C | C | A | A |  | D | A | A | D | A |
| Approach Vol，veh／h |  | 179 |  |  | 45 |  |  |  | 1375 |  |  | 1156 |
| Approach Delay，s／veh |  | 28.4 |  |  | 24.7 |  |  |  | 10.7 |  |  | 9.5 |
| Approach LOS |  | C |  |  | C |  |  |  | B |  |  | A |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），$s$ | 7.9 | 39.4 |  | 12.8 | 9.7 | 37.5 |  | 12.8 |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ）， s | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |  | 6.0 |  |  |  |  |
| Max Green Setting（Gmax），s | 5.0 | 19.0 |  | 18.0 | 6.0 | 18.0 |  | 18.0 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 2.9 | 11.1 |  | 6.4 | 4.7 | 9.6 |  | 4.2 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 4.7 |  | 0.5 | 0.0 | 4.4 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 11.6 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U－Turning movement．

| Movement | SBR |
| :---: | :---: |
|  | 「 |
| Traffic Volume (veh/h) | 83 |
| Future Volume (veh/h) | 83 |
| Initial Q (Qb), veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1811 |
| Adj Flow Rate, veh/h | 87 |
| Peak Hour Factor | 0.95 |
| Percent Heavy Veh, \% | 6 |
| Cap, veh/h | 807 |
| Arrive On Green | 0.53 |
| Sat Flow, veh/h | 1535 |
| Grp Volume(v), veh/h | 87 |
| Grp Sat Flow(s),veh/h/ln | 1535 |
| Q Serve(g_s), s | 1.7 |
| Cycle Q Clear(g_c), s | 1.7 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 807 |
| V/C Ratio(X) | 0.11 |
| Avail Cap(c_a), veh/h | 807 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(I) | 1.00 |
| Uniform Delay (d), s/veh | 7.2 |
| Incr Delay (d2), s/veh | 0.3 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(50\%),veh/In | 0.5 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d),s/veh | 7.4 |
| LnGrp LOS | A |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |






|  | $\stackrel{ }{*}$ |  |  | $\dagger$ |  | 4 | $\dagger$ | 4 | $\uparrow$ | $p$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\uparrow$ | 7 |  | $\dagger$ |  |  | \％ | 㔼 |  | \％ | 个个4 |
| Traffic Volume（veh／h） | 54 | 0 | 82 | 25 | 0 | 34 | 70 | 93 | 2244 | 25 | 25 | 2720 |
| Future Volume（veh／h） | 54 | 0 | 82 | 25 | 0 | 34 | 70 | 93 | 2244 | 25 | 25 | 2720 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  | No |  |  | No |
| Adj Sat Flow，veh／h／ln | 1826 | 1870 | 1826 | 1870 | 1870 | 1870 |  | 1826 | 1826 | 1870 | 1870 | 1826 |
| Adj Flow Rate，veh／h | 57 | 0 | 86 | 26 | 0 | 36 |  | 98 | 2362 | 26 | 26 | 2863 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh，\％ | 5 | 2 | 5 | 2 | 2 | 2 |  | 5 | 5 | 2 | 2 | 5 |
| Cap，veh／h | 180 | 0 | 125 | 75 | 14 | 53 |  | 123 | 3626 | 40 | 46 | 3331 |
| Arrive On Green | 0.08 | 0.00 | 0.08 | 0.08 | 0.00 | 0.08 |  | 0.07 | 0.71 | 0.71 | 0.03 | 0.67 |
| Sat Flow，veh／h | 1334 | 0 | 1547 | 298 | 177 | 657 |  | 1739 | 5083 | 56 | 1781 | 4985 |
| Grp Volume（v），veh／h | 57 | 0 | 86 | 62 | 0 | 0 |  | 98 | 1543 | 845 | 26 | 2863 |
| Grp Sat Flow（s），veh／h／ln | 1334 | 0 | 1547 | 1132 | 0 | 0 |  | 1739 | 1662 | 1816 | 1781 | 1662 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 5.4 | 1.8 | 0.0 | 0.0 |  | 5.5 | 24.8 | 24.9 | 1.4 | 44.8 |
| Cycle Q Clear（g＿c），s | 4.1 | 0.0 | 5.4 | 6.0 | 0.0 | 0.0 |  | 5.5 | 24.8 | 24.9 | 1.4 | 44.8 |
| Prop In Lane | 1.00 |  | 1.00 | 0.42 |  | 0.58 |  | 1.00 |  | 0.03 | 1.00 |  |
| Lane Grp Cap（c），veh／h | 180 | 0 | 125 | 143 | 0 | 0 |  | 123 | 2371 | 1295 | 46 | 3331 |
| V／C Ratio（X） | 0.32 | 0.00 | 0.69 | 0.43 | 0.00 | 0.00 |  | 0.80 | 0.65 | 0.65 | 0.57 | 0.86 |
| Avail Cap（c＿a），veh／h | 316 | 0 | 279 | 287 | 0 | 0 |  | 157 | 2371 | 1295 | 89 | 3331 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 44.1 | 0.0 | 44.7 | 44.8 | 0.0 | 0.0 |  | 45.8 | 7.7 | 7.7 | 48.2 | 12.9 |
| Incr Delay（d2），s／veh | 1.0 | 0.0 | 6.5 | 2.1 | 0.0 | 0.0 |  | 19.5 | 1.4 | 2.6 | 10.6 | 3.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 1.4 | 0.0 | 2.3 | 1.6 | 0.0 | 0.0 |  | 3.0 | 7.1 | 8.2 | 0.8 | 14.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 45.1 | 0.0 | 51.2 | 46.9 | 0.0 | 0.0 |  | 65.3 | 9.1 | 10.2 | 58.7 | 16.1 |
| LnGrp LOS | D | A | D | D | A | A |  | E | A | B | E | B |
| Approach Vol，veh／h |  | 143 |  |  | 62 |  |  |  | 2486 |  |  | 2936 |
| Approach Delay，s／veh |  | 48.8 |  |  | 46.9 |  |  |  | 11.7 |  |  | 16.3 |
| Approach LOS |  | D |  |  | D |  |  |  | B |  |  | B |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），$s$ | 8.6 | 77.3 |  | 14.1 | 13.1 | 72.8 |  | 14.1 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |  | 6.0 |  |  |  |  |
| Max Green Setting（Gmax），s | 5.0 | 59.0 |  | 18.0 | 9.0 | 55.0 |  | 18.0 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 3.4 | 26.9 |  | 7.4 | 7.5 | 46.8 |  | 8.0 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 23.0 |  | 0.4 | 0.0 | 7.9 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 15.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U－Turning movement．

| Movement | SBR |
| :---: | :---: |
| Lâde Configurations | 7' |
| Traffic Volume (veh/h) | 45 |
| Future Volume (veh/h) | 45 |
| Initial Q (Qb), veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1826 |
| Adj Flow Rate, veh/h | 47 |
| Peak Hour Factor | 0.95 |
| Percent Heavy Veh, \% | 5 |
| Cap, veh/h | 1034 |
| Arrive On Green | 0.67 |
| Sat Flow, veh/h | 1547 |
| Grp Volume(v), veh/h | 47 |
| Grp Sat Flow(s), veh/h/ln | 1547 |
| Q Serve(g_s), s | 1.0 |
| Cycle Q Clear(g_c), s | 1.0 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 1034 |
| V/C Ratio(X) | 0.05 |
| Avail Cap(c_a), veh/h | 1034 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(I) | 1.00 |
| Uniform Delay (d), s/veh | 5.7 |
| Incr Delay (d2), s/veh | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.3 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d),s/veh | 5.8 |
| LnGrp LOS | A |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |




Platoon blocked, \%
Mov Cap-1 Maneuver - $-\sim 166 \quad-\quad-\sim 99 \sim 74 \quad-\quad-\quad \sim-5 \sim-5 \quad-\quad$ -

Mov Cap-2 Maneuver
Stage 1
Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, S\$ 520.9 | $\$ 541$ | 9.4 |  |  |
| HCM LOS | F | F |  |  |


| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | $\sim 74$ | - | - | 166 | 99 | + | - |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 s \quad+$ : Computation Not Defined $\quad$ : All major volume in platoon



| Approach | WB | NB | SB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 105.4 | 7.5 | 78.4 |


| Minor Lane/Major Mvmt | NBL | NBT | NBRWBLn1 | SBL | SBT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 159 | - | 95 | ~33 | - |  |
| HCM Lane V/C Ratio | 1.046 | - | - 0.709 | 3.892 | - |  |
| HCM Control Delay (s) | 141.7 | - | - 105.91 | 574.1 | - |  |
| HCM Lane LOS | F | - | F | F | - |  |
| HCM 95th \%tile Q(veh) | 8.4 | - | 3.6 | 15.1 | - |  |
| Notes |  |  |  |  |  |  |
| $\sim$ : Volume exceeds capacity | \$: Delay exceeds 300s +: Computation Not Defined |  |  |  |  | *: All major volume in platoon |



## Notes

User approved ignoring U-Turning movement.

| Movement | SBR |
| :---: | :---: |
| Lâde Configurations | 「 |
| Traffic Volume (veh/h) | 98 |
| Future Volume (veh/h) | 98 |
| Initial $Q(Q b)$, veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1826 |
| Adj Flow Rate, veh/h | 103 |
| Peak Hour Factor | 0.95 |
| Percent Heavy Veh, \% | 5 |
| Cap, veh/h | 953 |
| Arrive On Green | 0.62 |
| Sat Flow, veh/h | 1547 |
| Grp Volume(v), veh/h | 103 |
| Grp Sat Flow(s), veh/h/ln | 1547 |
| Q Serve(g_s), s | 2.5 |
| Cycle Q Clear(g_c), s | 2.5 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 953 |
| V/C Ratio(X) | 0.11 |
| Avail Cap(c_a), veh/h | 953 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(l) | 1.00 |
| Uniform Delay (d), s/veh | 7.1 |
| Incr Delay (d2), s/veh | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.8 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d),s/veh | 7.3 |
| LnGrp LOS | A |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |




|  | $\stackrel{*}{ }$ | $\rightarrow$ | $\downarrow$ | 7 |  | 4 | $\dagger$ | 4 | 4 | \％ | （ | $\frac{1}{\dagger}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\uparrow$ | 「 |  | \＆ |  |  | \％ | 种险 |  | ${ }^{1 /}$ | 种 |
| Traffic Volume（veh／h） | 44 | 0 | 59 | 20 | 0 | 28 | 56 | 77 | 967 | 20 | 20 | 1174 |
| Future Volume（veh／h） | 44 | 0 | 59 | 20 | 0 | 28 | 56 | 77 | 967 | 20 | 20 | 1174 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  | No |  |  | No |
| Adj Sat Flow，veh／h／ln | 1811 | 1870 | 1811 | 1870 | 1870 | 1870 |  | 1811 | 1811 | 1870 | 1870 | 1811 |
| Adj Flow Rate，veh／h | 46 | 0 | 62 | 21 | 0 | 29 |  | 81 | 1018 | 21 | 21 | 1236 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh，\％ | 6 | 2 | 6 | 2 | 2 | 2 |  | 6 | 6 | 2 | 2 | 6 |
| Cap，veh／h | 242 | 0 | 119 | 118 | 12 | 61 |  | 106 | 2982 | 61 | 44 | 2773 |
| Arrive On Green | 0.08 | 0.00 | 0.08 | 0.08 | 0.00 | 0.08 |  | 0.06 | 0.60 | 0.60 | 0.02 | 0.56 |
| Sat Flow，veh／h | 1580 | 0 | 1535 | 423 | 150 | 790 |  | 1725 | 4986 | 103 | 1781 | 4944 |
| Grp Volume（v），veh／h | 46 | 0 | 62 | 50 | 0 | 0 |  | 81 | 673 | 366 | 21 | 1236 |
| Grp Sat Flow（s），veh／h／ln | 1580 | 0 | 1535 | 1363 | 0 | 0 |  | 1725 | 1648 | 1793 | 1781 | 1648 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 2.3 | 0.8 | 0.0 | 0.0 |  | 2.8 | 6.2 | 6.2 | 0.7 | 8.8 |
| Cycle Q Clear（g＿c），s | 1.5 | 0.0 | 2.3 | 2.3 | 0.0 | 0.0 |  | 2.8 | 6.2 | 6.2 | 0.7 | 8.8 |
| Prop In Lane | 1.00 |  | 1.00 | 0.42 |  | 0.58 |  | 1.00 |  | 0.06 | 1.00 |  |
| Lane Grp Cap（c），veh／h | 242 | 0 | 119 | 191 | 0 | 0 |  | 106 | 1971 | 1072 | 44 | 2773 |
| V／C Ratio（X） | 0.19 | 0.00 | 0.52 | 0.26 | 0.00 | 0.00 |  | 0.76 | 0.34 | 0.34 | 0.48 | 0.45 |
| Avail Cap（c＿a），veh／h | 550 | 0 | 460 | 518 | 0 | 0 |  | 172 | 1971 | 1072 | 148 | 2773 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 26.2 | 0.0 | 26.6 | 26.5 | 0.0 | 0.0 |  | 27.7 | 6.1 | 6.1 | 28.9 | 7.7 |
| Incr Delay（d2），s／veh | 0.4 | 0.0 | 3.5 | 0.7 | 0.0 | 0.0 |  | 10.6 | 0.5 | 0.9 | 7.9 | 0.5 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.6 | 0.0 | 0.9 | 0.7 | 0.0 | 0.0 |  | 1.4 | 1.6 | 1.8 | 0.4 | 2.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 26.6 | 0.0 | 30.1 | 27.3 | 0.0 | 0.0 |  | 38.3 | 6.6 | 7.0 | 36.8 | 8.2 |
| LnGrp LOS | C | A | C | C | A | A |  | D | A | A | D | A |
| Approach Vol，veh／h |  | 108 |  |  | 50 |  |  |  | 1120 |  |  | 1297 |
| Approach Delay，s／veh |  | 28.6 |  |  | 27.3 |  |  |  | 9.0 |  |  | 8.6 |
| Approach LOS |  | C |  |  | C |  |  |  | A |  |  | A |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 7.5 | 41.9 | 10.6 | 9.7 | 39.7 | 10.6 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Max Green Setting（Gmax），s | 5.0 | 19.0 | 18.0 | 6.0 | 18.0 | 18.0 |
| Max Q Clear Time（g＿c＋11），s | 2.7 | 8.2 | 4.3 | 4.8 | 10.8 | 4.3 |
| Green Ext Time（p＿c），s | 0.0 | 4.7 | 0.3 | 0.0 | 4.4 | 0.1 |

Intersection Summary

| HCM 6th Ctrl Delay | 10.0 |
| :--- | ---: |
| HCM 6th LOS | A |

Notes
User approved ignoring U－Turning movement．

| Movement | SBR |
| :---: | :---: |
| Lâde Configurations | 「 |
| Traffic Volume (veh/h) | 38 |
| Future Volume (veh/h) | 38 |
| Initial $Q(Q b)$, veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1811 |
| Adj Flow Rate, veh/h | 40 |
| Peak Hour Factor | 0.95 |
| Percent Heavy Veh, \% | 6 |
| Cap, veh/h | 861 |
| Arrive On Green | 0.56 |
| Sat Flow, veh/h | 1535 |
| Grp Volume(v), veh/h | 40 |
| Grp Sat Flow(s), veh/h/ln | 1535 |
| Q Serve(g_s), s | 0.7 |
| Cycle Q Clear(g_c), s | 0.7 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 861 |
| V/C Ratio(X) | 0.05 |
| Avail Cap(c_a), veh/h | 861 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(l) | 1.00 |
| Uniform Delay (d), s/veh | 5.9 |
| Incr Delay (d2), s/veh | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.2 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d),s/veh | 6.0 |
| LnGrp LOS | A |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |




|  | $\dagger$ | $\rightarrow$ |  | 7 |  |  | $\dagger$ | 4 | $\uparrow$ | $p$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\uparrow$ | 7 |  | \$ |  |  | \% |  |  | \% | 个个4 |
| Traffic Volume (veh/h) | 58 | 0 | 112 | 27 | 0 | 16 | 103 | 76 | 1204 | 27 | 27 | 989 |
| Future Volume (veh/h) | 58 | 0 | 112 | 27 | 0 | 16 | 103 | 76 | 1204 | 27 | 27 | 989 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  | No |  |  | No |
| Adj Sat Flow, veh/h/ln | 1811 | 1870 | 1811 | 1870 | 1870 | 1870 |  | 1811 | 1811 | 1870 | 1870 | 1811 |
| Adj Flow Rate, veh/h | 61 | 0 | 118 | 28 | 0 | 17 |  | 80 | 1267 | 28 | 28 | 1041 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, \% | 6 | 2 | 6 | 2 | 2 | 2 |  | 6 | 6 | 2 | 2 | 6 |
| Cap, veh/h | 292 | 0 | 173 | 167 | 21 | 55 |  | 106 | 2768 | 61 | 55 | 2600 |
| Arrive On Green | 0.11 | 0.00 | 0.11 | 0.11 | 0.00 | 0.11 |  | 0.06 | 0.56 | 0.56 | 0.03 | 0.53 |
| Sat Flow, veh/h | 1522 | 0 | 1535 | 617 | 188 | 489 |  | 1725 | 4977 | 110 | 1781 | 4944 |
| Grp Volume(v), veh/h | 61 | 0 | 118 | 45 | 0 | 0 |  | 80 | 839 | 456 | 28 | 1041 |
| Grp Sat Flow(s),veh/h/n | 1522 | 0 | 1535 | 1295 | 0 | 0 |  | 1725 | 1648 | 1791 | 1781 | 1648 |
| Q Serve(g_s), s | 0.0 | 0.0 | 4.4 | 0.3 | 0.0 | 0.0 |  | 2.7 | 9.1 | 9.1 | 0.9 | 7.6 |
| Cycle Q Clear (g_c), s | 1.9 | 0.0 | 4.4 | 2.2 | 0.0 | 0.0 |  | 2.7 | 9.1 | 9.1 | 0.9 | 7.6 |
| Prop In Lane | 1.00 |  | 1.00 | 0.62 |  | 0.38 |  | 1.00 |  | 0.06 | 1.00 |  |
| Lane Grp Cap (c), veh/h | 292 | 0 | 173 | 243 | 0 | 0 |  | 106 | 1833 | 996 | 55 | 2600 |
| V/C Ratio(X) | 0.21 | 0.00 | 0.68 | 0.18 | 0.00 | 0.00 |  | 0.76 | 0.46 | 0.46 | 0.51 | 0.40 |
| Avail Cap(c_a), veh/h | 553 | 0 | 460 | 501 | 0 | 0 |  | 172 | 1833 | 996 | 148 | 2600 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 24.4 | 0.0 | 25.6 | 24.4 | 0.0 | 0.0 |  | 27.7 | 7.9 | 7.9 | 28.6 | 8.5 |
| Incr Delay (d2), s/veh | 0.4 | 0.0 | 4.7 | 0.4 | 0.0 | 0.0 |  | 10.4 | 0.8 | 1.5 | 7.0 | 0.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.8 | 0.0 | 1.7 | 0.6 | 0.0 | 0.0 |  | 1.3 | 2.5 | 2.9 | 0.5 | 2.1 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 24.8 | 0.0 | 30.2 | 24.7 | 0.0 | 0.0 |  | 38.1 | 8.8 | 9.4 | 35.6 | 9.0 |
| LnGrp LOS | C | A | C | C | A | A |  | D | A | A | D | A |
| Approach Vol, veh/h |  | 179 |  |  | 45 |  |  |  | 1375 |  |  | 1156 |
| Approach Delay, s/veh |  | 28.4 |  |  | 24.7 |  |  |  | 10.7 |  |  | 9.5 |
| Approach LOS |  | C |  |  | C |  |  |  | B |  |  | A |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 7.9 | 39.4 |  | 12.8 | 9.7 | 37.5 |  | 12.8 |  |  |  |  |
| Change Period ( $Y+R \mathrm{Rc}$ ), s | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |  | 6.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.0 | 19.0 |  | 18.0 | 6.0 | 18.0 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 2.9 | 11.1 |  | 6.4 | 4.7 | 9.6 |  | 4.2 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 4.7 |  | 0.5 | 0.0 | 4.4 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr DelayHCM 6th LOS |  |  | 11.6 |  |  |  |  |  |  |  |  |  |
|  |  |  | B |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U-Turning movement.

| Movement | SBR |
| :---: | :---: |
| Lâde Configurations | 「 |
| Traffic Volume (veh/h) | 83 |
| Future Volume (veh/h) | 83 |
| Initial $Q(Q b)$, veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1811 |
| Adj Flow Rate, veh/h | 87 |
| Peak Hour Factor | 0.95 |
| Percent Heavy Veh, \% | 6 |
| Cap, veh/h | 807 |
| Arrive On Green | 0.53 |
| Sat Flow, veh/h | 1535 |
| Grp Volume(v), veh/h | 87 |
| Grp Sat Flow(s),veh/h/ln | 1535 |
| Q Serve(g_s), s | 1.7 |
| Cycle Q Clear(g_c), s | 1.7 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 807 |
| V/C Ratio(X) | 0.11 |
| Avail Cap(c_a), veh/h | 807 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(I) | 1.00 |
| Uniform Delay (d), s/veh | 7.2 |
| Incr Delay (d2), s/veh | 0.3 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.5 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d),s/veh | 7.4 |
| LnGrp LOS | A |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |




| Approach | WB | NB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 10.8 | 1.2 |


| Minor Lane/Major Mvmt | NBL | NBT | NBRWBLn1 | SBL | SBT |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 101 | - | - | - | 155 | - |
| HCM Lane V/C Ratio | 1.199 | - | - | -0.475 | - |  |
| HCM Control Delay (s) | 231 | - | - | 0 | 47.7 | - |
| HCM Lane LOS | F | - | - | A | E | - |
| HCM 95th \%tile Q(veh) | 8.1 | - | - | - | 2.2 | - |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 s \quad+$ : Computation Not Defined $\quad$ : All major volume in platoon


## Notes

User approved ignoring U-Turning movement.

| Movement | SBR |
| :---: | :---: |
| Lâde Configurations | 7' |
| Traffic Volume (veh/h) | 45 |
| Future Volume (veh/h) | 45 |
| Initial Q (Qb), veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1826 |
| Adj Flow Rate, veh/h | 47 |
| Peak Hour Factor | 0.95 |
| Percent Heavy Veh, \% | 5 |
| Cap, veh/h | 1034 |
| Arrive On Green | 0.67 |
| Sat Flow, veh/h | 1547 |
| Grp Volume(v), veh/h | 47 |
| Grp Sat Flow(s), veh/h/ln | 1547 |
| Q Serve(g_s), s | 1.0 |
| Cycle Q Clear(g_c), s | 1.0 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 1034 |
| V/C Ratio(X) | 0.05 |
| Avail Cap(c_a), veh/h | 1034 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(I) | 1.00 |
| Uniform Delay (d), s/veh | 5.7 |
| Incr Delay (d2), s/veh | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(95\%),veh/ln | 0.6 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d),s/veh | 5.8 |
| LnGrp LOS | A |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |




| Approach | WB | NB | SB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 105.4 | 29.7 | 78.4 |
| HCM LOS | F |  |  |


| Minor Lane/Major Mvmt | NBL | NBT | NBRWBLn1 | SBL | SBT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 159 | - | 95 | ~33 | - |  |
| HCM Lane V/C Ratio | 1.648 | - | - 0.709 | 3.892 | - |  |
| HCM Control Delay (s) | \$ 368.7 | - | - 105.91 | 574.1 | - |  |
| HCM Lane LOS | F | - | F | F | - |  |
| HCM 95th \%tile Q(veh) | 18.3 | - | 3.6 | 15.1 | - |  |
| Notes |  |  |  |  |  |  |
| $\sim$ Volume exceeds capacity | \$: Delay exceeds 300s +: Computation Not Defined |  |  |  |  | *: All major volume in platoon |


|  | $\stackrel{ }{*}$ | $\rightarrow$ |  | 7 |  | 4 | $\dagger$ | 4 | $\uparrow$ | $p$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\uparrow$ | F |  | ¢ |  |  | \％ | 个中t |  | \％ | 个种 |
| Traffic Volume（veh／h） | 68 | 0 | 132 | 32 | 0 | 16 | 122 | 89 | 2710 | 32 | 32 | 2183 |
| Future Volume（veh／h） | 68 | 0 | 132 | 32 | 0 | 16 | 122 | 89 | 2710 | 32 | 32 | 2183 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  | No |  |  | No |
| Adj Sat Flow，veh／h／ln | 1826 | 1870 | 1826 | 1870 | 1870 | 1870 |  | 1826 | 1826 | 1870 | 1870 | 1826 |
| Adj Flow Rate，veh／h | 72 | 0 | 139 | 34 | 0 | 17 |  | 94 | 2853 | 34 | 34 | 2298 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh，\％ | 5 | 2 | 5 | 2 | 2 | 2 |  | 5 | 5 | 2 | 2 | 5 |
| Cap，veh／h | 246 | 0 | 178 | 129 | 13 | 38 |  | 120 | 3317 | 39 | 57 | 3071 |
| Arrive On Green | 0.11 | 0.00 | 0.11 | 0.11 | 0.00 | 0.11 |  | 0.07 | 0.65 | 0.65 | 0.03 | 0.62 |
| Sat Flow，veh／h | 1448 | 0 | 1547 | 545 | 113 | 329 |  | 1739 | 5078 | 60 | 1781 | 4985 |
| Grp Volume（v），veh／h | 72 | 0 | 139 | 51 | 0 | 0 |  | 94 | 1863 | 1024 | 34 | 2298 |
| Grp Sat Flow（s），veh／h／ln | 1448 | 0 | 1547 | 987 | 0 | 0 |  | 1739 | 1662 | 1815 | 1781 | 1662 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 7.9 | 1.9 | 0.0 | 0.0 |  | 4.8 | 39.8 | 40.4 | 1.7 | 29.6 |
| Cycle Q Clear（g＿c），s | 4.1 | 0.0 | 7.9 | 6.0 | 0.0 | 0.0 |  | 4.8 | 39.8 | 40.4 | 1.7 | 29.6 |
| Prop In Lane | 1.00 |  | 1.00 | 0.67 |  | 0.33 |  | 1.00 |  | 0.03 | 1.00 |  |
| Lane Grp Cap（c），veh／h | 246 | 0 | 178 | 180 | 0 | 0 |  | 120 | 2171 | 1186 | 57 | 3071 |
| V／C Ratio（X） | 0.29 | 0.00 | 0.78 | 0.28 | 0.00 | 0.00 |  | 0.78 | 0.86 | 0.86 | 0.60 | 0.75 |
| Avail Cap（c＿a），veh／h | 365 | 0 | 309 | 294 | 0 | 0 |  | 232 | 2171 | 1186 | 99 | 3071 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 37.0 | 0.0 | 38.7 | 38.1 | 0.0 | 0.0 |  | 41.2 | 12.3 | 12.4 | 43.0 | 12.3 |
| Incr Delay（d2），s／veh | 0.7 | 0.0 | 7.3 | 0.9 | 0.0 | 0.0 |  | 10.6 | 4.7 | 8.4 | 9.8 | 1.7 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（95\％），veh／ln | 2.7 | 0.0 | 5.9 | 2.0 | 0.0 | 0.0 |  | 4.2 | 18.6 | 21.7 | 1.6 | 14.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 37.7 | 0.0 | 46.0 | 38.9 | 0.0 | 0.0 |  | 51.8 | 17.0 | 20.8 | 52.8 | 14.0 |
| LnGrp LOS | D | A | D | D | A | A |  | D | B | C | D | B |
| Approach Vol，veh／h |  | 211 |  |  | 51 |  |  |  | 2981 |  |  | 2435 |
| Approach Delay，s／veh |  | 43.2 |  |  | 38.9 |  |  |  | 19.4 |  |  | 14.3 |
| Approach LOS |  | D |  |  | D |  |  |  | B |  |  | B |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s | 8.9 | 64.8 |  | 16.3 | 12.2 | 61.4 |  | 16.3 |  |  |  |  |
| Change Period（ $Y+R \mathrm{C}$ ），s | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |  | 6.0 |  |  |  |  |
| Max Green Setting（Gmax），s | 5.0 | 49.0 |  | 18.0 | 12.0 | 42.0 |  | 18.0 |  |  |  |  |
| Max Q Clear Time（g＿c＋1），s | 3.7 | 42.4 |  | 9.9 | 6.8 | 31.6 |  | 8.0 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 6.3 |  | 0.5 | 0.1 | 9.1 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 18.3 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U－Turning movement．

| Movement | SBR |
| :---: | :---: |
| Lâde Configurations | 「 |
| Traffic Volume (veh/h) | 98 |
| Future Volume (veh/h) | 98 |
| Initial $Q(Q b)$, veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1826 |
| Adj Flow Rate, veh/h | 103 |
| Peak Hour Factor | 0.95 |
| Percent Heavy Veh, \% | 5 |
| Cap, veh/h | 953 |
| Arrive On Green | 0.62 |
| Sat Flow, veh/h | 1547 |
| Grp Volume(v), veh/h | 103 |
| Grp Sat Flow(s), veh/h/ln | 1547 |
| Q Serve(g_s), s | 2.5 |
| Cycle Q Clear(g_c), s | 2.5 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 953 |
| V/C Ratio(X) | 0.11 |
| Avail Cap(c_a), veh/h | 953 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(l) | 1.00 |
| Uniform Delay (d), s/veh | 7.1 |
| Incr Delay (d2), s/veh | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(95\%),veh/ln | 1.4 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d),s/veh | 7.3 |
| LnGrp LOS | A |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |

