

PROJECT TRAFFIC ANALYSIS REPORT

Florida Department of Transportation

District One

SR 70 Project Development and Environment (PD&E) Study

Limits of Project: From Lonesome Island Road to the Southern Leg of CR 721

Highlands County, Florida

Financial Management Number: 449851-1-22-01

ETDM Number: 14490

Date: January 2025

The environmental review, consultation, and other actions required by applicable federal environmental laws for this project are being, or have been, carried out by the Florida Department of Transportation (FDOT) pursuant to 23 U.S.C. § 327 and a Memorandum of Understanding dated May 26, 2022, and executed by the Federal Highway Administration and FDOT.

Project Traffic Analysis Report
SR 70 from Lonesome Island Road to the Southern Leg of CR 721

PROFESSIONAL ENGINEER CERTIFICATE

I hereby certify that I am registered professional engineer in the State of Florida practicing with Kisinger Campo & Associates, and that I have supervised the preparation of, and approved the analysis, findings, opinions, conclusions, and technical advice reported in:

REPORT: Project Traffic Analysis Report
PROJECT: SR 70 from Lonesome Island Road to the Southern Leg of CR 721
LOCATION: Highlands County
FPID NO.: 449851-1-22-01
CLIENT: District 1

The following duly authorized engineering business performed the engineering work represented by this report:

Kisinger Campo & Associates, Corp.
201 N. Franklin St., Suite 400
Tampa, FL 33602
Telephone: (813) 871-5331

I, M. Fathy Abdalla, Florida P.E. Number 63914, have prepared this Project Traffic Analysis Report (PTAR) for SR 70 from Lonesome Island Road to the Southern Leg of CR 721. This PTAR contains detailed engineering information that fulfills the purpose and need for this project.

I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of transportation engineering as applied through design standards and criteria set forth by the federal, state, and local regulatory agencies as well as professional judgement and experience.

Name: M. Fathy Abdalla, P.E.

Signature: _____

P.E. Number: 63914

Date: _____

This report has been digitally signed and sealed by M. Fathy Abdalla, P.E. on the date indicated here. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies

Executive Summary

The Florida Department of Transportation (FDOT) District One is conducting a Project Development and Environment (PD&E) study for proposed improvements to the State Road (SR) 70 corridor in Highlands County. The intent is to provide additional roadway capacity and enhance safety along the SR 70 corridor, a major east-west roadway spanning the state. The project limits extend approximately 7.6 miles from Lonesome Island Road to the southern leg of County Road (CR) 721 in Highlands County. SR 70 is a designated hurricane evacuation route and part of Florida's Strategic Intermodal System (SIS). Facilities on the SIS are subject to special standards and criteria for design speed, level of service and other requirements. The existing SR 70 does not meet SIS facility criteria.

The study focuses on improving capacity and safety of this section of SR 70. Alternatives to be evaluated include adding an additional through lane in each direction, adding a median, and widening travel lanes from 10 feet to 12 feet as part of the project. Multimodal facilities (i.e., a shared use path) will also be considered along the project segment. Each alternative will be evaluated to determine social and environmental impacts, safety enhancements, additional right-of-way needs, and traffic performance.

This Project Traffic Analysis Report (PTAR) is for SR 70 from Lonesome Island Rd to the Southern Leg of CR 721, a two-lane roadway segment approximately 7.6 miles long. The purpose of this PTAR is to analyze the existing and proposed conditions of SR 70 and make recommendations that will improve arterial level of service (LOS), driver safety, and reduce the number of crashes experienced along the corridor. This PTAR also evaluates additional capacity needs to maintain acceptable clearance time during emergency evacuation scenarios along the corridor in the coming years.

Purpose and Need: SR 70 project improvements are recommended based on historic crash data of the corridor, existing evacuation clearance times, and population growth in the project area. SR 70 serves as a major east-west corridor and evacuation route in Highlands County and across the state of Florida.

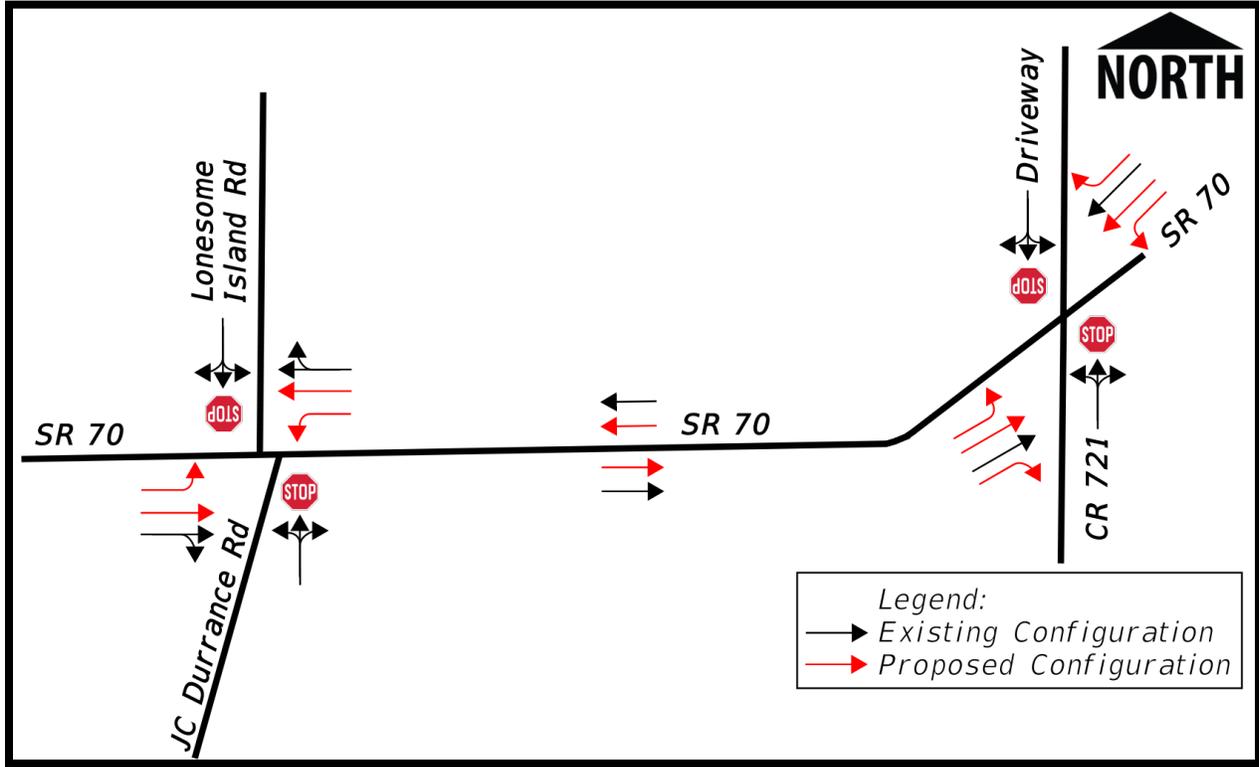
Existing Analysis: The Existing Year 2022 capacity analysis shows that SR 70 currently operates at an acceptable LOS. However, analysis of the crashes that have occurred along the corridor in the past 5 years show that the crash rate for the corridor is currently 36% higher than the statewide average for rural 2-3 lanes two-way undivided roadways. Existing evacuation scenarios for Highlands County show excessive evacuation clearance times for Out of County evacuations. Concerns about the road's ability to handle future evacuation scenarios have arisen due to the projected population growth of the surrounding areas.

Future Analysis: This study forecasts Opening Year 2032 and Design Year 2052 traffic volumes to assess the improvements needed to meet the expected demand within the study area. In addition, the following two different design alternatives were evaluated to compare LOS, safety, and evacuation clearance times:

1. No-Build scenario consisting of the existing two-lane undivided mainline and intersection configurations within the project area. The Design Year 2052 No-Build capacity analysis shows that SR 70 and both intersections are expected to operate at an acceptable LOS.
2. Build scenario consisting of widening SR 70 from a two-lane undivided roadway to a four-lane divided roadway with a median. At the intersections of SR 70 at Lonesome Island Rd/JC Durrance Rd and SR 70 at CR 721, the Build scenario consists of adding dedicated left turn storage lanes. Both intersections

would remain as two-way stop-controlled (TWSC) intersections under the Build scenario. The following figure shows the proposed lane geometry of the Build scenario.

Build Scenario Proposed Lane Geometry



The Design Year 2052 Build capacity analysis shows that SR 70 and both intersections are expected to operate at an acceptable LOS. Widening SR 70 from two to four lanes will decrease crashes by preventing drivers from using the oncoming lane to pass other vehicles. Also, by widening SR 70, the number of crashes in 2052 are predicted to decrease by approximately 54% (26.2 crashes per year) when compared to the predicted No-Build 2052 number of crashes of 48.2 crashes per year. The proposed widening of SR 70 will also increase the capacity of the roadway, leading to decreased evacuation clearance times for Highlands County in the future.

The Build Alternative is the recommended design alternative. Widening SR 70 from two lanes to four lanes from Lonesome Island Road to the Southern Leg of CR 721 is projected to decrease future number of crashes and evacuation clearance times, while maintaining an acceptable LOS throughout the corridor and at both intersections.

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Section 1 Introduction

The objective of the Project Development and Environment (PD&E) study is to assist the Florida Department of Transportation's (FDOT) Office of Environmental Management (OEM) in reaching a decision on the type, location, and conceptual design of the proposed improvements for the widening of SR 70. This study documents the need for the improvements as well as the procedures utilized to develop and evaluate various improvements, including elements such as proposed typical sections, preliminary horizontal alignments, stormwater management facility (SMF) and floodplain compensation (FPC) sites, and intersection enhancements.

The PD&E study satisfies all applicable requirements, including the National Environmental Policy Act (NEPA), to qualify for federal-aid funding of subsequent development phases (design, right of way acquisition, and construction). This project was screened through the FDOT's Efficient Transportation Decision Making (ETDM) process as ETDM Project No. 14490. The ETDM Programming Screen Summary Report was published on June 1, 2023, containing details concerning agency comments from the Environmental Technical Advisory Team (ETAT) on the project's potential effects to natural, cultural, and community resources; and provide additional documentation of activities related to the Programming Phase of the project. physical, and social resources. A Type 2 Categorical Exclusion is anticipated as the class of action for this PD&E study.

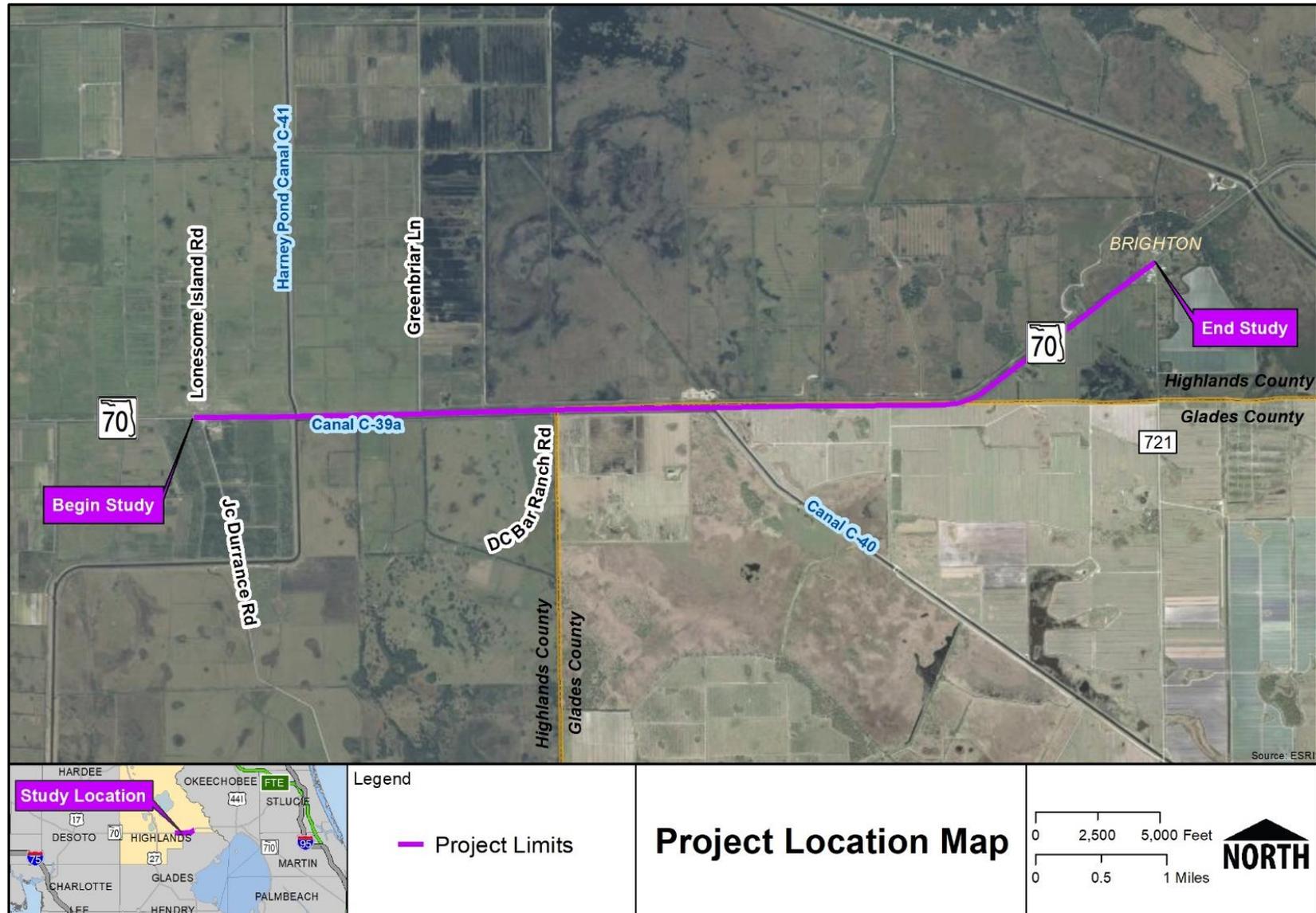
1.1 Project Description

This roadway project proposes the widening of a two-lane facility up to a four-lane, divided facility and/or the inclusion of operational improvements along 7.6 miles of SR 70 from Lonesome Island Road to the southern leg of CR 721 in Highlands County. Travel lane widths may be widened from 10 feet to 12 feet as part of the project. Multimodal facilities will also be considered along the project segment, where appropriate.

SR 70 is part of Florida's Strategic Intermodal System (SIS) highway network and designated state hurricane evacuation route network. As part of the National Highway System, SR 70 is critical to the transportation network as it facilitates local and regional traffic and the movement of goods/freight. SR 70 is functionally classified as "Rural Principal Arterial – Other" within the project area, and the project segment of the roadway has an existing context classification of C2-Rural. The existing typical section consists of a two-lane undivided facility with 10-foot (ft) travel lanes. There are 8-ft shoulders, 4-ft of which are paved; however, there are no designated bicycle lanes or sidewalks present on either side. The posted speed limit along the project corridor is 60 miles per hour.

The existing right-of-way (ROW) width along SR 70 project segment is generally 50-70 ft. A deep canal runs intermittently along the southern border of the project limits. Additional ROW is expected to accommodate the proposed improvements. A project location map is provided in **Figure 1-1**.

Figure 1-1 | Project Location Map



1.2 Purpose and Need

The purpose of this project is to address traffic safety conditions on State Road (SR) 70 from Lonesome Island Road to the southern leg of County Road (CR) 721 within Highlands County. Other goals of the project are to maintain important east-west connectivity within the regional transportation network and accommodate freight activity within the area.

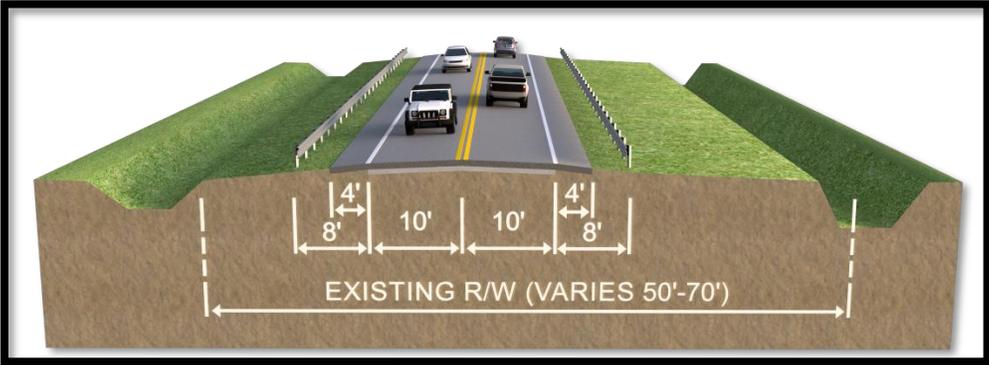
This project is needed to improve traffic safety conditions, emergency evacuation, and incident response times. Other goals of the project are to maintain important east-west connectivity within the regional transportation network and accommodate freight activity within the area.

1.3 Existing Roadway and Proposed Improvements

1.3.1 Existing Roadway

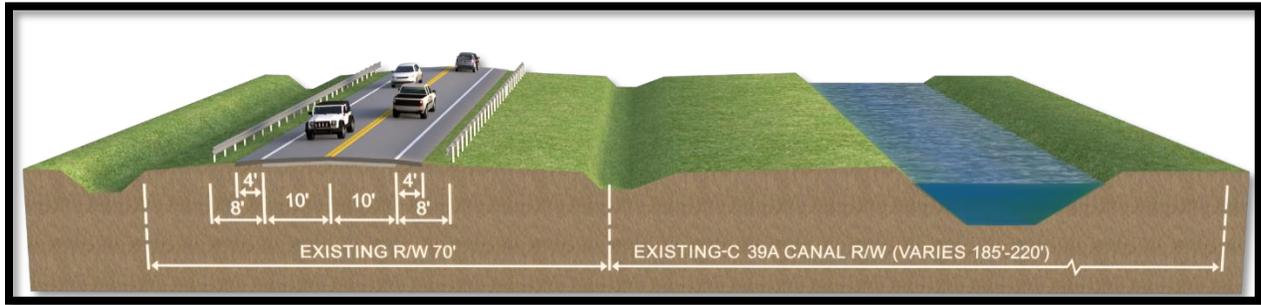
Within the project area, SR 70 is currently a two-lane undivided roadway functionally classified as a rural principal arterial other roadway with a posted speed limit of 60 miles per hour (mph). The roadway has one 10-foot (ft) lane in each direction, with shoulders that are approximately 8-ft wide (4-ft paved) on both the south and north side throughout the corridor with no dedicated bicycle lanes or sidewalk. The existing ROW width varies along the corridor, and is a minimum of 50 ft. There are two existing typical sections within the study limits. The limits of existing roadway Typical Section One is from Lonesome Island Road to Harvey Pond Canal C-41 and from Indian Prairie Canal C-40 to CR 721 (Southern Leg) and is provided as **Figure 1-2**. The limits of existing roadway Typical Section Two are from Harvey Pond Canal C-41 to Indian Prairie Canal C-40 and is provided as **Figure 1-3**.

Figure 1-2 | SR 70 – Existing Roadway Typical Section One



From Lonesome Island Road to Harvey Pond Canal C-41 and
From Indian Prairie Canal C-40 to CR 721 (Southern Leg)

Figure 1-3 | SR 70 – Existing Roadway Typical Section Two



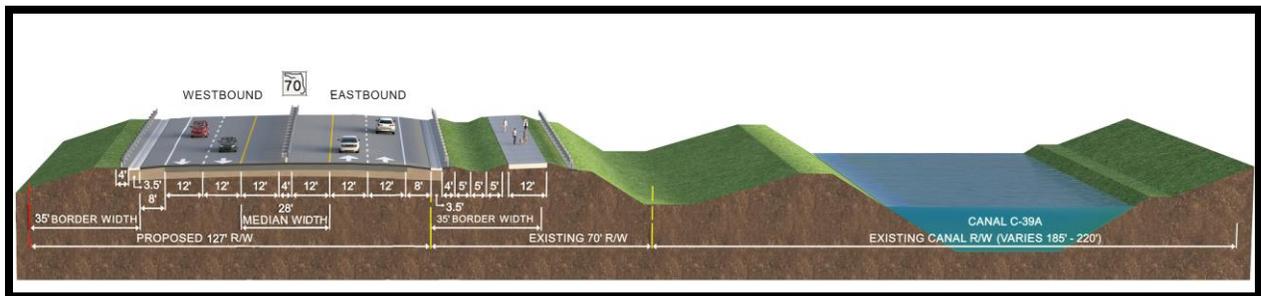
From Harvey Pond Canal C-41 to Indian Prairie Canal C-40

1.3.2 Proposed Improvements

The proposed typical sections show widening SR 70 to a four-lane divided rural roadway. There will be two 12-ft travel lanes in each direction, with outside shoulders. Throughout the corridor, a 12-ft shared use path is proposed along the south side of the road. The proposed ROW varies along the corridor, and is a minimum of an additional 60 ft. There are three proposed typical sections within the study limits. The proposed Typical Section One shows widening SR 70 to a four-lane divided rural roadway with a 4-ft guardrail. There will be two 12-ft travel lanes in each direction, with outside shoulders that are approximately 8-ft wide (3.5-ft paved). Proposed Typical Section One is from Lonesome Island Road to Indian Prairie Canal C-40 and is provided as **Figure 1-4**.

The proposed typical section is being evaluated to determine social and environmental impacts, safety enhancements, additional right-of-way needs, and traffic performance. The project includes the evaluation of SMF and FPC sites. Additional ROW will be required along SR 70 and for SMF and FPC sites.

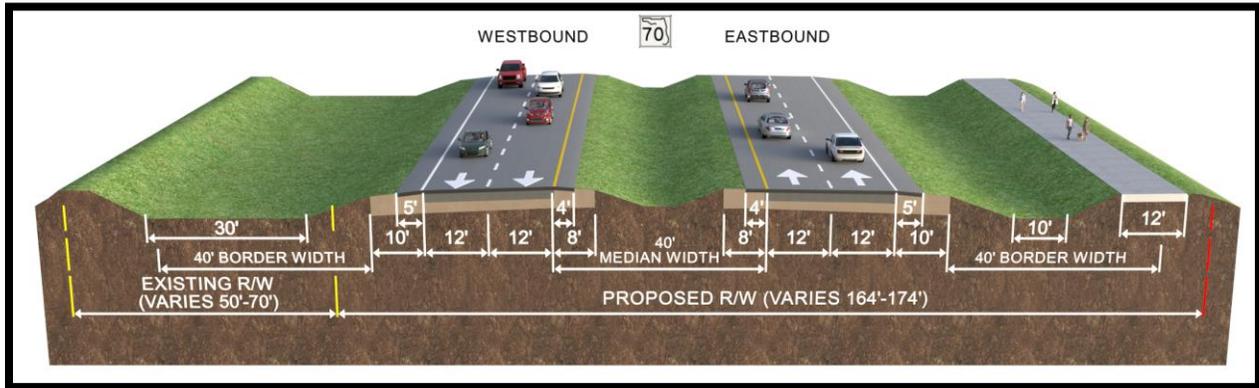
Figure 1-4 | SR 70 – Proposed Roadway Typical Section One



From Lonesome Island Road to Indian Prairie Canal C-40

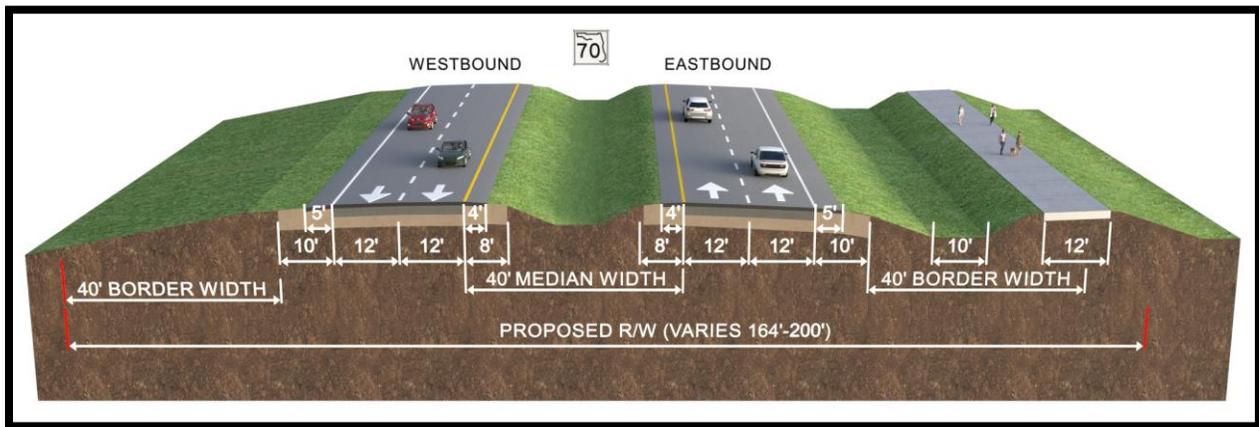
The proposed Typical Section Two and Three show widening SR 70 to a four-lane divided rural roadway with a 40-ft median. There will be two 12-ft travel lanes in each direction, with outside shoulders that are approximately 10-ft wide (5-ft paved). Proposed Typical Section Two is from Indian Prairie Canal C-40 to West of CR 721 (Southern Leg) and is provided as **Figure 1-5**. Proposed Typical Section Three is from West of CR 721 (Southern Leg) to CR 721 (Southern Leg) and is provided as **Figure 1-6**.

Figure 1-5 | SR 70 – Proposed Roadway Typical Section Two



From East of Indian Prairie Canal C-40 to West of CR 721

Figure 1-6 | SR 70 – Proposed Roadway Typical Section Three



From West of CR 721 to CR 721

1.4 Report Purpose

This Project Traffic Analysis Report (PTAR) summarizes the traffic data collected and the traffic level of service (LOS) analyses for the SR 70 project in Highlands County, Florida. The purpose of this PTAR is to analyze the existing and proposed conditions of SR 70 and make recommendations that will improve arterial LOS, driver safety, and reduce the number of crashes experienced along the corridor. This PTAR also evaluates additional capacity needs to maintain acceptable clearance time during emergency evacuation scenarios along the corridor in the coming years. **Appendix A** includes a copy of the Methodology Letter of Understanding (MLOU) for this project.

Section 2 Existing Conditions

The following section provides an evaluation of the existing conditions within the influence area. **Figure 2-1** shows the project study area. The discussion items include existing traffic data and existing operating conditions. The intersections along the study corridor as listed below are a part of this study:

1. SR 70 at Lonesome Island Road/JC Durrance Road
2. SR 70 at CR 721

Figure 2-1 | SR 70 – Project Study Area



2.1 Existing Geometry

The segment of SR 70 between Lonesome Island Road and CR 721 is a two-lane roadway approximately 7.6 miles long. There are existing unsignalized intersections at Lonesome Island Road/JC Durrance Road and CR 721, as well as driveways and side streets throughout the segment. The existing lane geometry is shown in **Figure 2-2**.

Lonesome Island Road/JC Durrance Road at SR 70 is a two-way stop-controlled (TWSC) intersection. The eastbound and westbound approaches consist of one shared through left-turn right-turn lane. The northbound approach consists of one shared left-turn right-turn lane. The southbound approach operates as stop-controlled despite the lack of an existing stop sign. The northbound and southbound approaches do not line up across from one another; however, for simplicity the two unpaved side streets were modeled together as one intersection. There are no existing pedestrian signals, crosswalks, bike lanes, curb ramps,

or sidewalks along any approaches to the intersection. The existing posted speed on SR 70 is 60 mph. The existing intersection conditions are shown in **Figure 2-3**.

Figure 2-2 | SR 70 – Existing Lane Geometry

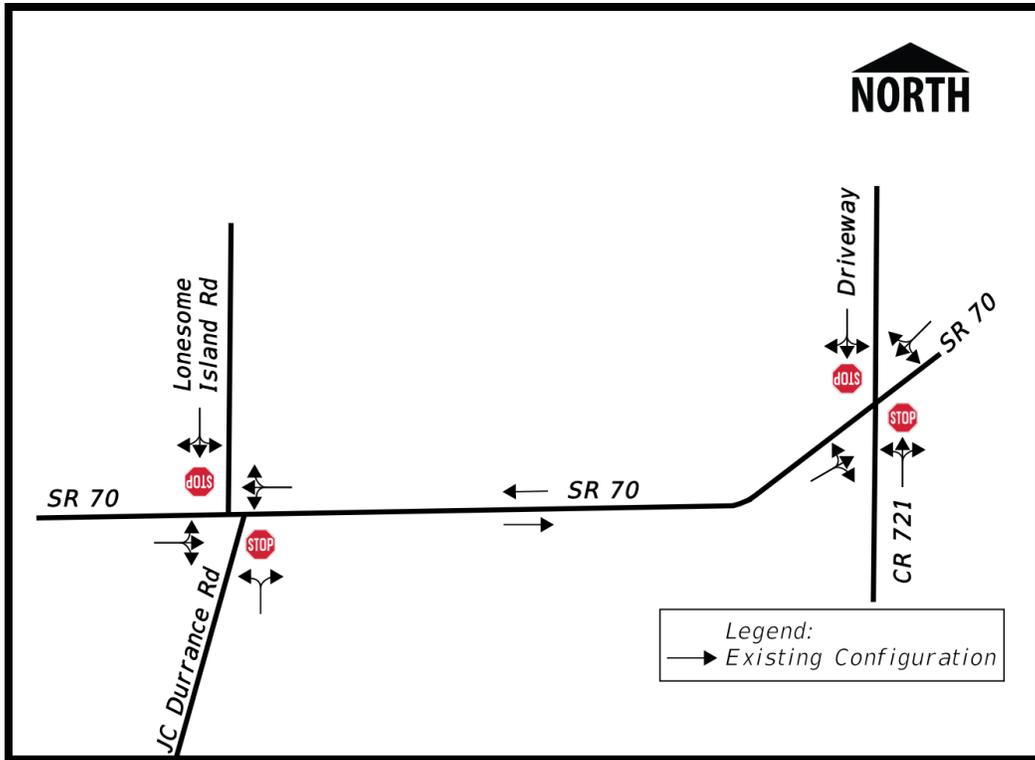


Figure 2-3 | Existing Conditions – Lonesome Island Road/JC Durrance Road at SR 70



CR 721 at SR 70 is a TWSC intersection and consists of two overhead yellow/red flashing signals along each approach. The existing signals are mast arm-mounted and give priority to the eastbound and westbound approaches. All approaches consist of one shared through left-turn right-turn lane. There are no existing pedestrian signals, crosswalks, curb ramps, or sidewalks along any approaches to the intersection. Along the westbound approach, there exists an unmarked shoulder that may serve as a de facto bike lane. Along the eastbound approach, there exists a wide, unmarked paved shoulder that may serve as a de facto right-turn lane. The existing posted speed limit on CR 721 is 45 mph. Additionally, there is an advisory speed of 45 mph along SR 70 through the intersection. The existing lane geometry is shown in **Figure 2-4**.

Figure 2-4 | Existing Conditions – CR 721 at SR 70



2.2 Traffic Counts

The Existing Year 2022 Annual Average Daily Traffic (AADT) volumes from the SR 70 Design Traffic Technical Memorandum (DTTM) prepared by RS&H, Inc. at the direction of FDOT District One in July 2023 are listed in **Table 2-1** and found in **Appendix B**.

Table 2-1 | Existing Year 2022 Annual Average Daily Traffic (AADT)

| Roadway/Segment | 2022 AADT | K % | D % | T % |
|------------------------|-----------|-----|------|------|
| SR 70, West of CR 721 | 5,600 | 9.5 | 55.0 | 32.0 |
| SR 70, East of CR 721 | 5,400 | 9.5 | 58.0 | 25.0 |
| CR 721, South of SR 70 | 1,900 | 9.5 | 70.0 | 15.0 |

Figure 2-5 depicts the Existing Year 2022 AADT volumes on the map. Four-hour manual turning movement counts (TMC) were conducted on Tuesday November 15th, 2022, at both study intersections from 7:00 AM to 9:00 AM and from 4:00 PM to 6:00 PM. The weather was clear during the time the traffic counts were conducted. Appendix C includes a copy of the manual TMC. Figure 2-6 depicts the Existing Year 2022 AM and PM TMC.

Figure 2-5 | SR 70 Existing Year 2022 AADT

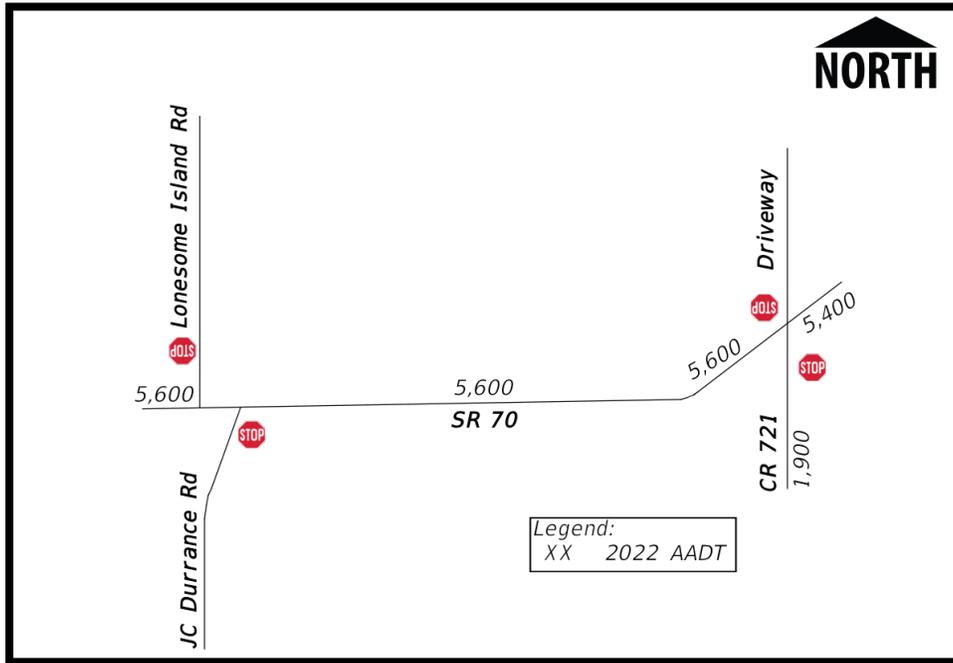
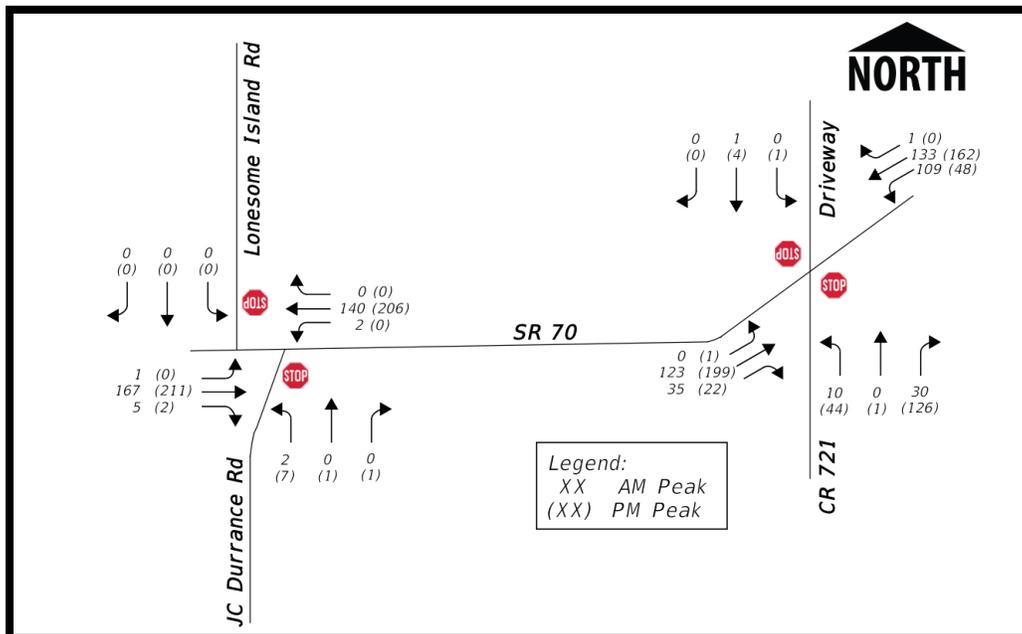


Figure 2-6 | SR 70 Existing Year 2022 TMC



2.3 Design Traffic Factors

Traffic design factors such as K, D, and T factors for this project were derived from Chapter 2.3 of the SR 70 DTTM. See **Table 2-1** for a full list of the design traffic factors that were used for this project. See **Appendix B** for the SR 70 DTTM where these design traffic factors were derived from.

2.3.1 K-Factor

The design hour factor (K-Factor) is the proportion of AADT occurring during the peak hour. Table 2-7 in the SR 70 DTTM provided the K-Factors that were used for this project. A K-Factor of 9.50% was reported for SR 70 and CR 721.

2.3.2 D-Factor

The Directional Distribution Factor (D-Factor) is the proportion of traffic traveling in the peak direction of a roadway segment during the peak hour. Table 2-3 in the SR 70 DTTM provided the D-Factors that were used for this project.

2.3.3 T-Factor

The truck percentage factor (T-Factor) is the percentage of trucks passing through a segment of road daily. Table 2-6 in the SR 70 DTTM provided the T-Factors that were used for this project.

2.4 Existing Year 2022 LOS Analysis

This section presents the analysis results for the existing lane configuration under Existing Year 2022 traffic conditions. An existing traffic operational analysis was conducted for intersections of SR 70 at Lonesome Island Road/JC Durrance Road and at CR 721. The analysis consisted of determining the Level of Service (LOS) and delay at each intersection of SR 70. The Highway Capacity Manual, 6th Edition classifies roadway capacity based on LOS A through F, where LOS A represents a roadway operating below capacity (free-flow conditions with little or no delays) and LOS F suggests a roadway is operating above design capacity (congested traffic with forced flow conditions at very low operating speeds). The analysis was conducted using the latest versions of the Highway Capacity Software 7 (HCS7) and Synchro 11.

The LOS for a TWSC intersection is defined in terms of the average vehicle's delay for each minor-street movement (or shared movement) as well as major-street left-turns. A vehicular delay will also quantify the increase in travel time that the vehicle experiences due to a stop sign or a traffic signal control. This will provide a surrogate measure for driver discomfort and fuel consumption.

Existing Year 2022 LOS analysis was conducted based on the methodology outlined in the Highway Capacity Manual, 6th Edition using Synchro 11. **Appendix D** includes the copies of the Synchro and HCS LOS computer outputs. The existing year intersection Synchro analysis shows that both intersections in this project are currently operating at an overall LOS of A. The existing year arterial HCS analysis shows that the corridor of SR 70 from Lonesome Island Road to CR 721 is also currently operating at a LOS of A. **Table 2-2** shows the overall LOS and delay experienced by both intersections, as well as the individual delay and LOS of each approach of each intersection. **Table 2-3** shows the overall arterial LOS, as well as the vehicle miles-traveled, vehicle-hours delay, and follower density, currently experienced on SR 70. **Figure 2-7** depicts the Existing Year 2022 LOS on the map for AM and PM peak hours.

Table 2-2 | Existing Year 2022 Existing Intersection LOS

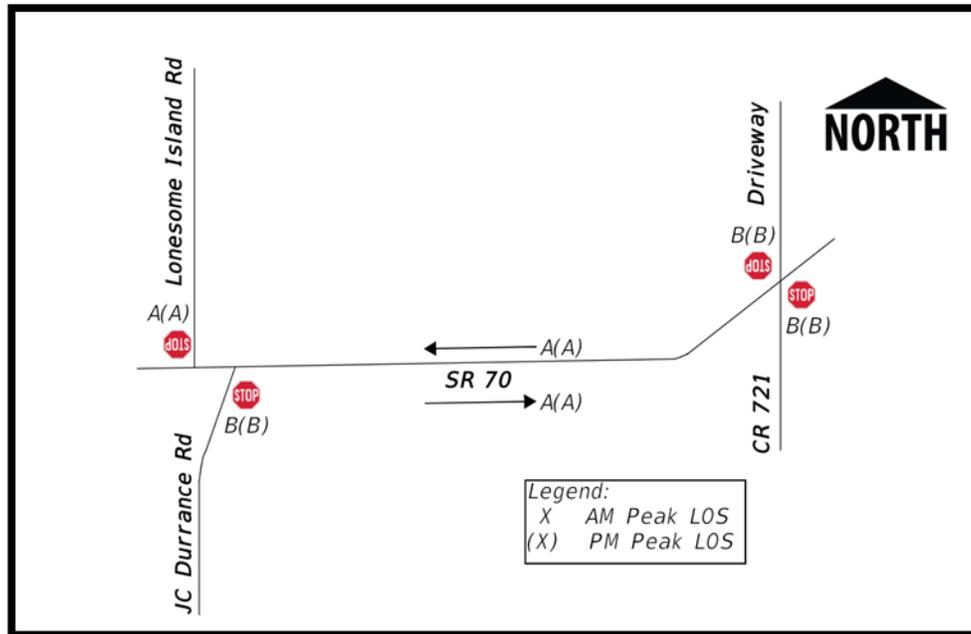
| Intersection | | Peak Hour | LOS | Overall Delay ¹ | NB Delay ¹ / LOS | SB Delay ¹ / LOS | EB Delay ¹ / LOS | WB Delay ¹ / LOS |
|-----------------------------------|---|-----------|-----|----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|
| Lonesome Island Rd/JC Durrance Rd |  | AM | A | 0.1 | 11.1 / B | 0.0 / A | 7.5 / A | 8.2 / A |
| | | PM | A | 0.2 | 11.8 / B | 0.0 / A | 0.0 / A | 0.0 / A |
| CR 721 |  | AM | A | 2.9 | 10.4 / B | 13.8 / B | 0.0 / A | 7.8 / A |
| | | PM | A | 4.2 | 12.4 / B | 13.7 / B | 7.6 / A | 7.8 / A |

¹Delay measured in seconds per vehicle

Table 2-3 | Existing Year 2022 Existing Arterial LOS

| Segment | Peak Hour | LOS | Average Speed (mph) | Segment Travel Time (minutes) | Follower Density (followers/mi/ln) | Percent Followers (%) |
|---|-----------|-----|---------------------|-------------------------------|------------------------------------|-----------------------|
| SR 70 from Lonesome Island Rd to CR 721 | AM | A | 58.3 | 7.92 | 1.7 | 35.8 |
| | PM | A | 58.4 | 7.91 | 1.5 | 34.3 |

Figure 2-7 | SR 70 Existing Year 2022 LOS



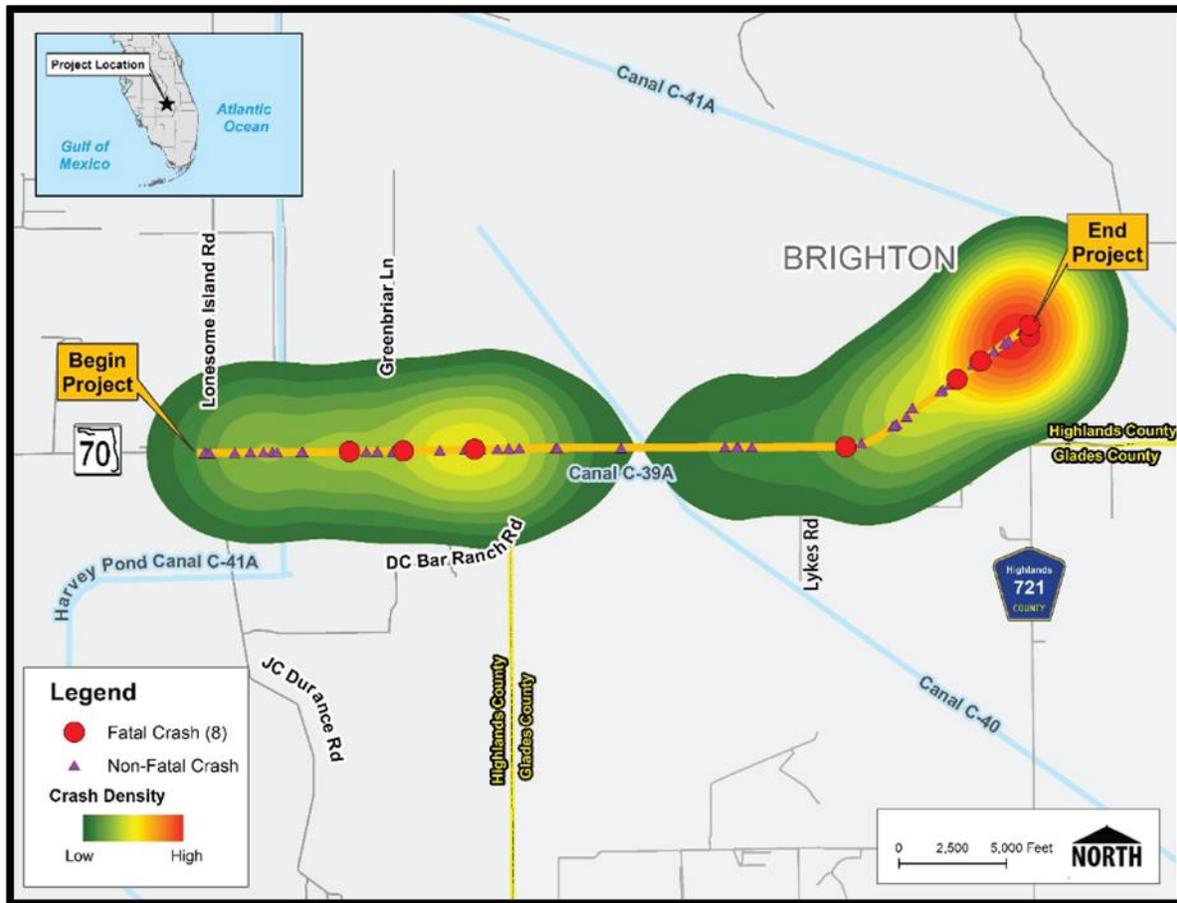
2.5 Historical Crash Data Analysis

A five (5) year historic crash analysis was completed in accordance with Part 2, Chapter 2 of the *PD&E Manual* for years 2018 to 2022. Crash Data for the five-year analysis period was obtained from the University of Florida's Signal Four Analytics database and verified through 2022 at the time the data was pulled. The crash data used for this study is provided in **Appendix E**.

2.5.1 Overall Crash Data along SR 70

The five-year crash analysis (2018-2022) found 84 total crashes (average of 17 crashes per year) for the overall study corridor along SR 70. Most of the reported crashes occur on the segments (68%). The segment from Lykes Road to the Southern Leg of CR 721 had the highest number of crashes (26 crashes). A heat map showing where crashes are concentrated along the study corridor is shown in **Figure 2-8**.

Figure 2-8 | Crash Data Heat Map (2018-2022)



Eight (8) fatal crashes were reported for this roadway during the five-year analysis period. The locations are shown by a red "dot" on **Figure 2-8**.

- A fatal crash reported in 2018 was a guardrail face crash type at the intersection of SR 70 and Greenbriar Lane under dark, not lighted, and dry conditions. Vehicle one was reported as heading east and Vehicle two was reported as heading west. Vehicle one goes out of the lane, hits the

guardrail face, and drives into the opposite direction lane, which causes vehicle one to hit vehicle two head on. The initial cause of this fatal crash was reported as the driver failed to keep in proper lane.

- A second fatal crash reported in 2018 was a fell/jumped from motor vehicle crash type on CR 721 near the intersection under daylight and dry conditions. The initial cause of this fatal crash was reported as running off roadway.
- A fatal crash reported in 2019 was a head on crash type on SR 70 near CR 721 under daylight and dry conditions. Vehicle one was traveling eastbound and vehicle two was traveling westbound. Vehicle one changed lanes to pass low speed traffic, does not notice vehicle two is approaching and hits vehicle two's front left. The initial cause of this fatal crash was reported as improper passing.
- A second fatal crash reported in 2019 was an angle crash type on SR 70 near Partnership Road under dark, not lighted, and dry conditions. There were three (3) vehicles reported to be involved in the crash. Vehicle one was stopped in the westbound lane facing south. Vehicle two was reported to be traveling westbound. Vehicle three came to a stop in the eastbound lane just west of vehicle one. Vehicle two did not see vehicle one stopped in the middle of the road and hit the left side of vehicle one. Vehicle one spins and hits vehicle three. The initial cause of this fatal crash was reported as "other contribution action".
- A fatal crash reported in 2020 was an opposing sideswipe crash about 1600 ft away from Greenbrier Lane under daylight and dry conditions. There were three (3) vehicles reported to be involved in the crash. Vehicle one that was a semi-trailer was reported as heading east, vehicle two was reported heading west going straight ahead and vehicle three was reported heading east going straight ahead. Vehicle one crosses the center lane causing vehicle two to collide with the front of vehicle one. Vehicle two was spinning out of control which hit vehicle three that was driving behind vehicle one. The initial cause of this fatal crash was reported as the driver failed to keep in proper lane.
- A second fatal crash reported in 2020 was an "other" crash type on SR 70 near CR 721 under dusk and dry conditions. Vehicle one was reported traveling eastbound and went off road hitting the southside guardrail. Vehicle one was redirected and traveled across both travel lanes and hit the guardrail on the northside of the roadway. The initial cause of this fatal crash was reported as operating motorized vehicle in careless or negligent manner.
- A fatal crash reported in 2022 was a minor street left turn crash at the intersection of SR 70 and CR 721 under daylight and dry conditions. Vehicle one was reported as stopped at the south leg of the intersection and vehicle two was reported as heading east going straight ahead. Vehicle one was a motorcycle that was stopped at the intersection and drove out in front of Vehicle two to make a left onto SR 70. This caused vehicle two to steer left onto the north grass shoulder. The initial cause of this fatal crash was reported as driver failed to yield right of way.
- A second fatal crash reported in 2022 was an angle crash near the SR 70 and CR 721 intersection under dark, not lighted, and dry conditions. Vehicle one was reported traveling westbound and vehicle two was also traveling westbound approaching vehicle one. Vehicle one attempted to make a U-turn causing vehicle two to hit the left rear side of vehicle one. This causes vehicle one to spin and hit the left side of vehicle two. The initial cause of this fatal crash was reported as an improper turn.

The crash data is also summarized by crash type on **Table 2-4**. The highest-ranking crash types for the study area were reported as opposing sideswipe and guardrail face crashes (both 15%), animal and rear end crashes (both 13%) as the second most prominent crash types, and angle crashes (8%) as the third most prominent crash type. The high percentage of opposing sideswipe collisions could be attributed to the vehicles wishing to pass a low-speed traffic and not seeing oncoming traffic. Guardrail face crashes could be attributed to distracted drivers, loss of control, and many other driver related causes. The animal crashes could be attributed to the surrounding area being rural and the ditches/canals located parallel to the roadway could potentially be attracting animal crossings. The rear end crashes are mainly due to operating the vehicle in a careless or negligent behavior. The most common types of crashes that can attributed to the current layout of the roadway are animal, guardrail face, head on, left leaving, and opposing sideswipe. These 5 types of crashes made up 49% of the crashes that occurred along SR 70 in the past 5 years. The likelihood and occurrence of these types of crashes can be reduced by widening the road from two lanes to four lanes, separating opposing directions of travel with a median, and restricting side streets to right turn only movements onto SR 70.

Table 2-4 | Crash Type Summary Along SR 70

| Crash Type | Year | | | | | Total | Percentage |
|-----------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-------------|
| | 2018 | 2019 | 2020 | 2021 | 2022 | | |
| Animal | 2 | 3 | 1 | 4 | 1 | 11 | 13% |
| Cargo/Equipment Loss or Shift | 0 | 0 | 0 | 0 | 1 | 1 | 1% |
| Ditch | 2 | 0 | 1 | 0 | 0 | 3 | 4% |
| Fell/Jumped from Motor Vehicle | 1 | 0 | 0 | 0 | 0 | 1 | 1% |
| Guardrail Face | 4 | 2 | 3 | 2 | 2 | 13 | 15% |
| Angle | 2 | 3 | 1 | 0 | 1 | 7 | 8% |
| Head On | 0 | 1 | 0 | 1 | 1 | 3 | 4% |
| Left Leaving | 0 | 0 | 0 | 1 | 1 | 2 | 2% |
| Opposing Sideswipe | 1 | 4 | 4 | 3 | 1 | 13 | 15% |
| Other | 0 | 0 | 2 | 1 | 0 | 3 | 4% |
| Rear End | 4 | 2 | 2 | 2 | 1 | 11 | 13% |
| Same Direction Sideswipe | 0 | 0 | 0 | 2 | 0 | 2 | 2% |
| Single Vehicle | 0 | 0 | 0 | 1 | 0 | 1 | 1% |
| Unknown | 0 | 0 | 0 | 1 | 0 | 1 | 1% |
| Other Non-Collision | 0 | 1 | 1 | 0 | 1 | 3 | 4% |
| Other Non-Fixed Object | 1 | 1 | 0 | 1 | 2 | 5 | 6% |
| Overturn/Rollover | 2 | 0 | 0 | 0 | 0 | 2 | 2% |
| Struck by Falling, Shifting Cargo | 0 | 1 | 0 | 0 | 0 | 1 | 1% |
| Thrown or Falling Object | 0 | 0 | 0 | 0 | 1 | 1 | 1% |
| Total | 19 | 18 | 15 | 19 | 13 | 84 | 100% |

There were no pedestrian or bike crashes during the crash analysis years (2018-2022). The average percentage of wet and dark crashes for the five-year period in the study area is 9.5% and 38.1%, respectively. The number of wet pavement crashes is below the statewide average of 11.6% from data as published on page 36 in the Florida Highway Safety and Motor Vehicles *Traffic Crash Facts Annual Report 2022* (provided in **Appendix E**). The percentage of dark lighting condition crashes is above the statewide average of 24.5% from data as published on page 37 in the Florida Highway Safety and Motor Vehicles *Traffic Crash Facts Annual Report 2022*. A crash summary for SR 70 for the five-year analysis period is shown in **Table 2-5**.

Table 2-5 | Summary of Crashes Along SR 70

| | Year | | | | | Total |
|-------------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|
| | 2018 | 2019 | 2020 | 2021 | 2022 | |
| No. of Fatal Crashes | 2 | 2 | 2 | 0 | 2 | 8 |
| No. of Serious Injury Crashes | 1 | 2 | 0 | 1 | 2 | 6 |
| No. of Injury Crashes | 4 | 3 | 3 | 3 | 3 | 16 |
| No. of Property Damage Only Crashes | 12 | 11 | 10 | 15 | 6 | 54 |
| Total Crashes | 19 | 18 | 15 | 19 | 13 | 84 |
| Pedestrian Crashes | 0 | 0 | 0 | 0 | 0 | 0 |
| Bike Crashes | 0 | 0 | 0 | 0 | 0 | 0 |
| Wet Surfaces Crashes | 2 | 2 | 4 | 0 | 0 | 8 |
| Dark Crashes | 6 | 10 | 2 | 9 | 5 | 32 |

2.5.2 Intersection and Segment Crash Data of SR 70

A five-year crash analysis (2018-2022) for the intersections and segments of SR 70 was completed. The top locations for crashes are the segment from Lykes Road to the Southern Leg of CR 721 (31%), the southern leg of CR 721 intersection (23%), and the segment from Lonesome Island Road to Greenbrier Lane (15%). Rear end crash types accounted for a majority of the crashes at intersections and segments. The high percentage of rear end collisions could be attributed to the high levels of congestion occurring along the corridor. **Table 2-6** provides a breakdown of intersection and segment crashes along SR 70.

Table 2-6 | Crash Summary for Segments and Intersections Along SR 70

| Segment | Crashes | Fatalities | Highest Crash Type | % of Crash Type | Dark Crashes | % of Total Crashes |
|-------------------------------------|---------|------------|--------------------|-----------------|--------------|--------------------|
| Lonesome Island Rd to Greenbrier Ln | 13 | 1 | Guardrail Face | 31% | 2 | 15% |
| Greenbrier Ln to DC Bar Ranch Rd | 10 | 2 | Opposing Sideswipe | 40% | 3 | 12% |
| DC Bar Ranch Rd to Lykes Rd | 8 | 0 | N/A | N/A | 2 | 10% |
| Lykes Rd to Southern Leg of CR 721 | 26 | 3 | Opposing Sideswipe | 17% | 13 | 31% |
| Intersection | Crashes | Fatalities | Highest Crash Type | % of Crash Type | Dark Crashes | % of Total Crashes |
| Lonesome Island Rd | 0 | 0 | N/A | N/A | N/A | 0% |
| JC Durrance Rd | 1 | 0 | Rear End | 100% | 0 | 1% |
| Greenbrier Ln | 4 | 0 | Animal | 50% | 2 | 5% |
| DC Bar Ranch Rd (DW access road) | 3 | 0 | N/A | N/A | 3 | 3% |
| Lykes Rd | 0 | 0 | N/A | N/A | N/A | 0% |
| Southern Leg of CR 721 | 19 | 2 | Rear End | 21% | 7 | 23% |

2.5.3 Crash Rates

Crash rates for the study area were calculated in million vehicle miles traveled (MVMT) for segments and million entering vehicles (MEV) for intersections. Crash rates were calculated based on the number of crashes that occurred within the five-year crash analysis period, length of roadway and annual average daily traffic volumes. The following equations were used to develop the crash rates for this study:

$$\text{Crash Rate for Segment} = \frac{\text{Total Number of Crashes} \times 1,000,000}{\text{AADT} \times 365 \times \text{Number of Years} \times \text{Length of Roadway Segment}}$$

$$\text{Crash Rate for Intersection} = \frac{\text{Total Number of Crashes} \times 1,000,000}{\text{Total Intersection Entering Volume Per Day} \times \text{Number of Years} \times 365}$$

The crash rates calculated for the SR 70 study are shown in **Table 2-7** and **Table 2-8** which includes five (5) segments and six (6) intersections crash rates. This crash rate on the segment Lykes Road to the Southern Leg of CR 721 was the highest with a rate of 1.077 crashes per MVMT. The Southern Leg of CR 721 intersection exhibited the highest intersection crash rate with a rate of 1.589 crashes per MEV. The high number of crashes on the segment is due to vehicles wishing to pass low speed vehicles and not seeing the oncoming traffic. This could be fixed with widening improvements for the corridor to eliminate vehicles crossing into opposing traffic to get around a slow truck or vehicle.

Table 2-7 | Crash Rates for Segments

| Segment | | Crashes | Length (mi) | 2022 AADT | Crash Rate (MVMT) | Statewide Average ⁽¹⁾ | Above Statewide Average? |
|--------------------|------------------------|---------|-------------|-----------|-------------------|----------------------------------|--------------------------|
| From | To | | | | | | |
| Lonesome Island Rd | Greenbrier Ln | 13 | 1.72 | 5,600 | 0.739 | 0.802 | NO |
| Greenbrier Ln | DC Bar Ranch Rd | 10 | 1.00 | 5,600 | 0.977 | 0.802 | YES |
| DC Bar Ranch Rd | Lykes Rd | 8 | 2.57 | 5,600 | 0.304 | 0.802 | NO |
| Lykes Rd | Southern Leg of CR 721 | 26 | 2.36 | 5,600 | 1.077 | 0.802 | YES |

(1) Statewide rates from FDOT Safety Office for years 2015-2019

(1) Note: Crashes reported to occur within intersection turn lanes were extracted out of the segments.

Table 2-8 | Crash Rates for Intersections

| SR 70 Intersection | Crashes | Entering Volume | Crash Rate (MEV) | Statewide Average ⁽¹⁾ | Above Statewide Average? |
|------------------------|---------|-----------------|------------------|----------------------------------|--------------------------|
| Lonesome Island Rd | 0 | 7,875 | 0.000 | 0.201 | NO |
| JC Durrance Rd | 1 | 7,900 | 0.097 | 0.201 | NO |
| Greenbrier Ln | 4 | 7,875 | 0.388 | 0.201 | YES |
| DC Bar Ranch Rd | 3 | 7,875 | 0.291 | 0.201 | YES |
| Lykes Rd | 0 | 7,875 | 0.000 | 0.201 | NO |
| Southern Leg of CR 721 | 19 | 10,500 | 1.589 | 0.258 | YES |

(2) Statewide rates from FDOT Safety Office for years 2015-2019

Calculating one average crash rate for the corridor that includes the intersection crashes with an average AADT yields a crash rate of 1.073 MVMT. This overall crash rate is 34% higher than the statewide average of 0.802 MVMT for rural 2-3 lanes two-way undivided roadways.

Section 3 Signal Warrant Analysis

A signal warrant analysis was performed at the intersection of SR 70 and CR 721 to evaluate the need to convert the intersection from TWSC to a signalized intersection based on Opening Year 2032 conditions. The FDOT traffic signal warrant analysis sheet was used to evaluate this intersection. This analysis sheet breaks down the criteria that could justify the placement of a traffic signal at an intersection into 9 different warrants. None of the nine signal warrants were satisfied. As a result, the build scenario will only analyze unsignalized options for the intersection of SR 70 and CR 721. **Appendix F** includes the signal warrant analysis for SR 70 and CR 721.

Section 4 Future Traffic Forecast

Forecasted AADTs and directional design hour volumes were developed for the Design Year 2052 for the No-Build and Build scenarios. Future AADTs were developed using growth rates for the project area provided by the SR 70 DTTM. These growth rates were used to calculate Opening Year 2032 and Design Year 2052 AADTs for both No-Build and Build scenarios.

4.1 Recommended Annual Growth Rate

For traffic projection purposes, this study used the individual annual growth rates of each roadway segment of the project found in Table 3-1 of the SR 70 DTTM prepared by RS&H, Inc. at the direction of FDOT District One in July 2023. The full SR 70 DTTM can be found in **Appendix B**. The recommended annual growth rates used for each roadway segment in the development of future year AADTs can be found in **Table 4-1**.

Table 4-1 | Annual Growth Rate Calculation

| Roadway | Segment | Annual No-Build Growth Rate % Used | Annual Build Growth Rate % Used |
|---------|--------------------------------------|------------------------------------|---------------------------------|
| SR 70 | West of JC Durrance Rd | 2.5% | 4.0% |
| | From JC Durrance Rd to Greenbrier Ln | 2.5% | 4.0% |
| | From Greenbrier Ln to CR 721 | 2.5% | 4.0% |
| | East of CR 721 | 3.0% | 4.5% |
| CR 721 | South of SR 70 | 3.0% | 4.0% |

4.2 Evacuation Impact Analysis

SR 70 is one of the major designated east-west evacuation routes in Highlands County and across the state of Florida. As the population of the county continues to increase, concerns about the ability of SR 70 to handle the capacity of emergency evacuations in the surrounding areas have begun to arise. Current evacuation models for Highlands County project an average clearance time for shelter evacuations of around 12.5 hours, while out-of-county evacuation clearance times range from 16.5 hours to 40.5 hours depending on the severity of evacuation being measured. See **Appendix G** for a map of the major evacuation routes in Highlands County, as well as Transportation Interface for Modeling Evacuations (TIME) reports for the existing statistics for all evacuation scenarios in Highlands County prepared by the Statewide Regional Evacuation Study Program (SRESP). By widening the stretch of SR 70 from Lonesome Island Road to CR 721 from two lanes to four lanes, the capacity of the road will increase, allowing for lower evacuation clearance times in emergency situations.

Section 5 Future Traffic Demand

This section depicts the traffic volumes for future years from the SR 70 DTTM.

5.1 Future Year Daily Traffic Volumes

The traffic AADT volumes have been rounded according to the 2019 FDOT *Project Traffic Forecasting Handbook*. **Table 5-1** shows the calculations for Design Year 2052 No-Build AADT based on the recommended annual growth rate for each roadway segment. **Table 5-2** provides the AADT values of the Existing Year 2022, Opening Year 2032, and Design Year 2052 No-Build scenarios. **Figure 5-1** shows Design Year 2052 No-Build AADT values on the project map.

Table 5-1 | Design Year 2052 No-Build AADT Calculation

| Roadway | Segment | 2022 AADT | Annual Growth Rate % Used | 2052 AADT | 2052 AADT (rounded) |
|---------|----------------|-----------|---------------------------|-----------|---------------------|
| SR 70 | West of CR 721 | 5,600 | 2.5% | 9,800 | 9,800 |
| | East of CR 721 | 5,400 | 3.0% | 10,260 | 10,500 |
| CR 721 | South of SR 70 | 1,900 | 3.0% | 3,610 | 3,600 |

Table 5-2 | No-Build AADT Summary

| Roadway | Segment | 2022 AADT | 2032 AADT | 2052 AADT |
|---------|----------------|-----------|-----------|-----------|
| SR 70 | West of CR 721 | 5,600 | 7,000 | 9,800 |
| | East of CR 721 | 5,400 | 7,000 | 10,500 |
| CR 721 | South of SR 70 | 1,900 | 2,500 | 3,600 |

Figure 5-1 | SR 70 Design Year 2052 No-Build AADT

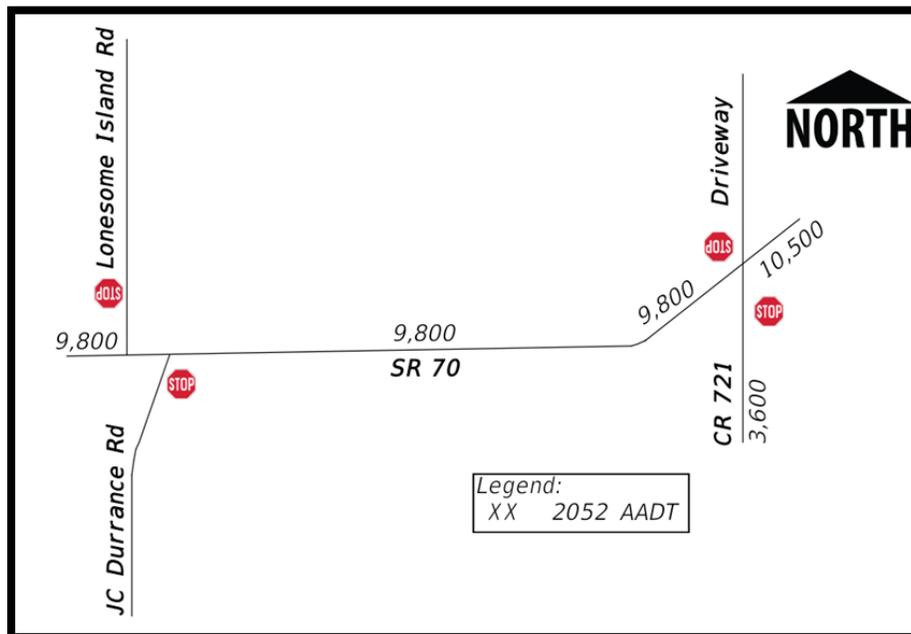


Table 5-3 shows the calculations for Design Year 2052 Build AADT values based on the recommended annual growth rate for each roadway segment. **Table 5-4** provides the AADT values of the Existing Year 2022, Opening Year 2032, and Design Year 2052 Build scenarios. **Figure 5-2** shows Opening Year 2032 Build AADT values on the project map. **Figure 5-3** shows Design Year 2052 Build AADT values on the project map.

Table 5-3 | Design Year 2052 Build AADT Calculation

| Roadway | Segment | 2022 AADT | Annual Growth Rate % Used | 2052 AADT | 2052 AADT (rounded) |
|---------|----------------|-----------|---------------------------|-----------|---------------------|
| SR 70 | West of CR 721 | 5,600 | 4.0% | 12,320 | 12,500 |
| | East of CR 721 | 5,400 | 4.5% | 12,690 | 12,500 |
| CR 721 | South of SR 70 | 1,900 | 4.0% | 4,180 | 4,200 |

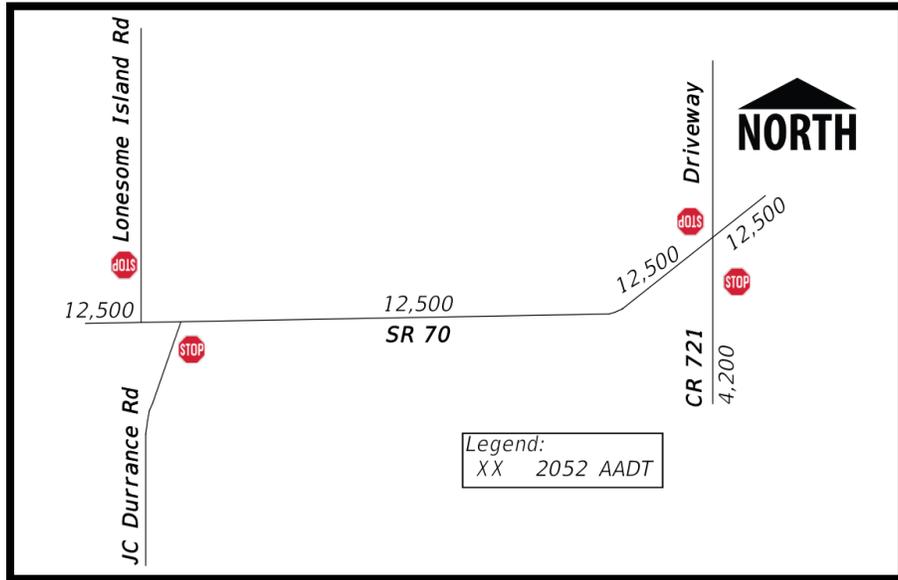
Table 5-4 | Build AADT Summary

| Roadway | Segment | 2022 AADT | 2032 AADT | 2052 AADT |
|---------|----------------|-----------|-----------|-----------|
| SR 70 | West of CR 721 | 5,600 | 7,800 | 12,500 |
| | East of CR 721 | 5,400 | 7,800 | 12,500 |
| CR 721 | South of SR 70 | 1,900 | 2,700 | 4,200 |

Figure 5-2 | SR 70 Opening Year 2032 Build AADT



Figure 5-3 | SR 70 Design Year 2052 Build AADT



5.2 Future Year Turning Movement Volumes

Figure 5-4 depicts the AM and PM turning movement volumes for the Design Year 2052 No-Build scenario from the SR 70 DTTM. Figure 5-5 depicts the AM and PM turning movement volumes for the Design Year 2032 Build scenario from the SR 70 DTTM. Figure 5-6 depicts the AM and PM turning movement volumes for the Design Year 2052 Build scenario from the SR 70 DTTM.

Figure 5-4 | SR 70 Design Year 2052 No-Build Turning Movement Volumes

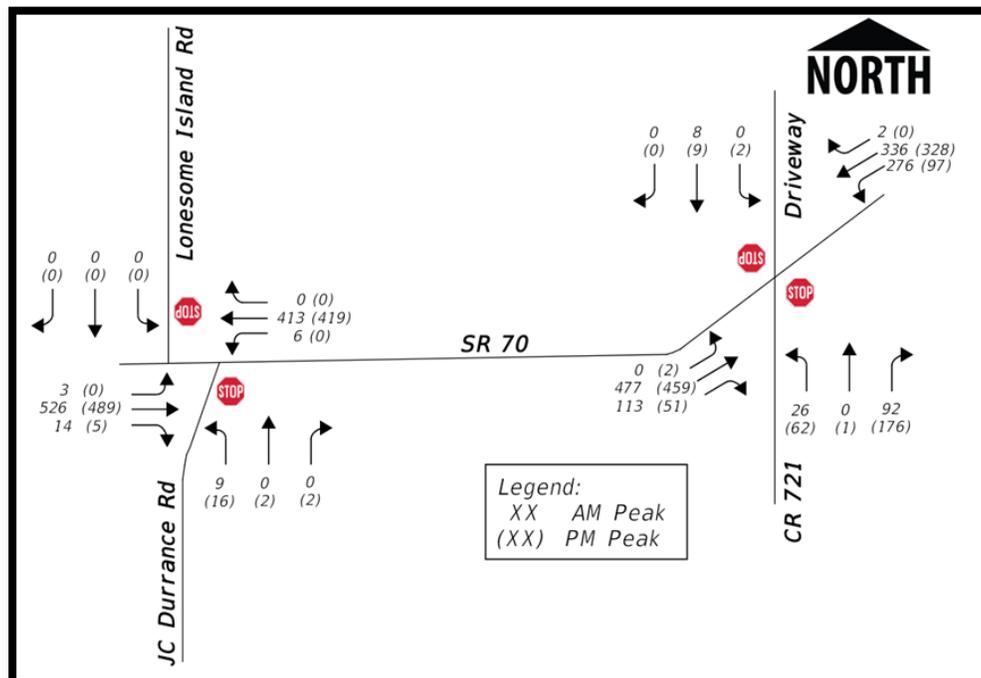


Figure 5-5 | SR 70 Opening Year 2032 Build Turning Movement Volumes

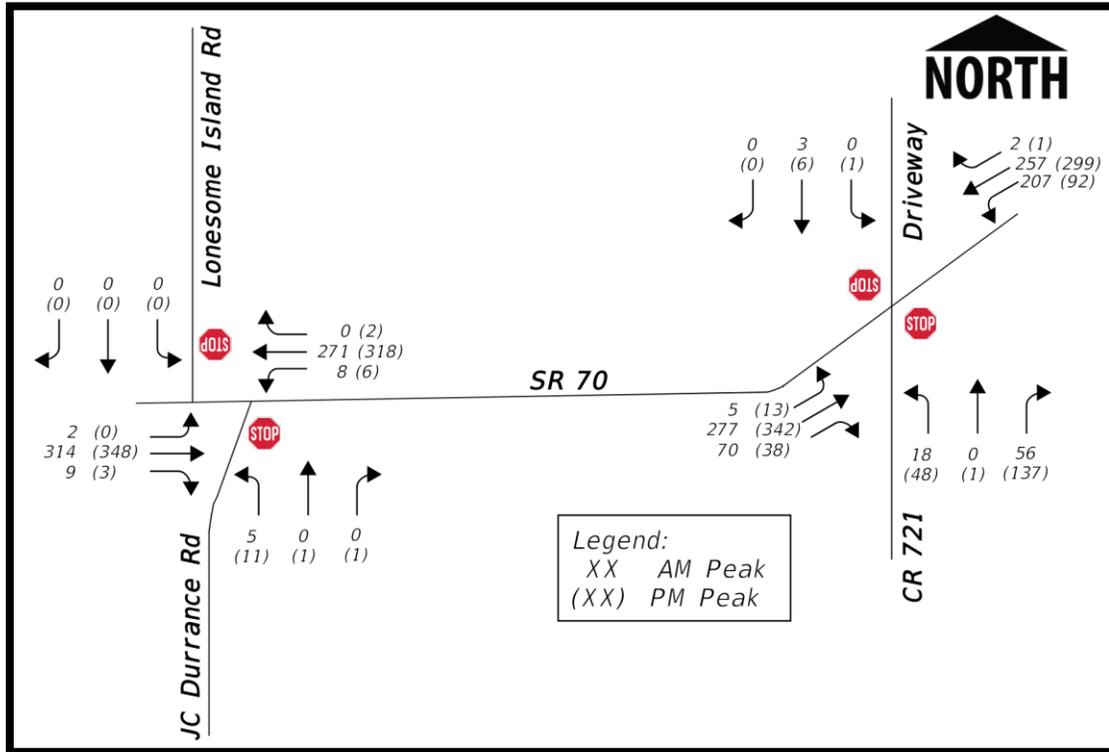
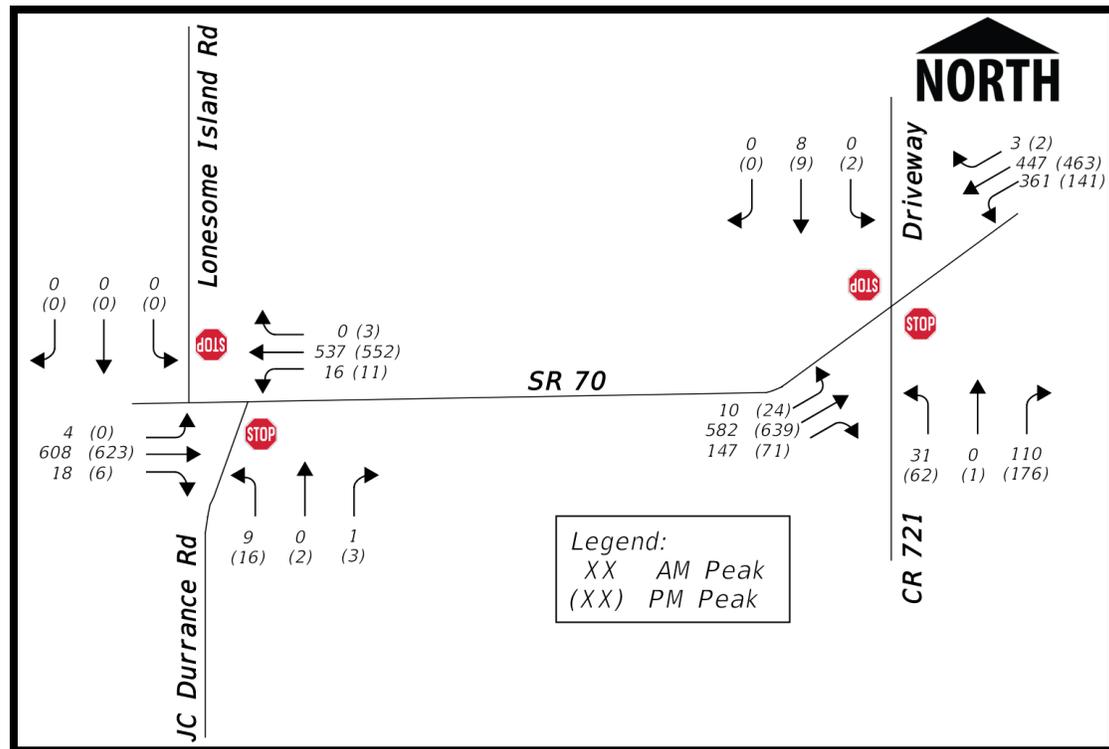


Figure 5-6 | SR 70 Design Year 2052 Build Turning Movement Volumes



Section 6 Capacity LOS Analysis

6.1 No-Build Analysis

Design Year 2052 LOS analysis was conducted based on the methodology outlined in the *Highway Capacity Manual, 6th Edition* using Synchro 11. **Appendix H** includes the copies of the Synchro, SIDRA, and HCS LOS computer outputs for future volumes. **Table 6-1** shows the overall LOS and Delay experienced by both intersections, as well as the individual delay and LOS of each approach of each intersection for the AM and PM peak hours for the Design Year 2052 No-Build scenario. **Table 6-2** shows the AM and PM Arterial LOS expected in the Design Year 2052 No-Build scenario. **Figure 6-1** depicts the No-Build Design Year 2052 LOS on the map.

Table 6-1 | Design Year 2052 No-Build Intersection LOS

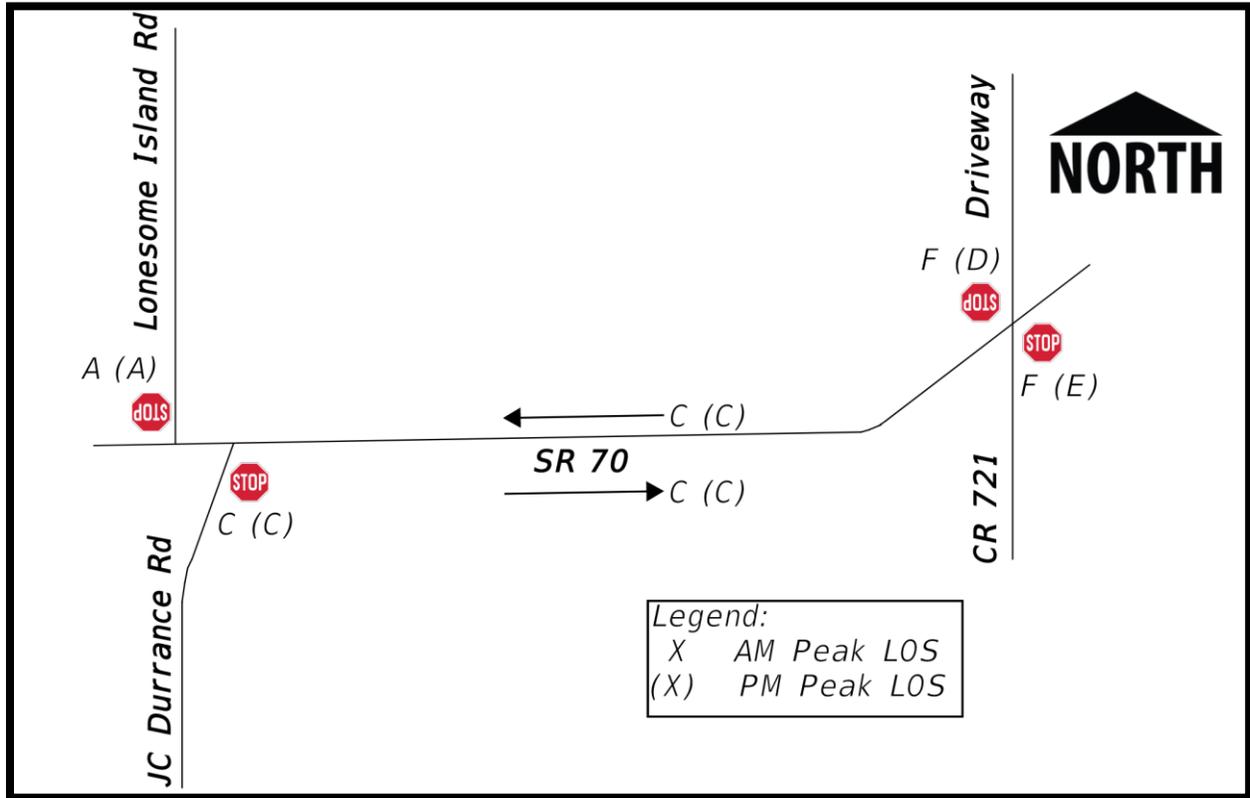
| Intersection | | Peak Hour | LOS | Overall Delay ¹ | NB Delay ¹ / LOS | SB Delay ¹ / LOS | EB Delay ¹ / LOS | WB Delay ¹ / LOS |
|-----------------------------------|---|-----------|-----|----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|
| Lonesome Island Rd/JC Durrance Rd |  | AM | A | 0.3 | 22.5 / C | 0.0 / A | 8.4 / A | 8.9 / A |
| | | PM | A | 0.4 | 20.4 / C | 0.0 / A | 0.0 / A | 0.0 / A |
| CR 721 |  | AM | A | 8.1 | 61.6 / F | 64.8 / F | 0.0 / A | 10.8 / B |
| | | PM | A | 9.3 | 41.4 / E | 27.6 / D | 8.2 / A | 9.1 / A |

¹Delay measured in seconds per vehicle

Table 6-2 | Design Year 2052 No-Build Arterial LOS

| Segment | Peak Hour | LOS | Average Speed (mph) | Segment Travel Time (minutes) | Follower Density (followers/mi/ln) | Percent Followers (%) |
|---|-----------|-----|---------------------|-------------------------------|------------------------------------|-----------------------|
| SR 70 from Lonesome Island Rd to CR 721 | AM | C | 57.3 | 8.05 | 6.8 | 60.0 |
| | PM | C | 57.0 | 8.09 | 5.1 | 54.3 |

Figure 6-1 | SR 70 Design Year 2052 No-Build LOS



6.2 Proposed Geometry

The Build Alternative geometry consists of widening SR 70 from a two-lane undivided roadway to a four-lane divided roadway with a median. An Intersection Control Evaluation (ICE) was performed to determine the highest operation and safety rated intersection configuration and can be found in **Appendix I**. The unsignalized intersection configuration options that were analyzed include the No-Build TWSC, Restricted Crossing U-Turn (RCUT) and Roundabout. The Design Year 2052 AM and PM peak hour intersection LOS values as well as the LOS of each approach to the intersection was calculated, recorded, and compared. **Table 6-3** shows the LOS results for each intersection configuration that was analyzed. Full Synchro and SIDRA LOS outputs for each intersection build can be found in **Appendix H**.

Table 6-3 | SR 70 at CR 721 Design Year 2052 Intersection Configuration LOS Comparison

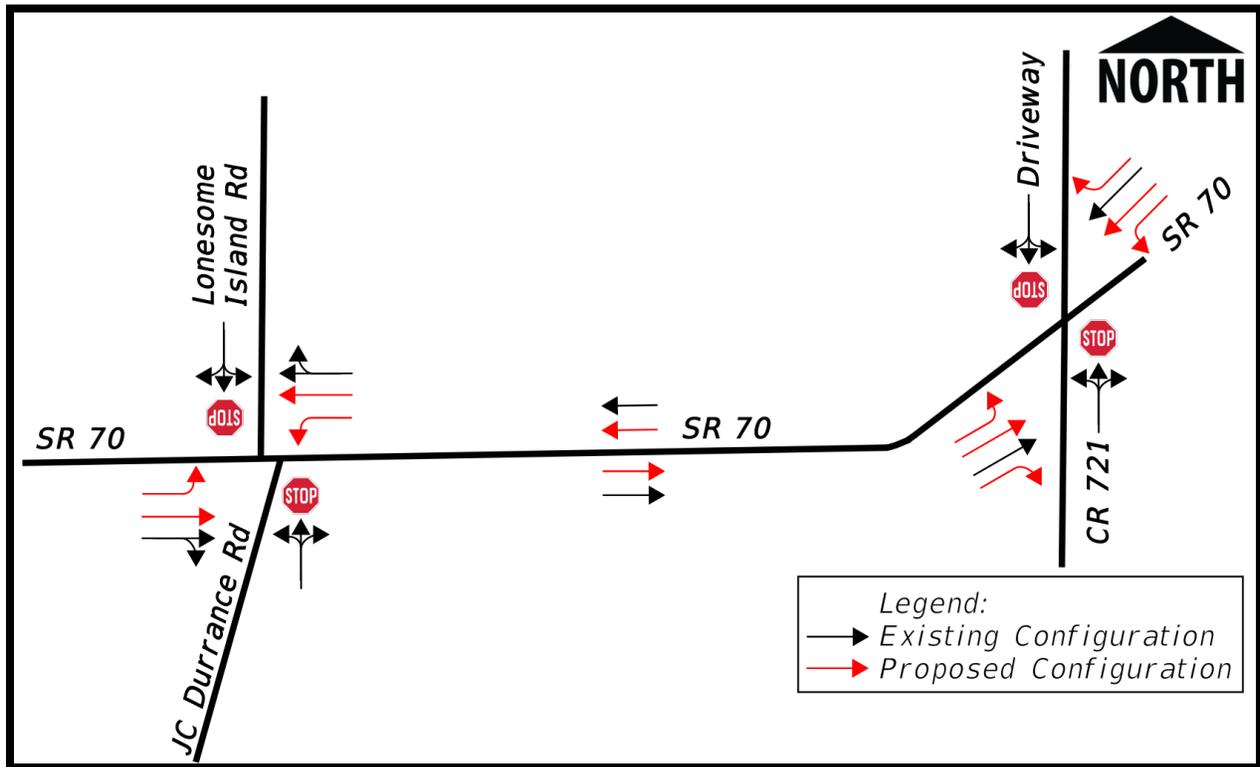
| Intersection Configuration | Peak Hour | LOS | Overall Delay ¹ | NB Delay ¹ / LOS | SB Delay ¹ / LOS | EB Delay ¹ / LOS | WB Delay ¹ / LOS |
|----------------------------|-----------|-----|----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|
| No-Build TWSC | AM | D | 29.0 | >300 / F | 168.6 / F | 8.7 / A | 14.1 / B |
| | PM | C | 19.5 | 120.0 / F | 53.1 / F | 8.8 / A | 10.6 / B |
| Restricted Crossing U-Turn | AM | A | 4.1 | 11.9 / B | 9.7 / A | 8.7 / A | 14.1 / B |
| | PM | A | 3.0 | 13.7 / B | 9.8 / A | 8.8 / A | 10.6 / B |
| Roundabout | AM | A | 8.8 | 8.2 / A | 7.4 / A | 12.0 / B | 6.1 / A |
| | PM | A | 7.5 | 12.2 / B | 6.0 / A | 7.5 / A | 5.7 / A |

¹Delay measured in seconds per vehicle

Although the unsignalized RCUT intersection provides the best performing intersection and approach LOS, the preference is for the intersections to remain fully open with the TWSC intersection configuration.

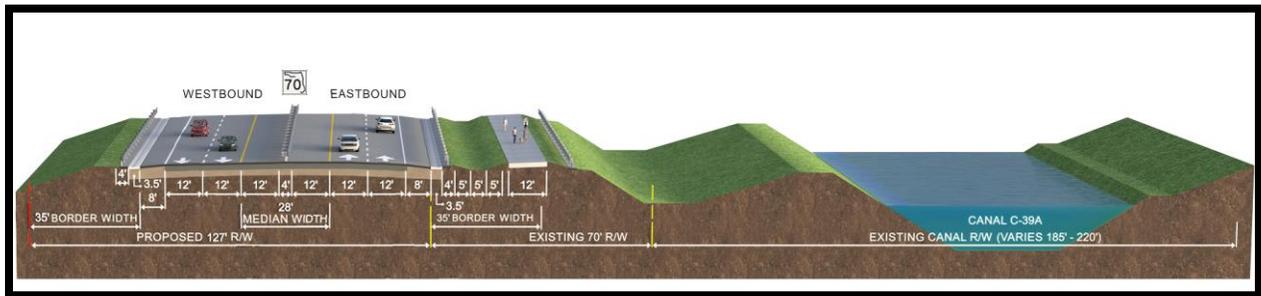
Figure 6-2 shows the proposed lane geometry for SR 70 and its intersections. Improvements to the intersections of SR 70 at Lonesome Island Rd/JC Durrance Rd and SR 70 at CR 721 consist of adding dedicated eastbound and westbound left turn lanes. Although volumes are low, exclusive left-turn lanes are recommended along SR 70 to improve safety and reduce the risk of rear-end crashes. The left-turn lanes will not require any additional widening since the storage will be within the proposed median.

Figure 6-2 | SR 70 Proposed Lane Geometry



The proposed typical sections show widening SR 70 to a four-lane divided rural roadway. There will be two 12-ft travel lanes in each direction, with outside shoulders. Throughout the corridor, a 12-ft shared use path is proposed along the south side of the road. The proposed ROW varies along the corridor, and is a minimum of an additional 60 ft. There are three proposed typical sections within the study limits. The proposed Typical Section One shows widening SR 70 to a four-lane divided rural roadway with a 4-ft guardrail. There will be two 12-ft travel lanes in each direction, with outside shoulders that are approximately 8-ft wide (3.5-ft paved). Proposed Typical Section One is from Lonesome Island Road to Indian Prairie Canal C-40 and is provided as **Figure 6-3**.

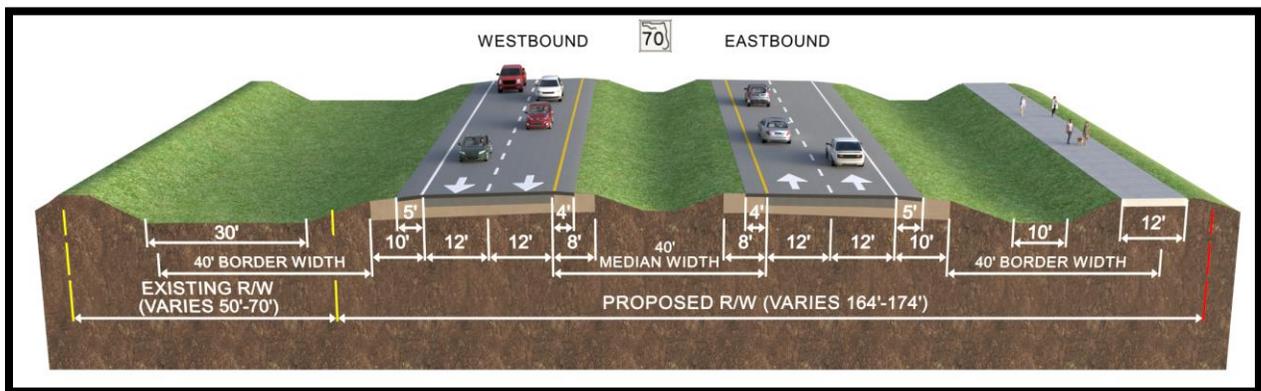
Figure 6-3 | SR 70 – Proposed Roadway Typical Section One



From Lonesome Island Road to Indian Prairie Canal C-40

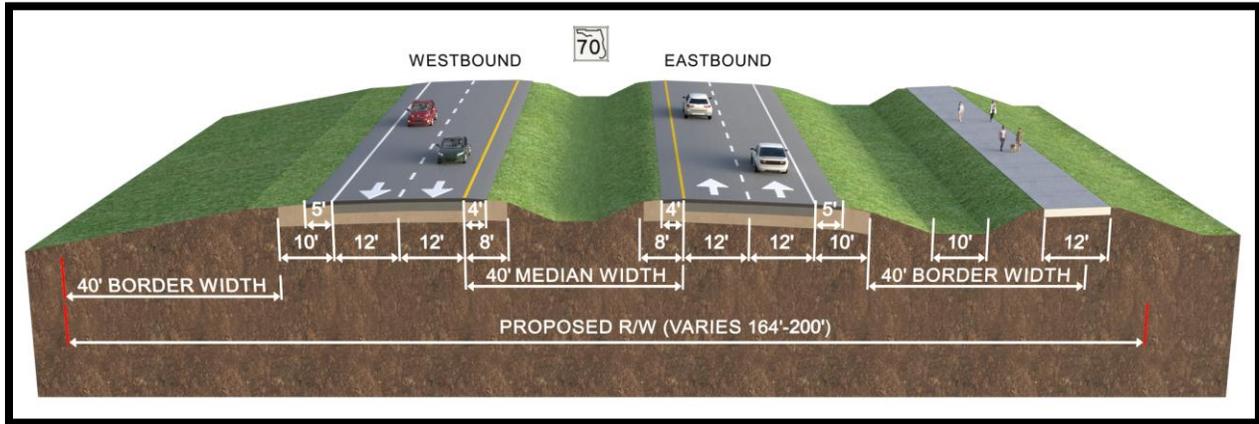
The proposed Typical Section Two and Three show widening SR 70 to a four-lane divided rural roadway with a 40-ft median. There will be two 12-ft travel lanes in each direction, with outside shoulders that are approximately 10-ft wide (5-ft paved). Proposed Typical Section Two is from Indian Prairie Canal C-40 to West of CR 721 (Southern Leg) and is provided as **Figure 6-4**. Proposed Typical Section Three is from West of CR 721 (Southern Leg) to CR 721 (Southern Leg) and is provided as **Figure 6-5**.

Figure 6-4 | SR 70 – Proposed Roadway Typical Section Two



From East of Indian Prairie Canal C-40 to West of CR 721

Figure 6-5 | SR 70 – Proposed Roadway Typical Section Three



From West of CR 721 to CR 721

6.3 Build Analysis

Table 6-4 shows the overall LOS and Delay expected at both intersections, as well as the individual delay and LOS of each approach of each intersection for the AM and PM peak hours for the Opening Year 2032 Build scenario. Table 6-5 shows the Arterial LOS, average speed, and density expected along SR 70 for the Opening Year 2032 Build scenario. Figure 6-6 depicts the Opening Year 2032 Build LOS on the map.

Table 6-4 | Opening Year 2032 Build LOS

| Intersection | Peak Hour | LOS | Overall Delay ¹ | NB Delay ¹ / LOS | SB Delay ¹ / LOS | EB Delay ¹ / LOS | WB Delay ¹ / LOS |
|-----------------------------------|-----------|-----|----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|
| Lonesome Island Rd/JC Durrance Rd | AM | A | 0.2 | 13.0 / B | 0.0 / A | 8.1 / A | 8.2 / A |
| | PM | A | 0.3 | 13.8 / B | 0.0 / A | 0.0 / A | 8.3 / A |
| CR 721 | AM | A | 3.4 | 14.6 / B | 25.9 / D | 8.0 / A | 9.0 / A |
| | PM | A | 4.1 | 16.1 / C | 20.5 / C | 8.2 / A | 8.7 / A |

¹Delay measured in seconds per vehicle

Table 6-5 | Opening Year 2032 Build Arterial LOS

| Segment | Peak Hour | LOS | Average Speed (mph) | Density (pc/mi/ln) |
|---|-----------|-----|---------------------|--------------------|
| SR 70 from Lonesome Island Rd to CR 721 | AM | A | 65.0 | 4.3 |
| | PM | A | 65.0 | 3.6 |

Figure 6-6 | SR 70 Opening Year 2032 Build LOS

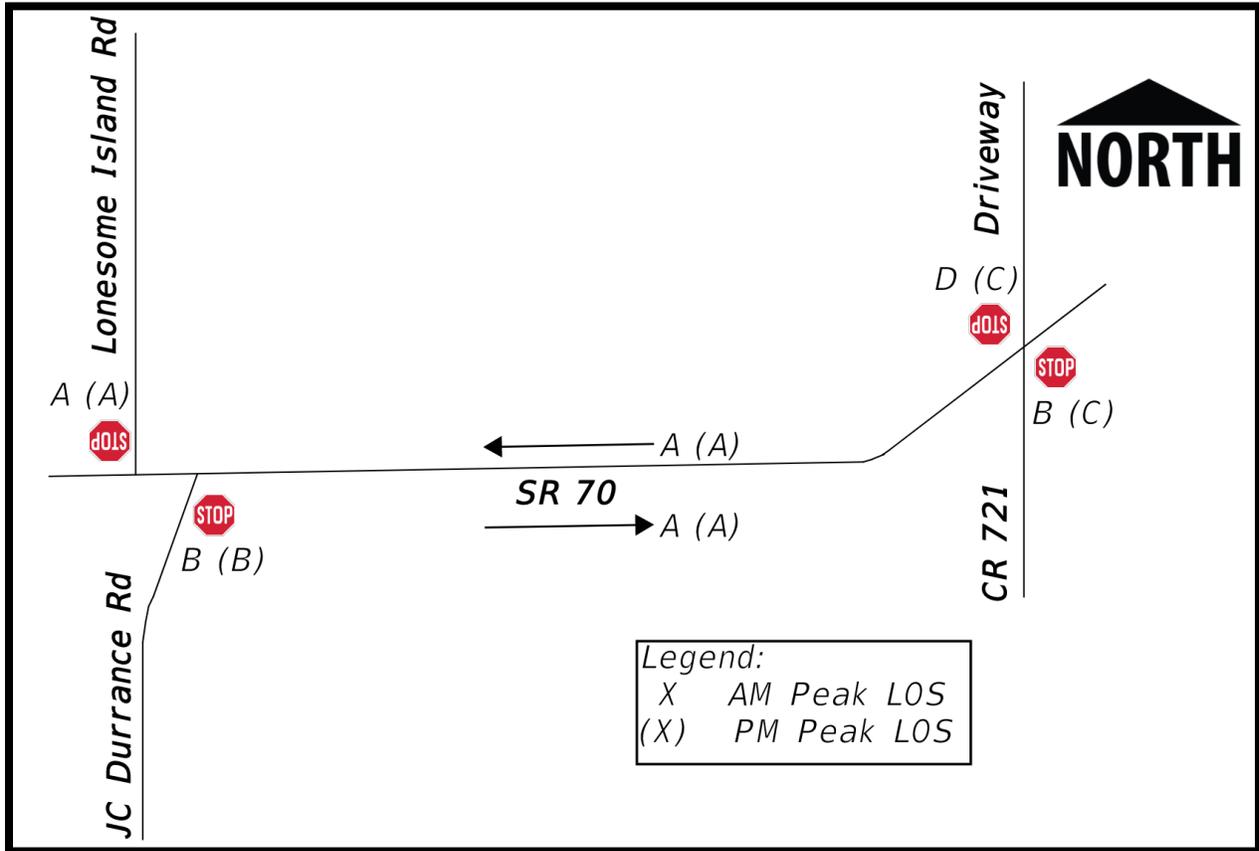


Table 6-6 shows the overall LOS and Delay expected at both intersections, as well as the individual delay and LOS of each approach of each intersection for the AM and PM peak hours for the Design Year 2052 Build scenario. Table 6-7 shows the Arterial LOS, average speed, and density expected along SR 70 for the Design Year 2052 Build scenario. Figure 6-7 depicts the Design Year 2052 Build LOS on the map.

Table 6-6 | Design Year 2052 Build Intersection LOS

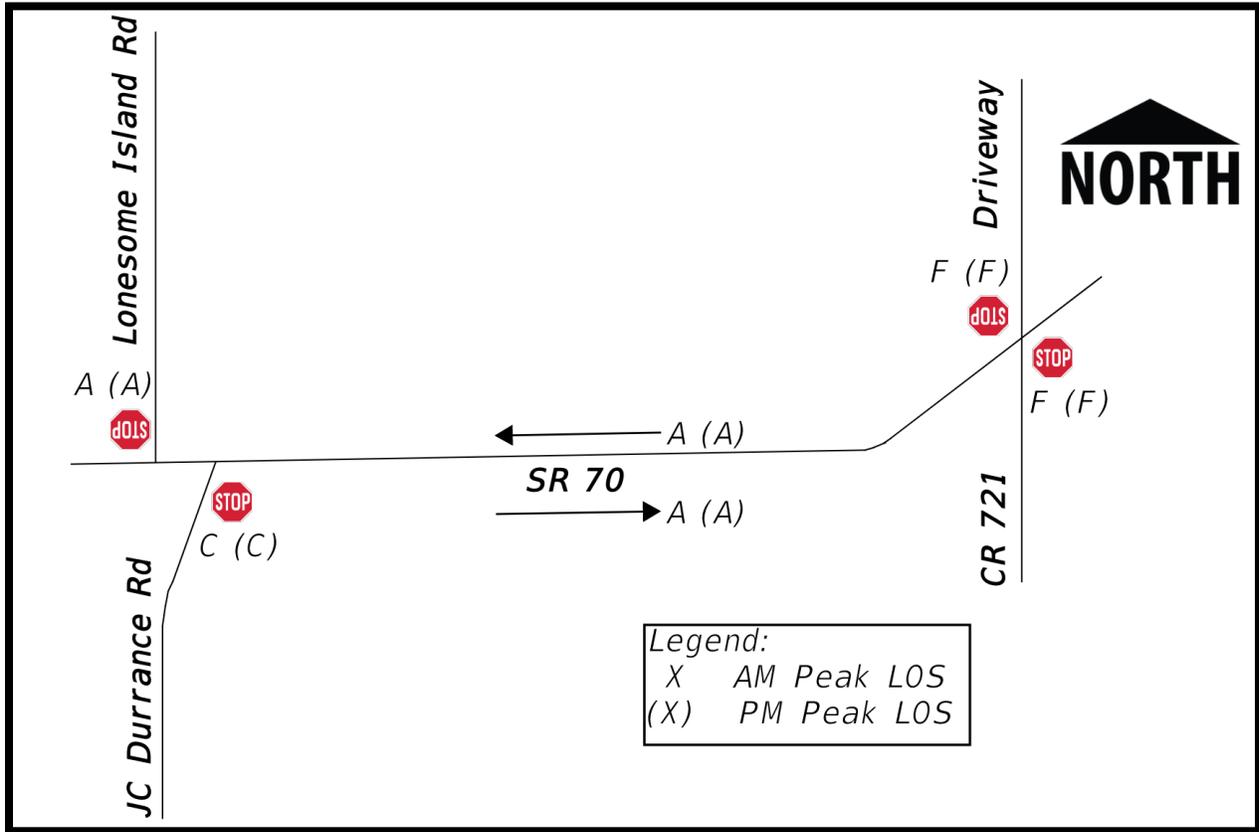
| Intersection | Peak Hour | LOS | Overall Delay ¹ | NB Delay ¹ / LOS | SB Delay ¹ / LOS | EB Delay ¹ / LOS | WB Delay ¹ / LOS |
|-----------------------------------|-----------|-----|----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|
| Lonesome Island Rd/JC Durrance Rd | AM | A | 0.3 | 22.5 / C | 0.0 / A | 9.0 / A | 9.4 / A |
| | PM | A | 0.5 | 23.3 / C | 0.0 / A | 0.0 / A | 9.4 / A |
| CR 721 | AM | D | 29.0 | >300 / F | 168.6 / F | 8.7 / A | 14.1 / B |
| | PM | C | 19.5 | 120.0 / F | 53.1 / F | 8.8 / A | 10.6 / B |

¹Delay measured in seconds per vehicle

Table 6-7 | Design Year 2052 Build Arterial LOS

| Segment | Peak Hour | LOS | Average Speed (mph) | Density (pc/mi/ln) |
|---|-----------|-----|---------------------|--------------------|
| SR 70 from Lonesome Island Rd to CR 721 | AM | A | 65.0 | 7.5 |
| | PM | A | 65.0 | 6.8 |

Figure 6-7 | SR 70 Design Year 2052 Build LOS



Section 7 Future Condition Safety Analysis

A safety analysis was conducted for the future conditions of SR 70 from Lonesome Island Road to the Southern Leg of CR 721. The safety predictive methods utilized in this evaluation were based on the Safety Performance Functions (SPFs) provided in the 2010 *Highway Safety Manual (HSM)* 1st Edition predictive methods Part C to forecast or predict crash frequency for the No-Build scenario. Predicted crash frequency for the SR 70 arterial segments and intersections was forecasted using the FDOT HSM spreadsheet tools available on the FDOT website. The FDOT HSM spreadsheets used to calculate the anticipated future crash frequencies are provided in **Appendix J**. The AADT traffic volumes utilized for the crash predictions for SR 70 and side streets in Opening Year (2032) and Design Year (2052) for No-Build and Build scenarios are summarized in **Table 7-1**.

Table 7-1 | SR 70 Mainline and Side Streets 2032 and 2052 AADT

| Roadway | 2032 AADT | 2052 AADT |
|------------------------|-----------|-----------|
| SR 70 | 7,800 | 12,500 |
| Lonesome Island Rd | 150 | 200 |
| JC Durrance Rd | 200 | 350 |
| Greenbrier Ln | 150 | 200 |
| DC Bar Ranch Rd | 150 | 200 |
| Lykes Rd | 150 | 200 |
| Southern Leg of CR 721 | 2,700 | 4,200 |

7.1 No-Build Arterial Predictive Crashes

Predictive crash analysis was conducted for the No-Build arterial segments and intersections within the study limits. The area of influence (AOI) includes the SR 70 mainline between Lonesome Island Road and the Southern Leg of CR 721. The roadway in the study limits is considered a rural two-lane road. The predictive method analysis consisted of using the HSM 1st Edition, Volume 2, Chapter 10: Predictive Method for Rural Two-Lane, Two-Way Roads spreadsheets provided on the FDOT website. The intersection of SR 70 at the Southern Leg of CR 721 has an AADT of 4,200 which exceeds the AADT for a minor road of a four-leg stop controlled intersection. The HSM states that AADTs outside this range may not provide accurate results. The HSM spreadsheet extrapolates the predicted crash at this location. The SR 70 predicted crashes for the No-Build scenario are summarized in **Table 7-2**. The HSM spreadsheet results for this safety analysis are provided in **Appendix J**.

Table 7-2 | No-Build Scenario Predicted Crashes – 2032 and 2052

| Crash Severity | Predicted (crashes/year) | |
|----------------------------|--------------------------|-----------|
| | Year 2032 | Year 2052 |
| Total Crashes | 31.4 | 48.2 |
| Fatal and injury (FI) | 11.0 | 16.8 |
| Property damage only (PDO) | 20.4 | 31.4 |

7.2 Build Arterial Predictive Crashes

Predictive crash analysis was conducted for the Build arterial segments and intersections within the study limits. The Build scenario consists of SR 70 operating as a four-lane divided arterial and conservative assumptions were made regarding access management. Full or directional median openings were assumed at all unsignalized intersections. Right turn lane recommendations were made based on the *FDOT Access Management Guidebook (2019)* criteria. The roadway access class was determined to be 3 which requires 1,320 feet of spacing for directional median openings and 2,640 feet of spacing for full median openings. The spacing requirements are expected to be compliant in the design of this project since the existing side streets are spaced adequately. The predictive method analysis consisted of using the HSM 1st Edition, Volume 2, Chapter 11: Predictive Method for Rural Multilane Highways spreadsheets provided on the FDOT website. The SR 70 predicted crashes for the Build scenario are summarized in **Table 7-3**. The HSM spreadsheet results for this safety analysis are provided in **Appendix J**.

Table 7-3 | Build Scenario Predicted Crashes – 2032 and 2052

| Crash Severity | Predicted (crashes/year) | |
|----------------------------|--------------------------|-----------|
| | Year 2032 | Year 2052 |
| Total Crashes | 12.6 | 22.0 |
| Fatal and injury (FI) | 5.8 | 9.7 |
| Property damage only (PDO) | 6.8 | 12.2 |

7.3 Future Arterial Predictive Crash Comparisons

The predicted crashes for the No-Build and Build scenarios for Opening Year (2032) were compared and are summarized in **Table 7-4**. Compared to the No-Build scenario, the total number of predicted crashes for the build scenario decreases by 60%. The property damage only crashes decreased by about 67%. The fatal and injury crashes decreased by about 47%. The crash reduction is primarily attributed to improving the roadway from a two-lane undivided section to a four-lane divided section with a 40-ft wide median. Other factors of the Build scenario improving the number of predicted crashes include widening lanes from 10-feet wide to 12-feet wide, improved shoulders and adding left turn lanes at intersections.

Table 7-4 | No-Build and Build Predicted Crash Comparison – Year 2032

| Crash Severity | Predicted (crashes/year) | |
|----------------------------|--------------------------|-------|
| | No-Build | Build |
| Total Crashes | 31.43 | 12.64 |
| Fatal and injury (FI) | 11.04 | 5.84 |
| Property damage only (PDO) | 20.39 | 6.80 |

The predicted crashes for the No-Build and Build scenarios for Design Year (2052) were compared and are summarized in **Table 7-5**. There is a 54% decrease in total crashes, a 42% decrease in fatal and injury crashes, and a 61% decrease in property damage only crashes comparing the No-Build and Build scenarios. The same factors stated above involved with the proposed Build scenario improvements influence the decrease in predicted crashes for year 2052.

Table 7-5 | No-Build and Build Predicted Crash Comparison – Year 2052

| Crash Severity | Predicted (crashes/year) | |
|----------------------------|--------------------------|-------|
| | No-Build | Build |
| Total Crashes | 48.17 | 21.96 |
| Fatal and injury (FI) | 16.79 | 9.73 |
| Property damage only (PDO) | 31.38 | 12.23 |

7.4 Predictive Crash Costs

The average cost per crash and crash distribution factors for roadway facility types were obtained from the 2023 FDM Section 122.6. The rural two-lane undivided roadway facility type was utilized for the analysis of the No-Build SR 70 arterial segments and intersections. The present-day cumulative costs for the predicted crashes for the No-Build scenario from 2032 through 2052 totals approximately \$304 million. The present-day cumulative costs for the Build scenario totals approximately \$145 million. Overall, the cumulative predicted crash cost for the Build scenario is decreased by about 52% compared to the No-Build scenario. The property damage only costs decrease by about 65% and fatal and injury costs decrease by about 52% for the Build scenario compared to the No-Build scenario. The cost summary is provided in **Table 7-6**. The breakdown of the cost estimates is provided in **Appendix J**.

Table 7-6 | Cumulative Predicted Crash Cost Comparison – Years 2032-2052

| Crash Severity | No-Build Scenario | Build Scenario | Build vs No-Build Difference % |
|----------------------------|-----------------------|-----------------------|--------------------------------|
| Fatal and injury (FI) | \$ 301,358,335 | \$ 144,376,651 | 52% decrease |
| Property damage only (PDO) | \$ 2,193,045 | \$ 768,032 | 65% decrease |
| Total | \$ 303,551,379 | \$ 145,144,682 | 52% decrease |

(3) Note: All costs are calculated as 2023 present-day costs

Section 8 Conclusions and Recommendations

Improvements to SR 70 from Lonesome Island Road to the Southern Leg of CR 721 are recommended based on historic crash data of the corridor, existing evacuation clearance times, and population growth in the project area. SR 70 serves as a major east-west corridor and evacuation route in Highlands County and across the state of Florida.

SR 70 from Lonesome Island Road to the Southern Leg of CR 721 is currently a two-lane undivided roadway operating at an acceptable LOS with a crash rate that is 36% higher than the statewide average. Based on future population projections, existing evacuation studies, and predictive crash analysis, the number of crashes and evacuation clearance times along SR 70 are expected to worsen with time. Therefore, it is recommended SR 70 from Lonesome Island Road to the Southern Leg of CR 721 be widened from a two-lane undivided highway to a four-lane divided highway with a median.

By widening the corridor from two lanes to four lanes, the capacity of vehicles that SR 70 can support in an emergency evacuation scenario will increase, leading to a decrease in evacuation clearance times throughout Highlands County for all evacuation scenarios. Also, by converting SR 70 from two lanes to four lanes, the number of crashes is expected to decrease by approximately 52% by 2052 when compared to the predicted 2052 number of crashes of the No-Build alternative for SR 70. Historic crash data shows that the most common types of crashes along this stretch of SR 70 are opposing sideswipes and guardrail face crashes, many of which are caused by vehicles crossing into the opposing lane while attempting to pass traffic traveling in the same direction. By adding more lanes and providing a median barrier, it is predicted that the number of opposing sideswipes, guardrail face crashes, and overall number of crashes will all decrease. SR 70 from Lonesome Island Rd to the Southern Leg of CR 721 is projected to continue to operate at an acceptable LOS in 2052 with the widening from two lanes to four lanes as well. There are several adjacent SR 70 projects (FPID's: 451649-1, 414506-1, 414506-5, 449851-1) that involve widening the road as well. It is recommended to widen SR 70 from Lonesome Island Road to the Southern Leg of CR 721 from two lanes to four lanes in order to provide a more consistent typical section throughout the various corridors of SR 70.

APPENDICES

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- APPENDIX B: SR 70 Design Traffic Technical Memorandum
- APPENDIX C: Manual Turning Movement Counts
- APPENDIX D: Existing Synchro and HCS LOS Computer Outputs
- APPENDIX E: Crash Data and FDOT Statewide Crash Facts
- APPENDIX F: Signal Warrant Analysis Report
- APPENDIX G: Existing Highlands County Evacuation Scenario Reports
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- APPENDIX J: HSM Spreadsheets and Costs
- APPENDIX K: Preliminary Roadway Design Concepts

APPENDIX A: Methodology Letter of Understanding

Project Traffic Analysis Report

SR 70 from Lonesome Island Road to the Southern Leg of CR 721

F.P.I.D. 449851-1



METHODOLOGY LETTER OF UNDERSTANDING

District One

June 2023

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1. Introduction

This memorandum serves as the Methodology Letter of Understanding for the ongoing Project Traffic Analysis Report (PTAR) of SR 70 from Lonesome Island Road to the Southern Leg of CR 721 in Highlands County, Florida. This memorandum covers the criteria, assumptions, traffic analysis methodology, and documentation for the ongoing PTAR.

2. Purpose and Need for Project

The Project Traffic Analysis Report (PTAR) will summarize the traffic data collected and the traffic level of service (LOS) analyses for SR 70 from Lonesome Island Road to the Southern Leg of CR 721 in Highlands County, Florida. The purpose of the SR 70 project is to provide additional roadway capacity, enhance safety, and improve hurricane evacuation along the SR 70 corridor, a major east-west roadway spanning the state. The PTAR will evaluate safety issues and conduct traffic capacity analysis along SR 70 in order to determine the required number of through lanes to maintain acceptable LOS through the Design Year 2052. Two stop-controlled intersection within the project area will also be evaluated for turn lanes and intersection improvement requirements.

3. Project Location

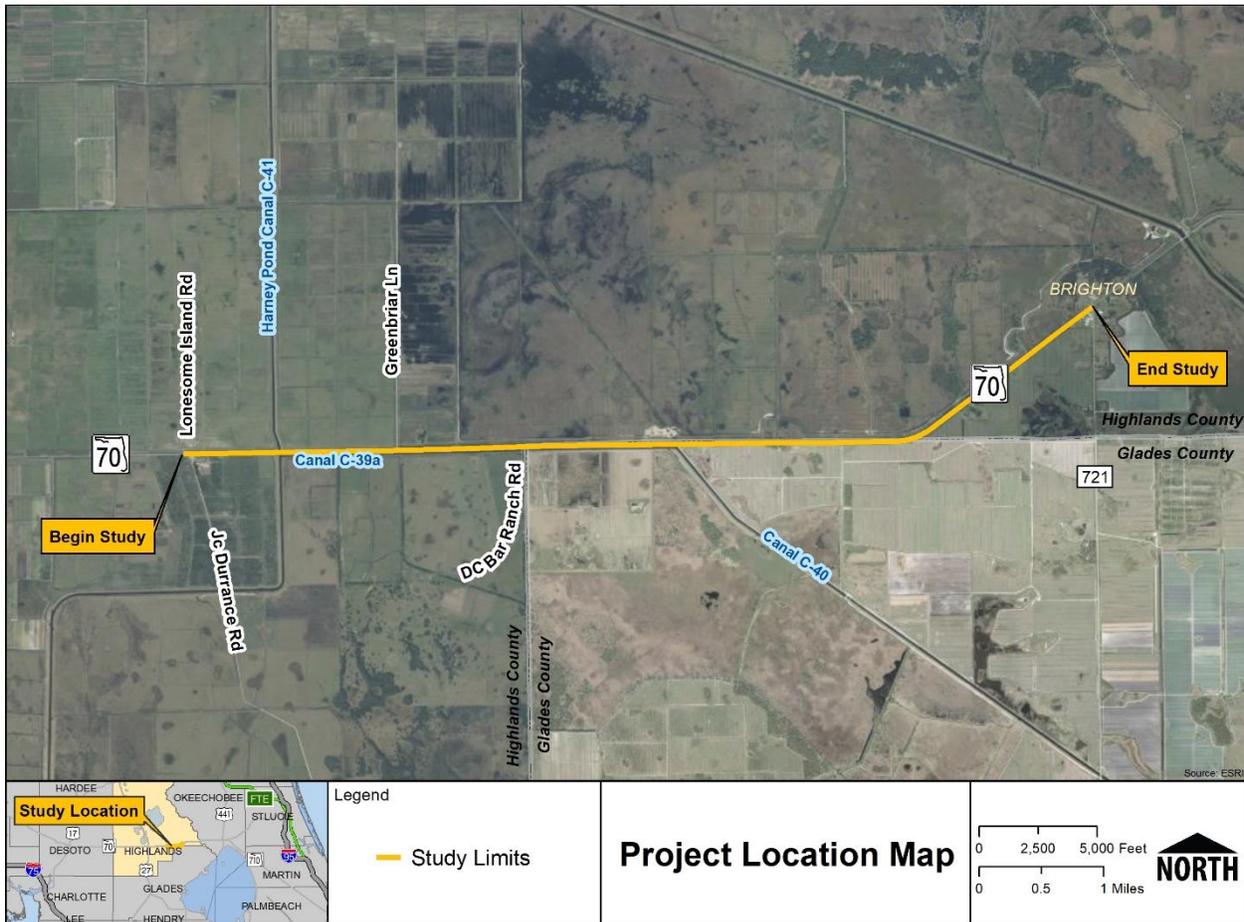
Exhibit 1 depicts the study area for this project. The project study area is rural agricultural with undeveloped land in southern Highlands County.

4. Project Schedule

The PTAR is anticipated to be completed in November 2023. Major milestones of the project are listed below:

- Methodology Letter of Understanding – May 2023
- Draft Project Traffic Analysis Report – September 2023
- Final Project Traffic Analysis Report – November 2023
- Final Preliminary Engineering Report – April 2024
- PD&E Study Complete – October 2025

Exhibit 1: Project Location Map



5. Analysis Years

Twenty four-hour bi-directional volume counts for this project will be provided by FDOT or utilize the available count stations from Florida Traffic Online. Twenty four-hour bi-directional volume counts will be multiplied by the appropriate adjustment factors to obtain the existing year volumes. The weekly seasonal adjustment factor and axle correction factor will be obtained from Florida Traffic Online. Manual Turning Movement Counts (TMC) for this project were completed in November 2022. The analysis years proposed for this project are:

- Existing Year 2022
- Opening Year 2032
- Design Year 2052

The travel demand model (District One Regional Planning Model) years proposed for this project are:

- Base Year 2015
- Horizon Year 2045

6. Considered Alternatives

The No-Build and Build alternatives shall be analyzed in the PTAR.

1. Alternative 1 – No-Build
2. Alternative 2 – Build

7. Traffic Data Collection and Sources

This study will include, but not limited to, the following sources of data:

- Field observations
- Plans, programs, and projects within the area of influence obtained from FDOT and Highlands County
- The latest available 5 years of certified crash data as well as more recent uncertified data that occurred in the study area
 - Source: Florida Signal Four Analytic crash database

The PTAR will include traffic counts provided by FDOT or found on Florida Traffic Online. The PTAR will include the following traffic counts completed in November 2022.

- Four-hour manual turning movement counts conducted for the AM and PM peak periods of a typical weekday at the following 2 locations:
 1. SR 70 at Jc Durance Road/Lonesome Island Road
 2. SR 70 at the southern leg of CR 721
- No Pedestrians or Bicycles crossed either intersection during the turning movement counts.

8. Travel Demand Forecasting

All future years' traffic forecasts will be provided by the Department.

Evacuation Scenarios

The Transportation Interface for Modeling Evacuations (TIME) software will be utilized as part of this study to determine the traffic demand projected during an evacuation scenario in the surrounding area. TIME was developed by the Florida Division of Emergency Management (FDEM) as part of the Statewide Regional Evacuation Study Program (SRESP) to analyze evacuation trips under a variety of evacuation conditions and to report evacuation clearance times. The clearance times from the TIME software for Highlands County will be utilized in this study and compared to the travel time along SR 70 within this study limits.

9. Adjustment Procedures

The 2052 AADTs will be developed by extrapolating the Future Year model output or using an appropriate established growth rate. The adjusted year 2052 AADTs will be balanced and evaluated using the latest 2022 traffic counts. The conversion of the AADT volumes into Directional Design Hour Volumes (DDHV) will be through the application of the K factor and D factor, in accordance with the 2019 FDOT Project Traffic Forecasting Handbook. The future peak direction of traffic flow will be developed based on existing traffic conditions with adjustments to account for any impacts as a result of future developments. Linear interpolation between Existing Year (2022) and Design Year (2052) traffic volumes will be employed to estimate Opening Year (2032) traffic volumes. The resulting project traffic turning movement volumes will be compared with the traffic counts as well as historic trends and other studies in the project area to ensure reasonability.

10. Traffic Factors

The PTAR will provide traffic design factors when all traffic counts are completed and prior to starting traffic analysis. The PTAR will include recommended traffic design factors with calculations.

The following traffic design factors will be used in the analysis and documentation in this study.

K-Factor

The K-Factor will be calculated using each of the 24-hour automatic volume approach count locations. This value will be compared to the appropriate standard K-Factor given in the 2019 FDOT Project Traffic Forecasting Handbook. A comparison will be made between the standard K-Factor and individual calculated factors, and engineering judgement will be used to determine the most appropriate K-Factor.

D-Factor

The D-Factor will be calculated using each of the 24-hour automatic volume approach count locations. The average measured D-Factor will be calculated based on the AM or PM peak hour. This value will be compared to the appropriate D-Factors given in the 2019 FDOT Project Traffic Forecasting Handbook. This will ensure the calculated value lies between the appropriate range of D-Factors.

T-Factor

The T-Factor will be calculated based on the 24-hour vehicle classification counts. The locations will be compared and evaluated.

11. Operations and Analysis Procedures

The Highway Capacity Manual, 6th Edition and Synchro 11 (Version 11, Build 140) will be used to analyze the roadway segments and intersections.

Operational Measures of Effectiveness (MOE) to be utilized for the evaluation of alternatives include:

- Arterial Segments – travel time, travel speed, density, LOS
- Unsignalized intersections – movement delay, movement LOS

12. Qualifying Provisions

The 2023 Multimodal Quality/Level of Service Handbook identifies the acceptable Level of Service (LOS) target for the State Highway System outside urbanized areas during peak travel hours as LOS C.

13. Safety Analysis

Crash analysis will be conducted with the latest available five years of certified crash data. A supplemental review of more recent uncertified crash data will also be performed to identify any changes in crash trends that may have occurred in the study area. Crashes along SR 70 will be evaluated and documented. The data collected will include crash type, location, severity, lighting conditions (day versus night), and pavement conditions (wet versus dry). Given the information obtained from the crash data, safety analysis will be performed to identify needs associated with the existing and future conditions. A predictive safety analysis will be performed to estimate the quantitative safety comparison between the no-build and build alternatives using the Highway Safety Manual Part C procedures.

APPENDIX B: SR 70 Design Traffic Technical Memorandum

July 2023

SR 70 from DeSoto/Highlands County Line to NW 128th Avenue

Final Design Traffic Technical Memorandum



SR 70
Final Design Traffic
Technical Memorandum

July 2023
Highlands County and Okeechobee
County, FL

Prepared by RS&H, Inc. at the direction
of FDOT District One

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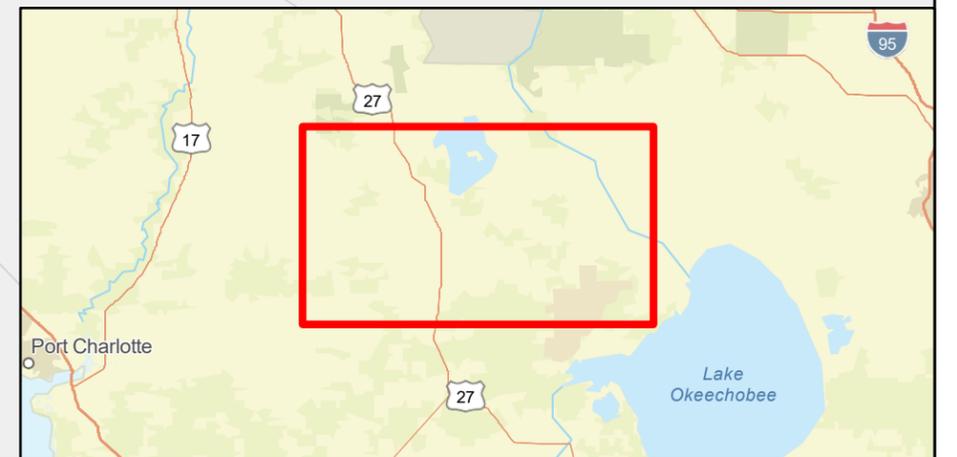
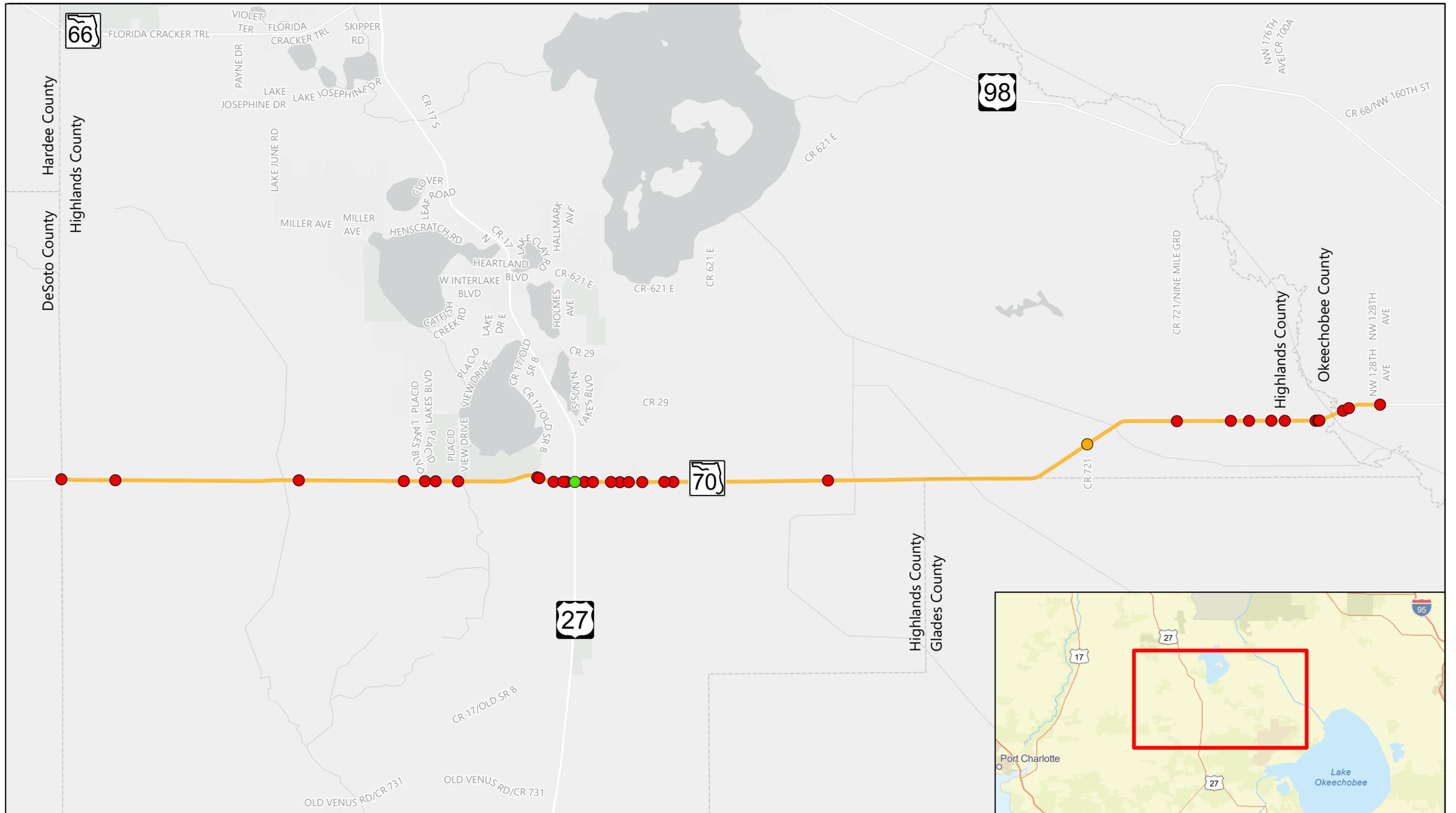
1 Introduction

1.1 Project Description

The purpose of this study is to evaluate capacity and safety improvements along SR 70 from the DeSoto County Line to NW 128th Avenue in Okeechobee County. The project limits are shown in **Figure 1-1** and the total project length is approximately 37.8 miles. This study is intended to develop updated traffic volumes for the study area using current traffic data and travel demand models to subsequently reevaluate the operational performance of a proposed condition for the corridor. The volumes developed will be used for upcoming PD&E studies.

1.2 Project Location

The SR 70 project limits spans from Highlands County Line Road to the Kissimmee River in Highlands County and from the Kissimmee River to NW 128th Avenue in Okeechobee County. SR 70 is a two-lane undivided facility with a posted speed limit of 60 miles per hour (mph) from Highlands County Line Road to Old State Route 8 (north), 55 mph from Old State Route 8 to Distribution Boulevard, 45 mph from Distribution Boulevard to Ekhoﬀ Lane, 55 mph from Ekhoﬀ Lane to Highlands Boulevard, and 60 mph from Highlands Boulevard to NW 128th Avenue. The existing typical section for SR 70 is a two-lane undivided rural roadway with one 12-foot lane in each direction and open ditches. There are no existing designated bicycle or pedestrian facilities. The SR 70 intersection at US 27 is the only signalized study intersection within the study limits. The SR 70 intersection at CR 721 South currently has flashing beacons. Overhead utilities are located throughout the project limits and agricultural land use is present along a majority of the corridor. The assigned SR 70 Context Classification within the project limits is C2 (Rural) from Highlands County Line Road to west of Jefferson Avenue, C1 (Natural) from west of Jefferson Avenue to Placid Lakes Boulevard, and C2 (Rural) from Placid Lakes Boulevard to NW 128th Avenue.



- Legend**
- Project Limits
- Study Intersection Control Type**
- Unsignalized (32)
 - Signalized (1)
 - Flashing Yellow (1)

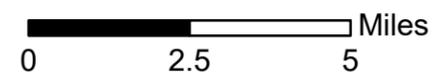


Figure 1-1: Project Location Map

2 Project History

2.1 Background

Multiple segments of SR 70 in Highlands County have been studied by FDOT in recent years. The SR 70 corridor from Jefferson Avenue to CR 29 was studied as part of the Project Development and Environment (PD&E) study that was conducted 2017 (see **Appendix A** for the Design Traffic Technical Memorandum). The intent of this document is to provide updated design traffic data to be utilized in ongoing and upcoming PD&E studies to obtain NEPA approval for project advancement. The following projects will be supported by this document:

- SR 70 from DeSoto County line to Jefferson Avenue (451649-1)
- SR 70 from Jefferson Avenue to US 27 (414506-3)
- SR 70 from US 27 to CR 29 (414506-4)
- SR 70 from CR 29 to Lonesome Island Road (414506-5)
- SR 70 from Lonesome Island Road to CR 721 (449851-1)
- SR 70 from CR 721 to NW 128th Avenue (450334-1)

2.2 Data Collection

A variety of transportation data was collected as part of this study. The following sections describe the types and methods of data collection that were employed. The raw data is included in **Appendix B**. **Figure 2-1** shows the data collection sites.

- 4-Hour Turning Movement Counts (TMC) were collected at the following locations from 7:00 AM – 9:00 AM and 4:00 PM – 6:00 PM:
 1. SR 70 at SE Highlands County Line Road
 2. SR 70 at Deer Run/Blue Head Street
 3. SR 70 at Robert McGee Road
 4. SR 70 at Lightsey Ranch Road
 5. SR 70 at Placid Lakes Boulevard/South Jefferson Avenue
 6. SR 70 at Park Land Drive
 7. SR 70 at Placid View Drive
 8. SR 70 at Old SR 8 North
 9. SR 70 at Old SR 8 South
 10. SR 70 at CNI Driveway
 11. SR 70 at Glades Electric Driveway
 12. SR 70 at Wedgeworth Driveway
 13. SR 70 at US 27
 14. SR 70 at Myers Road/Placid Pine Drive

15. SR 70 at North Edge
 16. SR 70 at Broward Avenue
 17. SR 70 at Highlands Boulevard
 18. SR 70 at Citrus Boulevard
 19. SR 70 at Bear Road
 20. SR 70 at Hall Road/Turner Too Road
 21. SR 70 at CR 29/KW Farms Road
 22. SR 70 at Lonesome Island Road/JC Durrance Road
 23. SR 70 at CR 721 South
 24. SR 70 at CR 721 North
 25. SR 70 at Boney Lane/Fulmar Terrace
 26. SR 70 at NW New Pine Ridge Road
 27. SR 70 at NW 175th Terrace
 28. SR 70 at Jordan Terrace/SW Rucks Dairy Road
 29. SR 70 at NW Riverside Road
 30. SR 70 at Shellcracker Loop
 31. SR 70 at Bream Cove
 32. SR 70 at SW 144th Parkway
 33. SR 70 at NW 141st Avenue
 34. SR 70 at NW 128th Avenue
- 48-Hour Volume Count
 - US 27 south of SR 70
 - CR 29 north of SR 70
 - SR 70 east of CR 721
 - 48-Hour Class Count
 - CR 721 south of SR 70
 - CR 721 north of SR 70
 - SR 70 west of CR 721
 - SR 70 east of Desoto County Line

Data was also gathered from other available sources, including sixteen (16) count stations included in FDOT's Florida Traffic Online (FTO) database. At some FTO count stations, data is not collected annually; values for 2021 are estimated and may not accurately reflect 2021 demand.

The development of Existing Year (2022) Average Annual Daily Traffic (AADT) values is documented in **Table 2-1** and **Table 2-2**. AADT values along SR 70 were developed using FTO Historical AADT data for 2021 and growing by one year using an assumed 2% annual growth rate. If FTO data was not available, volumes were developed using the collected volume/classification counts, seasonal factors, and axle correction factors (as necessary). AADTs for cross streets were developed a little differently as volume counts were not available for every

cross street. Based on the turning movement counts, the PM peak experienced the highest traffic volumes across most intersections. For intersections where an AADT from FTO was available, a “peak hour to daily volume factor” was developed, dividing the daily volume by the PM peak hour approach volume. On average, this factor was about 10. For cross streets without a volume count, the selected Existing Year (2022) AADT was calculated as the PM peak hour approach volume multiplied by 10. A minimum AADT was also assumed for cross streets where the calculated AADT was less than 100.

Existing AM and PM peak hour volumes collected as part of this study were utilized in the existing intersection analysis. Volumes were adjusted and balanced along the corridor by adding right-turn vehicles upstream/downstream of an intersection or using a dummy node as a sink/source to represent various minor access points (e.g., driveways).

The existing conditions lane configuration is shown in **Figure 2-2**. Existing Year (2022) daily and hourly traffic volumes are shown in **Figure 2-3**. SR 70 AADTs are only shown on **Figure 2-3** where counts were collected.

Table 2-1: Existing Year (2022) SR 70 AADT Development

| SR 70 Roadway Segment | Raw Daily Class Count | Raw Daily Volume Count | Average | Seasonal Factor ¹ | Axle Correction Factor ² | Adjusted AADT | FTO AADT (2021) | Assumed Annual Growth % | Estimated (2022) AADT | Selected Existing (2022) AADT |
|--|-----------------------|------------------------|---------|------------------------------|-------------------------------------|---------------|-----------------|-------------------------|-----------------------|-------------------------------|
| DeSoto County Line to Robert McGee Road | 4,911 | | 5,058 | 0.98 | | 4,957 | 5,700 | 2% | 5,800 | 5,800 |
| | 5,205 | | | | | | | | | |
| Robert McGee Road to Lightsey Ranch Road ³ | 4,911 | | 5,058 | 0.98 | | 4,957 | | | | 5,000 |
| | 5,205 | | | | | | | | | |
| Lightsey Ranch Road to Placid Lakes Boulevard | | | | | | | 4,400 | 2% | 4,500 | 4,500 |
| Placid Lakes Boulevard to US 27 | | | | | | | 5,000 | 2% | 5,100 | 5,100 |
| US 27 to CR 721 South ⁴ | 5,469 | | 5,488 | 0.98 | | 5,378 | 5,500 | 2% | 5,600 | 5,600 |
| | 5,506 | | | | | | | | | |
| CR 721 South to 144 th Parkway ⁵ | | 7,677 | 7,752 | 0.98 | 0.75 | 5,697 | 5,300 | 2% | 5,400 | 5,400 |
| | | 7,826 | | | | | | | | |
| 144 th Parkway to NW 128 th Avenue | | | | | | | 6,000 | 2% | 6,100 | 6,100 |

Notes:

¹Source: Highlands Countywide Report

²Source: 0912, SR 70, US 27 - Okeechobee

³Class counts were used for this segment as FTO counts were not available.

⁴Class count not used in developing existing AADTs. FTO counts were used.

⁵Volume count not used in developing existing AADTs. FTO counts were used.

Table 2-2: Existing Year (2022) Cross Street AADT Development

| Intersecting Roadway Segment | Raw Daily Class Count | Raw Daily Volume Count | Average | Seasonal Factor | Axle Correction Factor | Adjusted AADT | 2021 FTO AADT | PM Peak Hour Volume (5PM - 6PM) | PM Peak Hour to Daily Volume Factor | Selected K Factor | Estimated (2022) AADT | Selected Rounded Existing (2022) AADT |
|---|-----------------------|------------------------|---------|-------------------|------------------------|---------------|---------------|---------------------------------|-------------------------------------|-------------------|-----------------------|---------------------------------------|
| Highlands County Line Rd South of SR 70 | | | | | | | - | 5 | - | 9.5% | 52.63 | 100 |
| Deer Run Rd North of SR 70 | | | | | | | - | 0 | - | 9.5% | 0.00 | 100 |
| Blue Head Street South of SR 70 | | | | | | | - | 0 | - | 9.5% | 0.00 | 100 |
| Robert McGee Rd North of SR 70 | | | | | | | - | 4 | - | 9.5% | 42.11 | 100 |
| Lightsey Ranch Rd South of SR 70 | | | | | | | - | 0 | - | 9.5% | 0.00 | 100 |
| Placid Lakes Blvd North of SR 70 | | | | | | | 900 | 94 | 9.57 | - | - | 900 |
| Jefferson Ave South of SR 70 | | | | | | | - | 24 | - | 9.5% | 252.63 | 250 |
| Park Land Dr South of SR 70 | | | | | | | - | 29 | - | 9.5% | 305.26 | 300 |
| Placid View Dr North of SR 70 | | | | | | | 1,250 | 35 | 35.71 | 9.5% | 368.42 | 350 |
| Old SR 8 North of SR 70 | | | | | | | 1,100 | 124 | 8.87 | - | - | 1,100 |
| Old SR 8 South of SR 70 | | | | | | | 900 | 106 | 8.49 | - | - | 900 |
| CNI Driveway South of SR 70 | | | | | | | - | 6 | - | 9.5% | 63.16 | 100 |
| Glades Driveway North of SR 70 | | | | | | | - | 13 | - | 9.5% | 136.84 | 150 |
| Wedgeworth Driveway South of SR 70 | | | | | | | - | 6 | - | 9.5% | 63.16 | 100 |
| US 27 North of SR 70 | | | | | | | 9,400 | 770 | 12.21 | - | - | 9,400 |
| US 27 South of SR 70 ¹ | | 12,416 | 12,648 | 0.98 ³ | 0.73 ⁵ | 9,048 | 8,765 | 744 | 11.78 | - | - | 8,800 |
| | | 12,879 | | | | | | | | | | |
| Myers Rd North of SR 70 | | | | | | | - | 0 | - | 9.5% | 0.00 | 100 |
| Placid Pines Dr South of SR 70 | | | | | | | - | 37 | - | 9.5% | 389.47 | 400 |
| North Edge Dr North of SR 70 | | | | | | | - | 5 | - | 9.5% | 52.63 | 100 |
| Broward Ave North of SR 70 | | | | | | | - | 30 | - | 9.5% | 315.79 | 300 |

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| Intersecting Roadway Segment | Raw Daily Class Count | Raw Daily Volume Count | Average | Seasonal Factor | Axle Correction Factor | Adjusted AADT | 2021 FTO AADT | PM Peak Hour Volume (5PM - 6PM) | PM Peak Hour to Daily Volume Factor | Selected K Factor | Estimated (2022) AADT | Selected Rounded Existing (2022) AADT |
|---|-----------------------|------------------------|---------|-------------------|------------------------|---------------|---------------|---------------------------------|-------------------------------------|-------------------|-----------------------|---------------------------------------|
| Highland Ave North of SR 70 | | | | | | | - | 49 | - | 9.5% | 515.79 | 500 |
| Citrus Blvd North of SR 70 | | | | | | | - | 20 | - | 9.5% | 210.53 | 200 |
| Bear Rd North of SR 70 | | | | | | | - | 8 | - | 9.5% | 84.21 | 100 |
| Hall Rd North of SR 70 | | | | | | | - | 4 | - | 9.5% | 42.11 | 100 |
| Turner Too Rd South of SR 70 | | | | | | | - | 0 | - | 9.5% | 0.00 | 100 |
| CR 29 North of SR 70 ¹ | | 512 | 503 | 0.98 ⁴ | 0.75 ⁶ | 369 | 750 | 39 | 19.23 | - | - | 750 |
| | | 493 | | | | | | | | | | |
| KW Farms Road South of SR 70 | | | | | | | - | 2 | - | 9.5% | 21.05 | 100 |
| Lonesome Island Rd North of SR 70 | | | | | | | - | 2 | - | 9.5% | 21.05 | 100 |
| JC Durrance Rd South of SR 70 | | | | | | | - | 13 | - | 9.5% | 136.84 | 150 |
| Lykes Ranch Driveway North of SR 70 | | | | | | | - | 0 | - | 9.5% | 0.00 | 100 |
| CR 721 South of SR 70 ² | 2,136 | | 2,154 | 0.98 ⁴ | | 2,110 | 1,900 | 218 | 8.72 | - | - | 1,900 |
| | 2,171 | | | | | | | | | | | |
| CR 721 North of SR 70 ² | 1,067 | | 1,112 | 0.98 ⁴ | | 1,090 | 700 | 79 | 8.86 | - | - | 700 |
| | 1,157 | | | | | | | | | | | |
| Boney Ln North of SR 70 | | | | | | | - | 1 | - | 9.5% | 10.53 | 100 |
| Fulmar Terrace South of SR 70 | | | | | | | - | 15 | - | 9.5% | 157.89 | 150 |
| NW New Pine Ridge Rd North of SR 70 | | | | | | | - | 7 | - | 9.5% | 73.68 | 100 |
| 175th Terrace North of SR 70 | | | | | | | - | 22 | - | 9.5% | 231.58 | 250 |
| 172nd Terrace (Jordan Terrace) North of SR 70 | | | | | | | - | 37 | - | 9.5% | 389.47 | 400 |
| SW Rucks Dairy Rd South of SR 70 | | | | | | | - | 28 | - | 9.5% | 294.74 | 300 |
| Riverside Rd North of SR 70 | | | | | | | - | 11 | - | 9.5% | 115.79 | 100 |

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| Intersecting Roadway Segment | Raw Daily Class Count | Raw Daily Volume Count | Average | Seasonal Factor | Axle Correction Factor | Adjusted AADT | 2021 FTO AADT | PM Peak Hour Volume (5PM - 6PM) | PM Peak Hour to Daily Volume Factor | Selected K Factor | Estimated (2022) AADT | Selected Rounded Existing (2022) AADT |
|----------------------------------|-----------------------|------------------------|---------|-----------------|------------------------|---------------|---------------|---------------------------------|-------------------------------------|-------------------|-----------------------|---------------------------------------|
| Shellcracker Loop North of SR 70 | | | | | | | - | 13 | - | 9.5% | 136.84 | 150 |
| Driveway South of SR 70 | | | | | | | - | 0 | - | 9.5% | 0.00 | 100 |
| Bream Cove North of SR 70 | | | | | | | - | 14 | - | 9.5% | 147.37 | 150 |
| 144th Pkwy South of SR 70 | | | | | | | - | 27 | - | 9.5% | 284.21 | 300 |
| 141st Ave North of SR 70 | | | | | | | - | 11 | - | 9.5% | 115.79 | 100 |
| NW 128th Ave North of SR 70 | | | | | | | 400 | 46 | 8.70 | - | - | 400 |
| SW 128th Ave South of SR 70 | | | | | | | - | 5 | - | 9.5% | 52.63 | 100 |

Notes:

¹Volume count not used in developing existing AADTs. FTO counts were used.

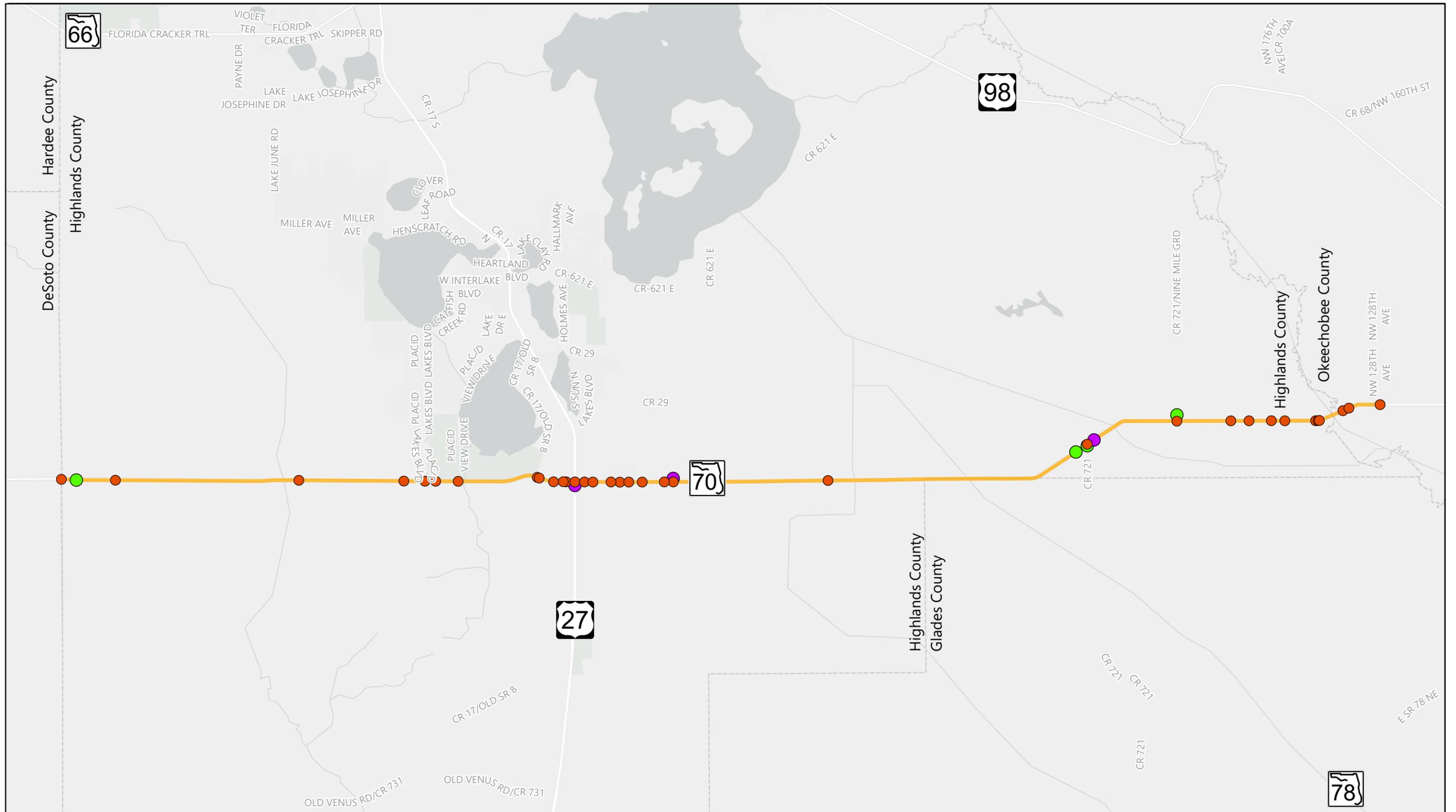
²Class count not used in developing existing AADTs. FTO counts were used.

³Source: 0901, US 27

⁴Source: Highlands Countywide Report

⁵Source: 0914, US 27, SR 70 – Glades County Line

⁶Source: 0903, SR 64, Hardee County Line to Olivia Drive



Legend

— Project Limits

Traffic Data Counts

- 48-Hour Class Count (4)
- 48-Hour Volume Count (3)
- 4-Hour Turning Movement Count (34)

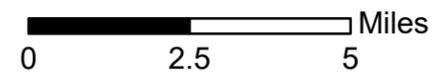
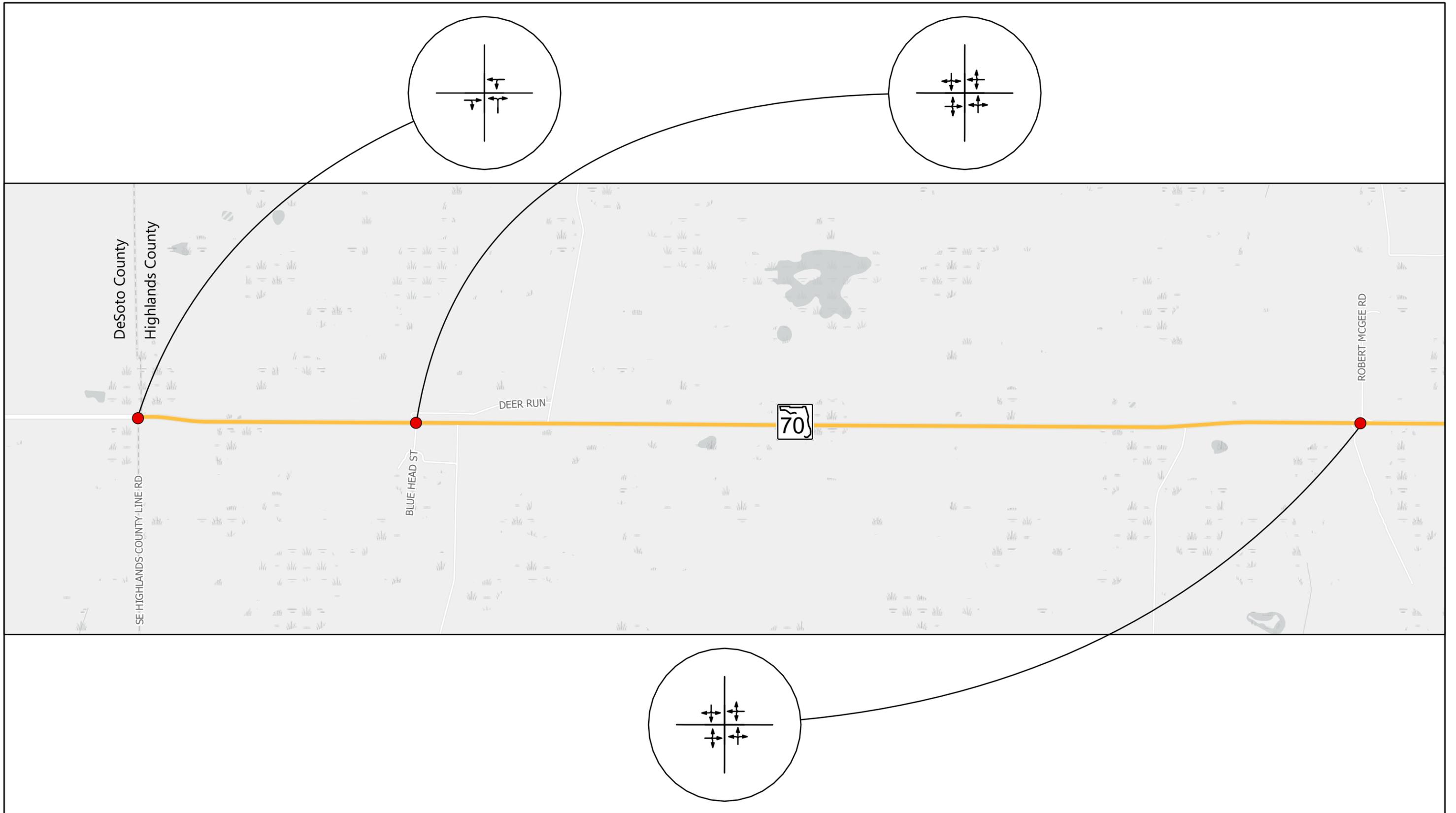


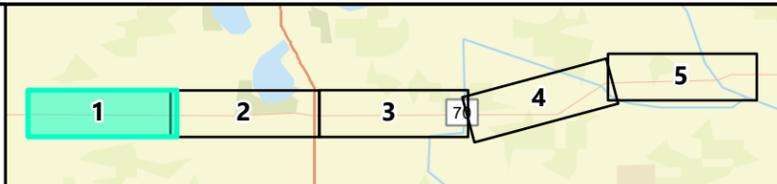
Figure 2-1: Data Collection Locations



Legend

- Project Limits
- Unsignalized (3)

↑↑↑ Lane Configuration

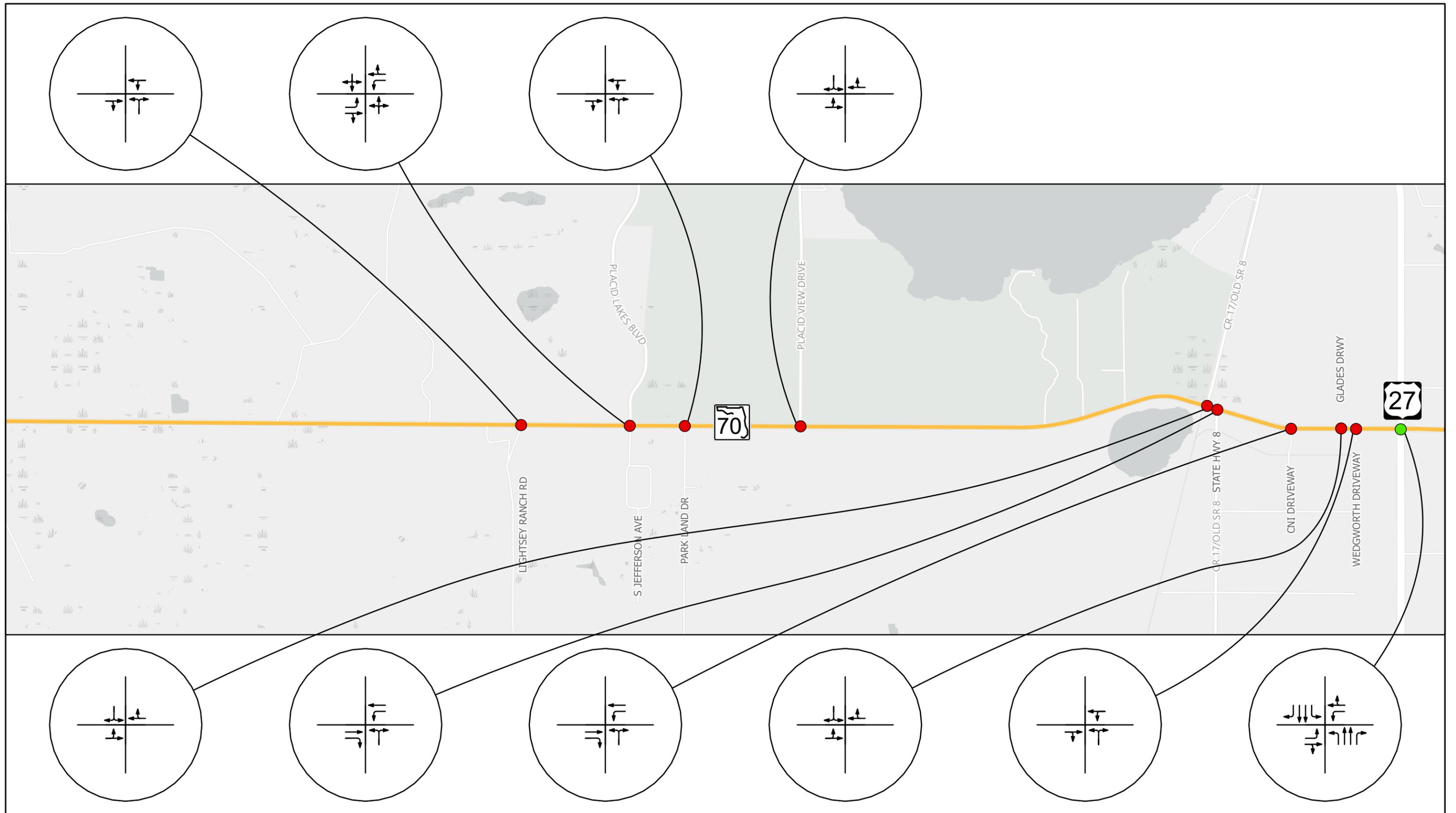


N

0 2,000 Feet

Figure 2-2: Existing Lane Configuration

Sheet 1 of 5



Legend

- Project Limits
- Unsignalized (10)
- Signalized (1)

Lane Configuration

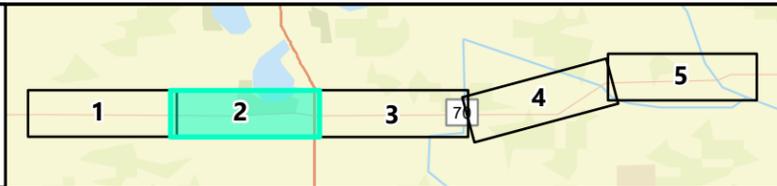
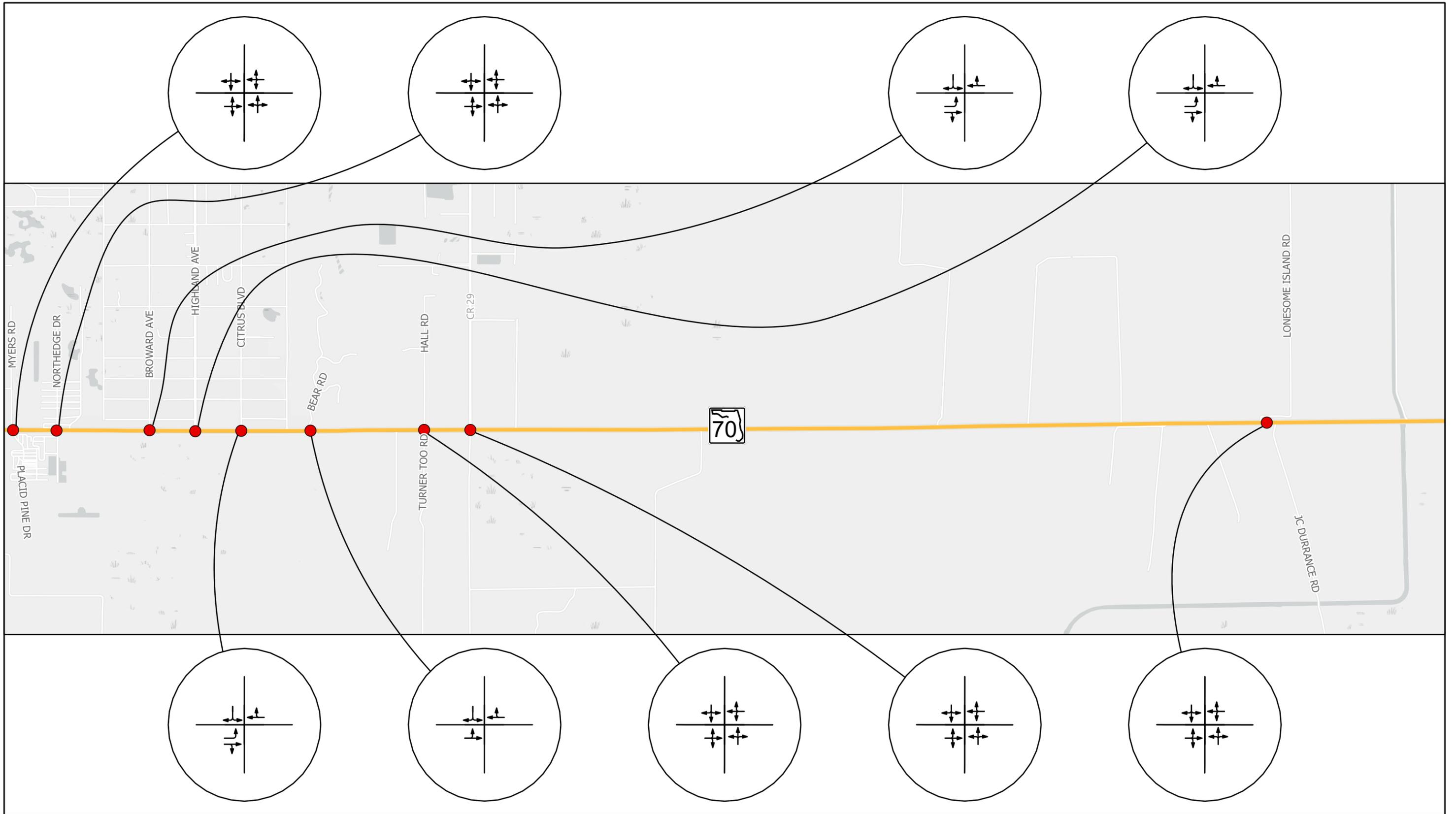


Figure 2-2: Existing Lane Configuration

Sheet 2 of 5



Legend
 — Project Limits
 ● Unsinalized (9)

↔ ↔ Lane Configuration

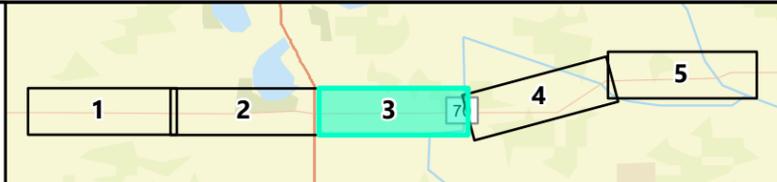
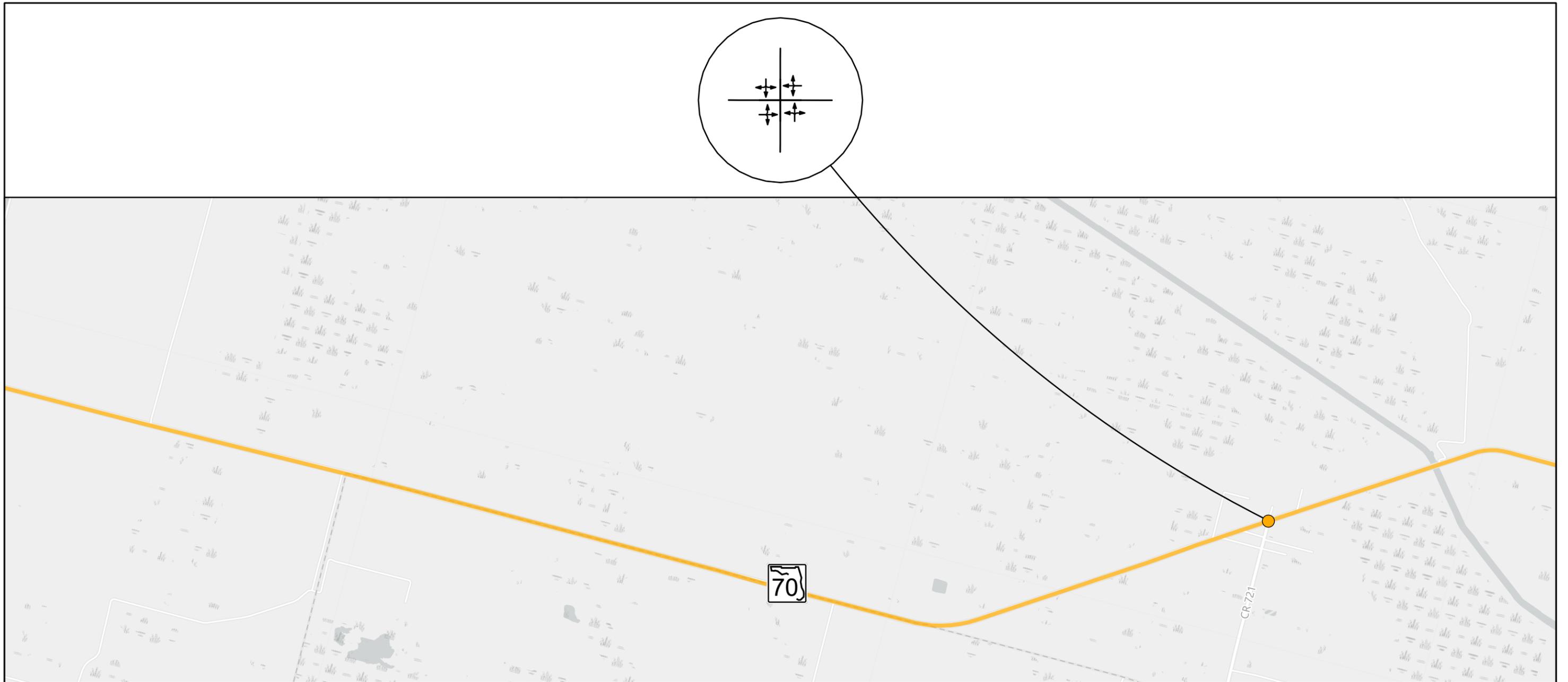


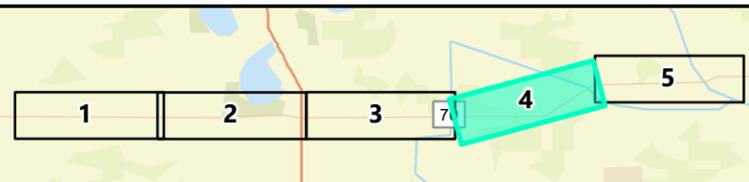
Figure 2-2: Existing Lane Configuration



Legend

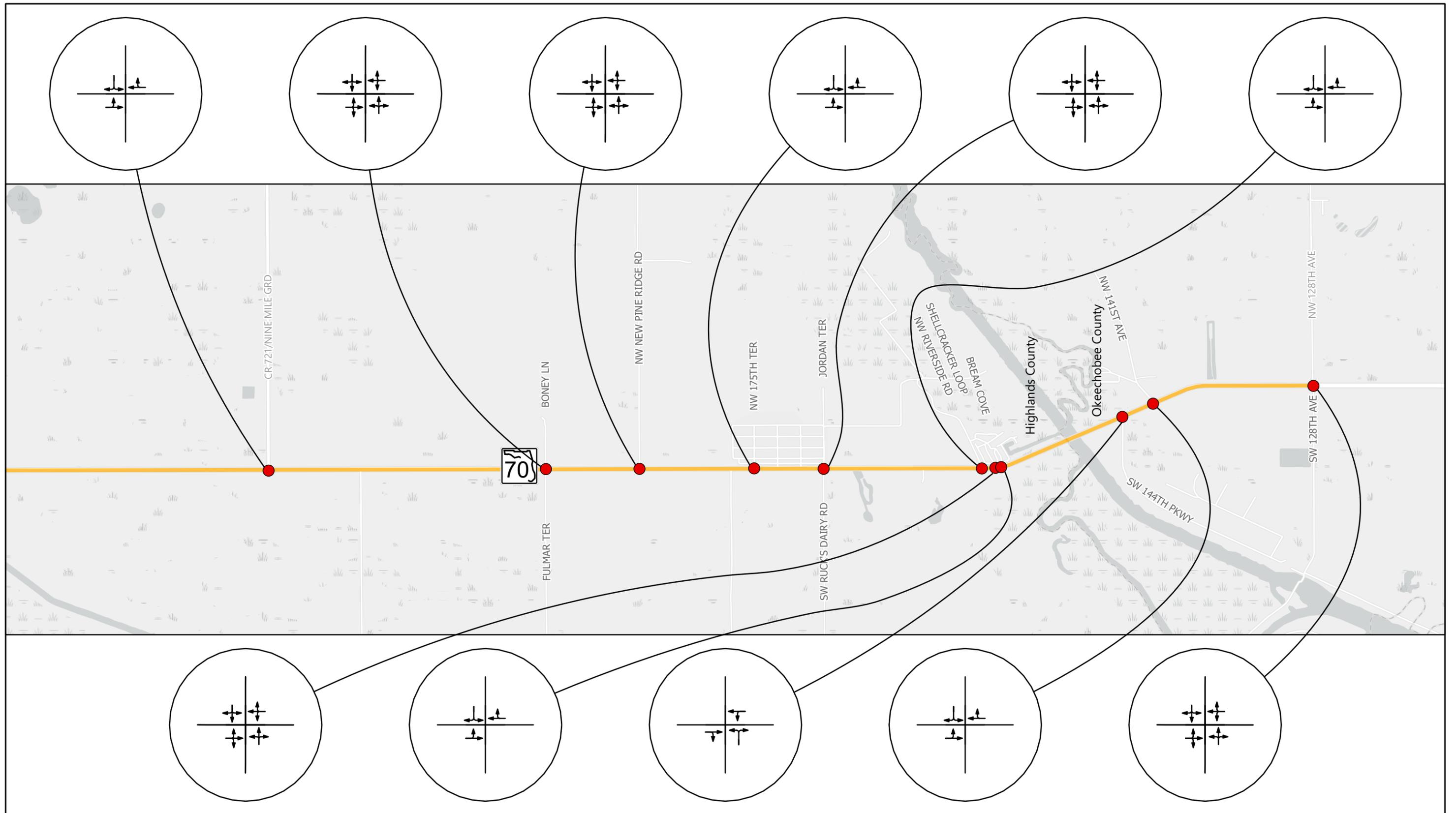
-  Project Limits
-  Flashing Yellow (1)

 Lane Configuration



0 2,000 Feet

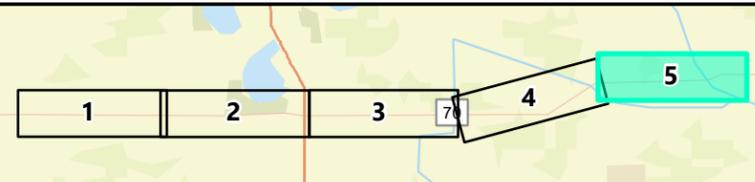
Figure 2-2: Existing Lane Configuration



Legend

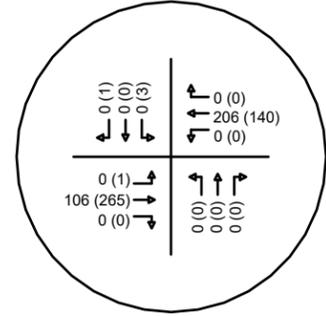
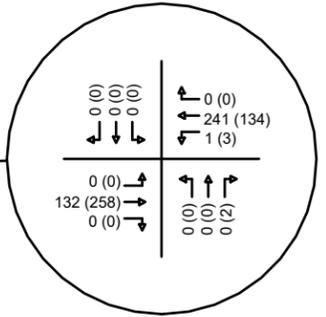
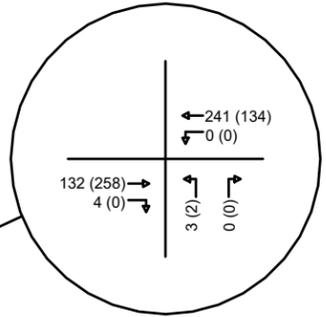
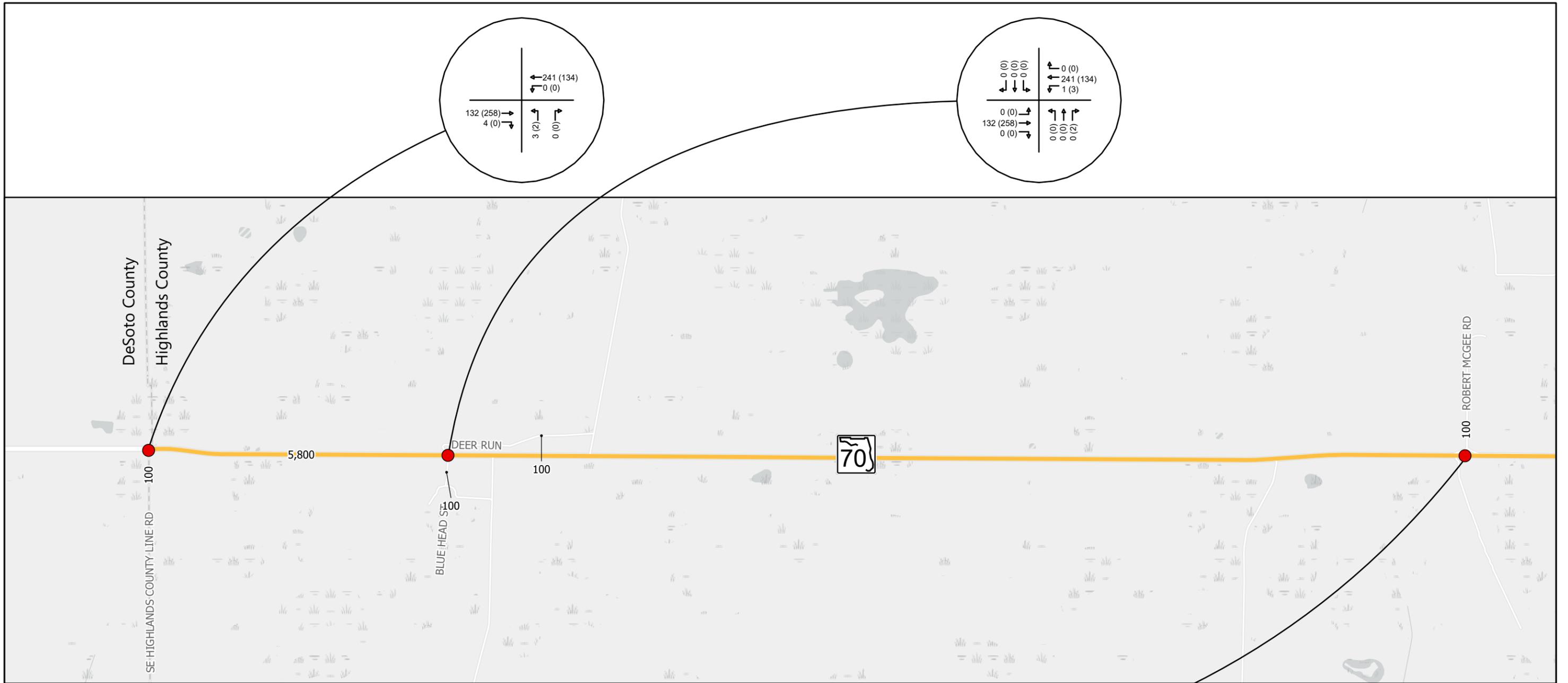
- Project Limits
- Unsignalized (11)

↔ ↔ ↔ Lane Configuration



0 2,000 Feet

Figure 2-2: Existing Lane Configuration



Legend
 Project Limits
 Unsignalized (3)

XX (XX) AM(PM) Peak Hour Volumes
 X,XXX AADT
 ↑↑↑ Turning Movements

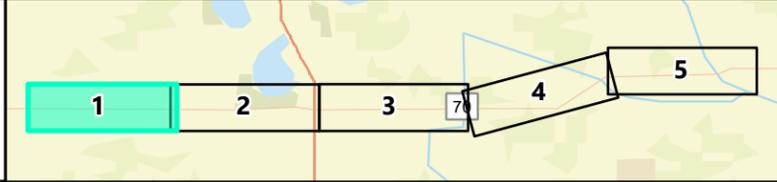
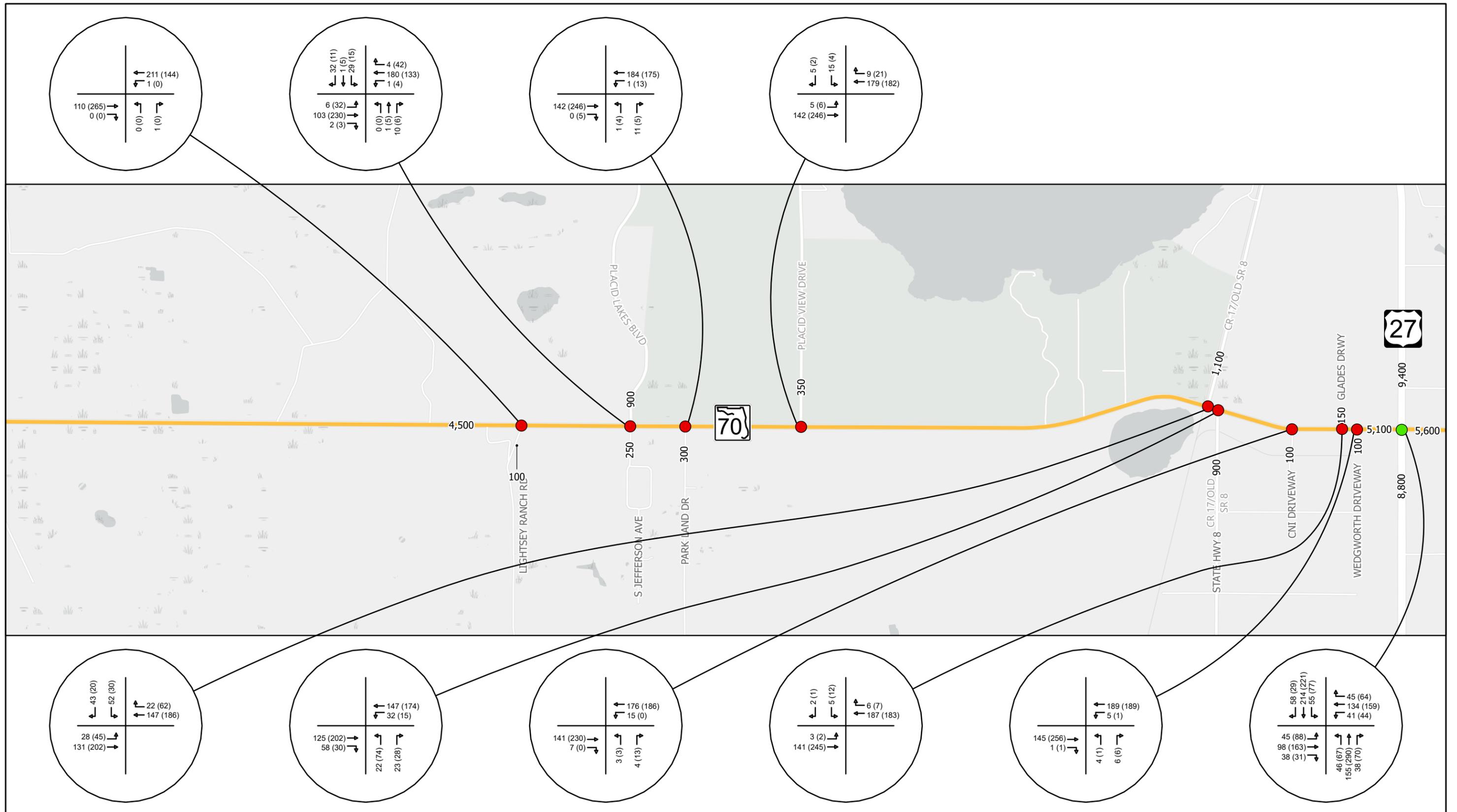


Figure 2-3: Existing Year (2022) AADT and AM (PM) Turning Movement Volumes
 Sheet 1 of 5



Legend

- Project Limits
- Unsignalized (10)
- Signalized (1)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- Turning Movements

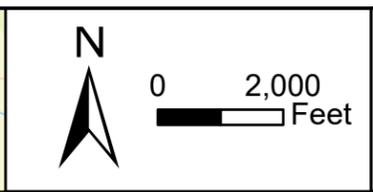
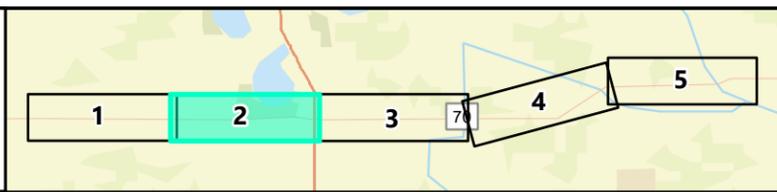
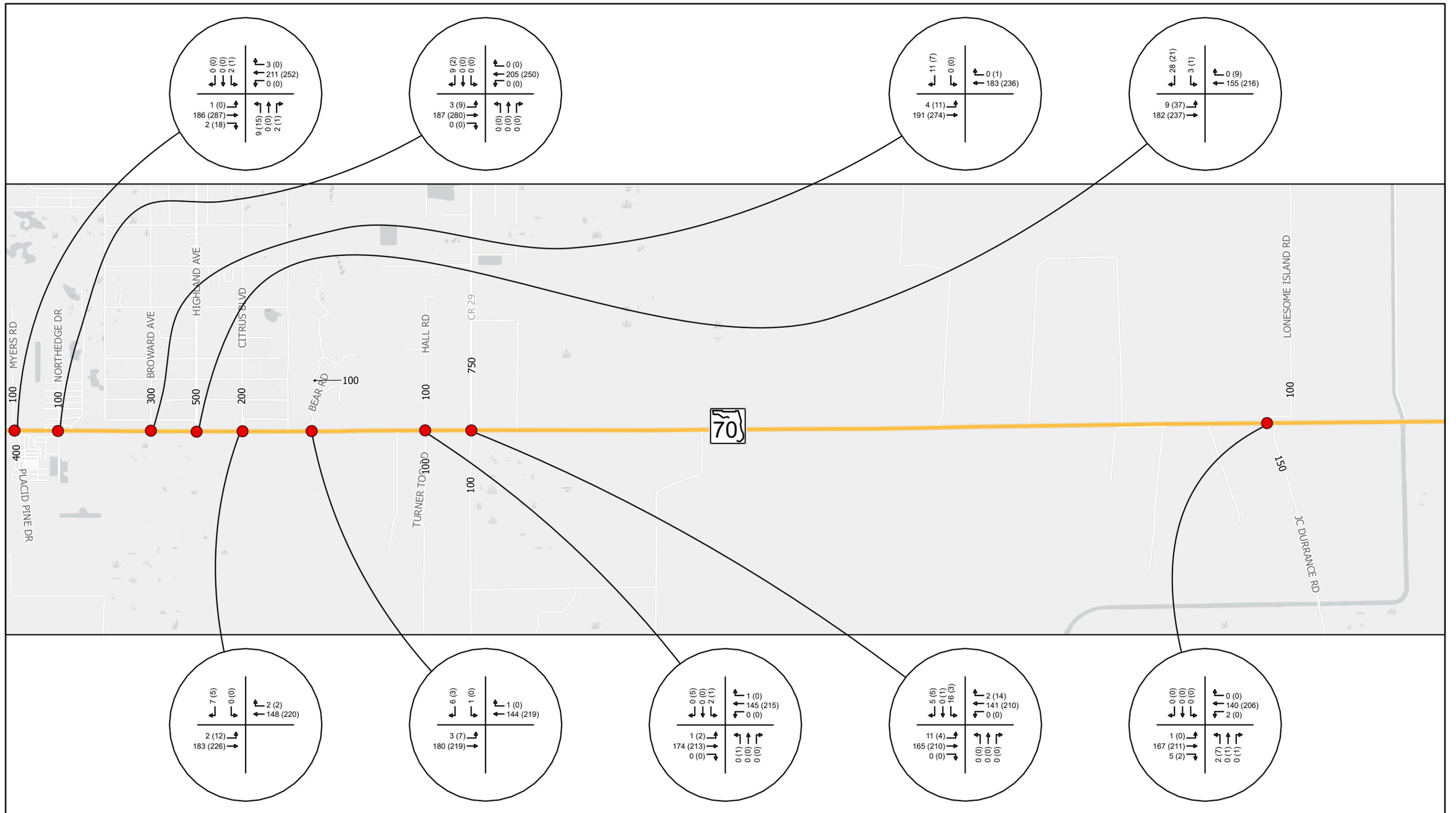


Figure 2-3: Existing Year (2022) AADT and AM (PM) Turning Movement Volumes
Sheet 2 of 5



Legend

- Project Limits
- Unsignalized (9)
- XX (XX) AM (PM) Peak Hour Volumes
- X,XXX AADT
- ↑↑↑ Turning Movements

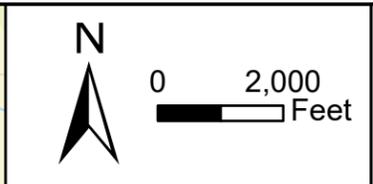
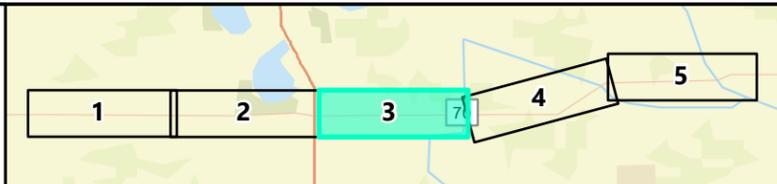
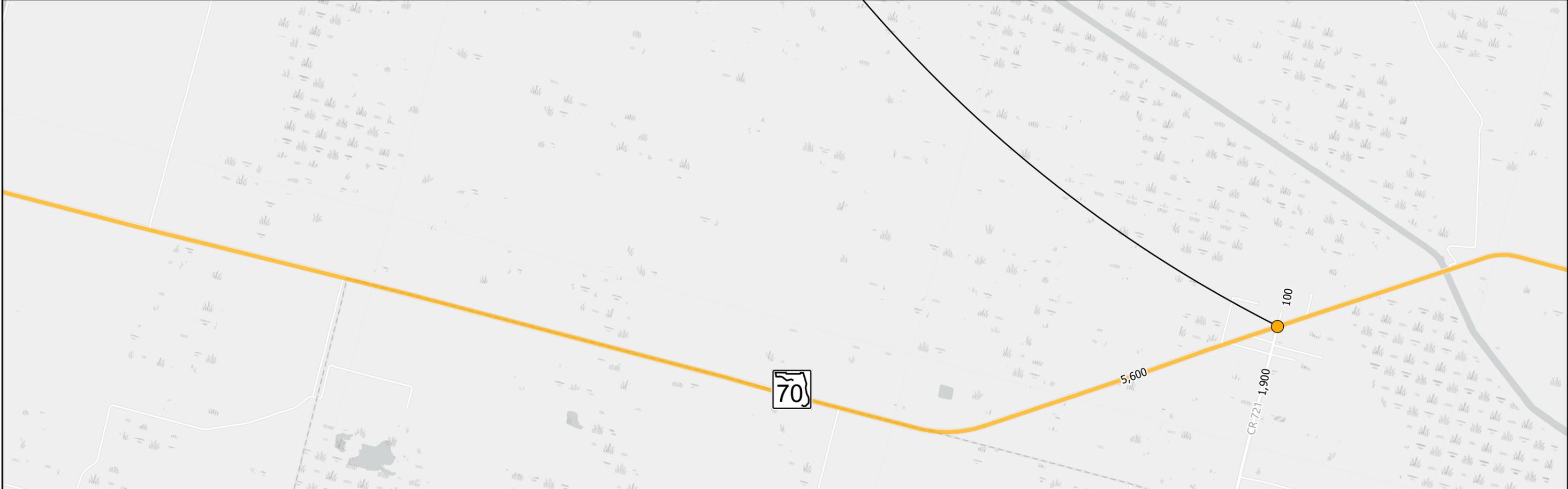
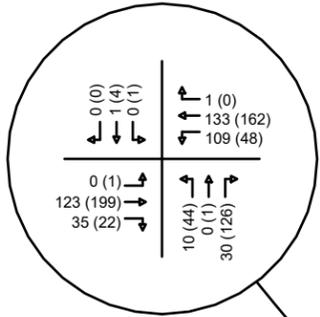


Figure 2-3: Existing Year (2022) AADT and AM (PM) Turning Movement Volumes
Sheet 3 of 5



Legend

- Project Limits
- Flashing Yellow (1)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- ↑↑↑ Turning Movements

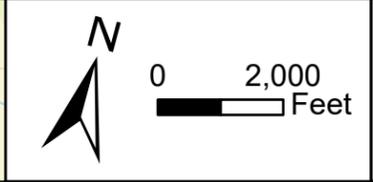
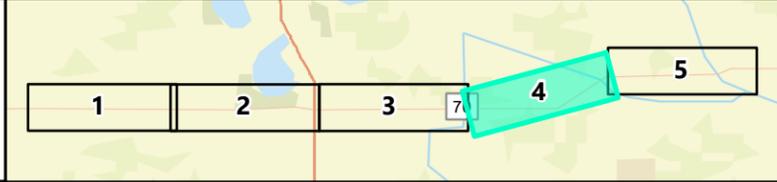
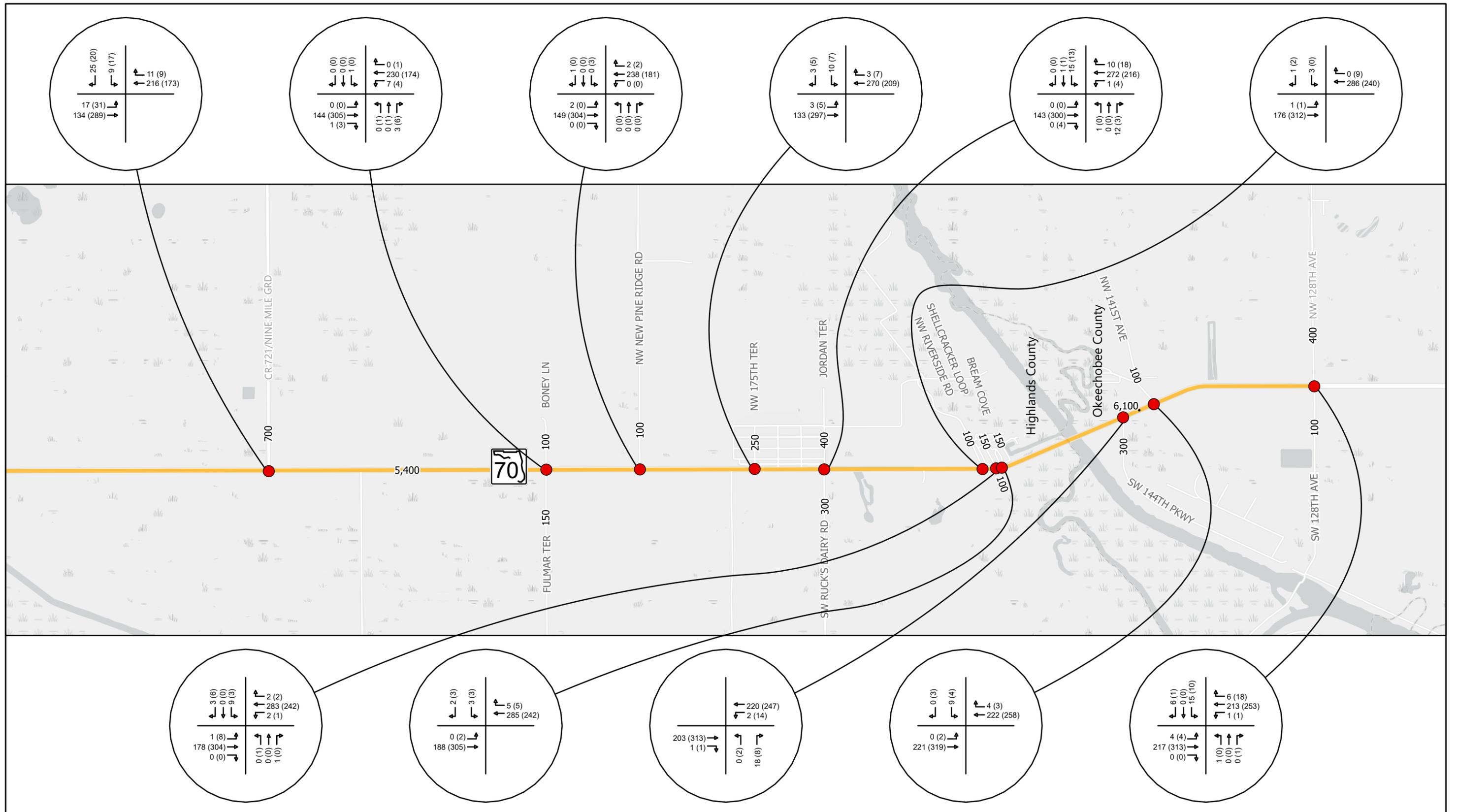


Figure 2-3: Existing Year (2022)
AADT and AM (PM) Turning
Movement Volumes
Sheet 4 of 5



Legend

- Project Limits
- Unsignalized (11)
- XX (XX) AM (PM) Peak Hour Volumes
- X,XXX AADT
- Turning Movements

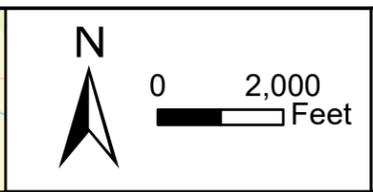
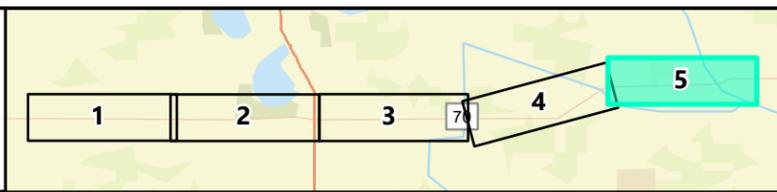


Figure 2-3: Existing Year (2022) AADT and AM (PM) Turning Movement Volumes
Sheet 5 of 5

2.3 Traffic Factors

The following subsections document the development and selection of the traffic factors used in the subsequent volume development and traffic analysis.

2.3.1 Directional Factors

Directional factors and accompanying peak directions were calculated and/or acquired for various locations within the study area based on data collected for this study and data available via FDOT’s Florida Traffic Online (FTO) Database (**Table 2-3**). These directional factors were compared to *Recommended D-Factors for Project Traffic Forecasting* (included as **Table 2-4**) from FDOT’s Project Traffic Forecasting Handbook to designate appropriate and realistic design-year directional factors. The selected D-factors and peak directions are listed in **Table 2-5**.

Table 2-3: Calculated Directional Factors

| SR 70 Intersection | Intersection Leg | FTO D-Factor | AM Peak Hour | | PM Peak Hour | |
|--------------------------------|----------------------------------|--------------|----------------|----------|----------------|----------|
| | | | Peak Direction | D-Factor | Peak Direction | D-Factor |
| Highlands County Line Road | East (SR 70) | - | WB | 65% | EB | 66% |
| | West (SR 70) | - | WB | 64% | EB | 65% |
| | South (Highlands County Line Rd) | - | SB | 57% | NB | 100% |
| Deer Run Road/Blue Head Street | East (SR 70) | - | WB | 65% | EB | 65% |
| | West (SR 70) | - | WB | 65% | EB | 66% |
| | North (Deer Run Road) | - | - | 0% | - | 0% |
| | South (Blue Head Street) | - | SB | 100% | SB | 60% |
| Robert McGee Road | East (SR 70) | - | WB | 66% | EB | 66% |
| | West (SR 70) | - | WB | 66% | EB | 65% |
| | North (Robert McGee Road) | - | - | 0% | SB | 80% |
| Lightsey Ranch Road | East (SR 70) | - | WB | 66% | EB | 65% |
| | West (SR 70) | - | WB | 66% | EB | 65% |
| | South (Lightsey Ranch Rd) | - | - | 50% | - | - |
| Placid Lakes Boulevard | East (SR 70) | - | WB | 57% | EB | 58% |
| | West (SR 70) | 60.2% | WB | 66% | EB | 65% |
| | North (Placid Lakes Blvd) | 60.5% | SB | 85% | NB | 72% |
| | South (Jefferson Ave) | - | NB | 73% | SB | 52% |
| Park Land Drive | East (SR 70) | - | WB | 55% | EB | 57% |
| | West (SR 70) | - | WB | 57% | EB | 58% |
| | South (Park Land Dr) | - | NB | 92% | SB | 67% |
| Placid View Drive | East (SR 70) | - | WB | 54% | EB | 55% |
| | West (SR 70) | - | WB | 56% | EB | 58% |
| | North (Placid View Dr) | 60.5% | SB | 59% | NB | 82% |
| Old SR 8 North | East (SR 70) | - | EB | 52% | WB | 52% |
| | West (SR 70) | - | WB | 54% | EB | 54% |
| | North (Old SR 8) | 60.5% | SB | 66% | NB | 68% |

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| SR 70 Intersection | Intersection Leg | FTO D-Factor | AM Peak Hour | | PM Peak Hour | |
|-------------------------------|-----------------------------|--------------|----------------|----------|----------------|----------|
| | | | Peak Direction | D-Factor | Peak Direction | D-Factor |
| Old SR 8 South | East (SR 70) | - | WB | 55% | EB | 55% |
| | West (SR 70) | - | EB | 52% | WB | 52% |
| | South (Old SR 8) | 60.5% | SB | 67% | NB | 69% |
| Distribution Boulevard | East (SR 70) | - | WB | 57% | EB | 57% |
| | West (SR 70) | - | WB | 55% | EB | 55% |
| | South (Distribution Blvd) | - | SB | 76% | NB | 100% |
| Glades Driveway | East (SR 70) | - | WB | 57% | EB | 57% |
| | West (SR 70) | - | WB | 57% | EB | 57% |
| | North (Glades Driveway) | - | NB | 56% | SB | 59% |
| Wedgeworth Driveway | East (SR 70) | - | WB | 56% | EB | 58% |
| | West (SR 70) | - | WB | 57% | EB | 57% |
| | South (Wedgeworth Driveway) | - | NB | 63% | NB | 78% |
| US 27 | East (SR 70) | 60.2% | WB | 54% | EB | 53% |
| | West (SR 70) | 60.2% | WB | 57% | EB | 53% |
| | North (US 27) | 61.2% | SB | 57% | NB | 58% |
| | South (US 27) | 61.1% | SB | 55% | NB | 59% |
| Myers Road/Placid Pines Drive | East (SR 70) | - | WB | 53% | EB | 53% |
| | West (SR 70) | - | WB | 54% | EB | 53% |
| | North (Myers Rd) | - | NB | 67% | SB | 100% |
| | South (Placid Pines Dr) | - | NB | 85% | SB | 53% |
| Northedge Drive | East (SR 70) | - | WB | 52% | EB | 53% |
| | West (SR 70) | - | WB | 53% | EB | 53% |
| | North (North Edge Dr) | - | SB | 75% | NB | 82% |
| Broward Avenue | East (SR 70) | - | EB | 51% | EB | 54% |
| | West (SR 70) | - | EB | 50% | EB | 54% |
| | North (Broward Ave) | - | SB | 73% | NB | 63% |
| Highlands Boulevard | East (SR 70) | - | EB | 54% | EB | 51% |
| | West (SR 70) | - | EB | 51% | EB | 54% |
| | North (Highlands Blvd) | - | SB | 78% | NB | 68% |
| Citrus Boulevard | East (SR 70) | - | EB | 55% | EB | 50% |
| | West (SR 70) | - | EB | 54% | EB | 51% |
| | North (Citrus Blvd) | - | SB | 64% | NB | 74% |
| Bear Road | East (SR 70) | - | EB | 56% | - | 50% |
| | West (SR 70) | - | EB | 55% | EB | 50% |
| | North (Bear Rd) | - | SB | 64% | NB | 70% |
| Hall Road/Turner Too Road | East (SR 70) | - | EB | 55% | WB | 50% |
| | West (SR 70) | - | EB | 55% | WB | 51% |
| | North (Hall Rd) | - | - | 50% | SB | 75% |
| | South (Turner Too Rd) | - | - | - | NB | 100% |

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| SR 70 Intersection | Intersection Leg | FTO D-Factor | AM Peak Hour | | PM Peak Hour | |
|---------------------------------------|------------------------------|--------------|----------------|----------|----------------|----------|
| | | | Peak Direction | D-Factor | Peak Direction | D-Factor |
| CR 29/KW Farms Road | East (SR 70) | - | EB | 56% | WB | 51% |
| | West (SR 70) | - | EB | 55% | WB | 50% |
| | North (CR 29) | 60.5% | SB | 62% | NB | 67% |
| | South (KW Farms Rd) | - | - | - | SB | 100% |
| Lonesome Island Road/JC Durrance Road | East (SR 70) | - | EB | 54% | EB | 51% |
| | West (SR 70) | - | EB | 55% | - | 50% |
| | North (Lonesome Island Road) | - | NB | 100% | NB | 100% |
| | South (JC Durrance Road) | - | SB | 78% | NB | 82% |
| CR 721 South | East (SR 70) | - | WB | 61% | EB | 61% |
| | West (SR 70) | - | EB | 52% | EB | 52% |
| | North (Driveway) | 60.5% | - | 50% | SB | 71% |
| | South (CR 721) | - | SB | 78% | NB | 70% |
| CR 721 North | East (SR 70) | 60.2% | WB | 61% | EB | 63% |
| | West (SR 70) | - | WB | 61% | EB | 62% |
| | North (CR 721) | 60.5% | SB | 55% | NB | 52% |
| Boney Lane/Fulmar Terrace | East (SR 70) | - | WB | 62% | EB | 63% |
| | West (SR 70) | - | WB | 61% | EB | 64% |
| | North (Boney Lane) | - | SB | 100% | NB | 100% |
| | South (Fulmar Terr) | - | SB | 73% | NB | 53% |
| NW New Pine Ridge Road | East (SR 70) | - | WB | 62% | EB | 63% |
| | West (SR 70) | - | WB | 61% | EB | 63% |
| | North (New Pine Ridge Rd) | - | NB | 80% | SB | 60% |
| 175th Terrace | East (SR 70) | - | WB | 66% | EB | 58% |
| | West (SR 70) | - | WB | 67% | EB | 58% |
| | North (175th Terr) | - | SB | 68% | - | 50% |
| 172nd Terrace/SW Rucks Dairy Road | East (SR 70) | - | WB | 63% | EB | 57% |
| | West (SR 70) | - | WB | 66% | EB | 58% |
| | North (172nd Terr) | - | SB | 62% | NB | 56% |
| | South (SW Rucks Dairy Rd) | - | NB | 87% | SB | 75% |
| Riverside Road | East (SR 70) | - | WB | 62% | EB | 56% |
| | West (SR 70) | - | WB | 63% | EB | 57% |
| | North (Riverside Rd) | - | SB | 80% | NB | 83% |
| Shellcracker Loop | East (SR 70) | - | WB | 60% | EB | 56% |
| | West (SR 70) | - | WB | 61% | EB | 56% |
| | North (Shellcracker Loop) | - | SB | 80% | NB | 53% |
| | South (Driveway) | - | SB | 67% | - | 50% |
| Bream Cove | East (SR 70) | - | WB | 60% | EB | 55% |
| | West (SR 70) | - | WB | 60% | EB | 56% |
| | North (Bream Cove) | - | - | 50% | NB | 54% |

| SR 70 Intersection | Intersection Leg | FTO D-Factor | AM Peak Hour | | PM Peak Hour | |
|--------------------|----------------------|--------------|----------------|----------|----------------|----------|
| | | | Peak Direction | D-Factor | Peak Direction | D-Factor |
| 144th Parkway | East (SR 70) | - | WB | 51% | EB | 55% |
| | West (SR 70) | 58.0% | WB | 53% | EB | 56% |
| | South (144th Pkwy) | - | NB | 86% | SB | 60% |
| 141st Avenue | East (SR 70) | - | EB | 51% | EB | 55% |
| | West (SR 70) | - | WB | 51% | EB | 55% |
| | North (141st Ave) | - | SB | 69% | SB | 58% |
| NW 128th Avenue | East (SR 70) | - | EB | 51% | EB | 54% |
| | West (SR 70) | - | EB | 50% | EB | 56% |
| | North (NW 128th Ave) | 58.0% | SB | 68% | NB | 67% |
| | South (SW 128th Ave) | - | - | 50% | - | 50% |

Table 2-4: Recommended D-Factors for Project Traffic Forecasting (FDOT)

| Road Type | Low | D | High | Standard Deviation |
|----------------|------|------|------|--------------------|
| Rural Freeway | 52.3 | 54.8 | 57.3 | 1.73 |
| Rural Arterial | 51.1 | 58.1 | 79.6 | 6.29 |
| Urban Freeway | 50.4 | 55.8 | 61.2 | 4.11 |
| Urban Arterial | 50.8 | 57.9 | 67.1 | 4.60 |

Table 2-5: Selected D-Factors

| SR 70 Intersection | Intersection Leg | Selected D-Factor | AM Direction | PM Direction |
|--------------------------------|----------------------------------|-------------------|--------------|--------------|
| Highlands County Line Road | East (SR 70) | 58.0% | WB | WB |
| | West (SR 70) | 58.0% | WB | EB |
| | South (Highlands County Line Rd) | 60.0% | SB | NB |
| Deer Run Road/Blue Head Street | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Deer Run Road) | 60.0% | - | - |
| | South (Blue Head Street) | 60.0% | SB | SB |
| Robert McGee Road | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Robert McGee Road) | 60.0% | - | SB |
| Lightsey Ranch Road | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | South (Lightsey Ranch Rd) | 60.0% | - | - |
| Placid Lakes Boulevard | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Placid Lakes Blvd) | 75.0% | SB | NB |
| | South (Jefferson Ave) | 60.0% | NB | SB |

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| SR 70 Intersection | Intersection Leg | Selected D-Factor | AM Direction | PM Direction |
|-------------------------------|-----------------------------|-------------------|--------------|--------------|
| Park Land Drive | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | South (Park Land Dr) | 75.0% | NB | SB |
| Placid View Drive | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Placid View Dr) | 70.0% | SB | NB |
| Old SR 8 North | East (SR 70) | 58.0% | EB | WB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Old SR 8) | 70.0% | SB | NB |
| Old SR 8 South | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | EB | WB |
| | South (Old SR 8) | 70.0% | SB | NB |
| Distribution Boulevard | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | South (Distribution Blvd) | 75.0% | SB | NB |
| Glades Driveway | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Glades Driveway) | 60.0% | NB | SB |
| Wedgeworth Driveway | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | South (Wedgeworth Driveway) | 70.0% | NB | NB |
| US 27 | East (SR 70) | 53.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (US 27) | 60.0% | SB | NB |
| | South (US 27) | 60.0% | SB | NB |
| Myers Road/Placid Pines Drive | East (SR 70) | 53.0% | WB | EB |
| | West (SR 70) | 53.0% | WB | EB |
| | North (Myers Rd) | 75.0% | NB | SB |
| | South (Placid Pines Dr) | 70.0% | NB | SB |
| Northedge Drive | East (SR 70) | 53.0% | WB | EB |
| | West (SR 70) | 53.0% | WB | EB |
| | North (North Edge Dr) | 75.0% | SB | NB |
| Broward Avenue | East (SR 70) | 53.0% | EB | EB |
| | West (SR 70) | 53.0% | EB | EB |
| | North (Broward Ave) | 70.0% | SB | NB |
| Highlands Boulevard | East (SR 70) | 53.0% | EB | EB |
| | West (SR 70) | 53.0% | EB | EB |
| | North (Highlands Blvd) | 75.0% | SB | NB |
| Citrus Boulevard | East (SR 70) | 53.0% | EB | EB |
| | West (SR 70) | 53.0% | EB | EB |
| | North (Citrus Blvd) | 70.0% | SB | NB |

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| SR 70 Intersection | Intersection Leg | Selected D-Factor | AM Direction | PM Direction |
|---------------------------------------|------------------------------|-------------------|--------------|--------------|
| Bear Road | East (SR 70) | 53.0% | EB | - |
| | West (SR 70) | 53.0% | EB | EB |
| | North (Bear Rd) | 65.0% | SB | NB |
| Hall Road/Turner Too Road | East (SR 70) | 53.0% | EB | WB |
| | West (SR 70) | 53.0% | EB | WB |
| | North (Hall Rd) | 65.0% | - | SB |
| | South (Turner Too Rd) | 70.0% | - | NB |
| CR 29/KW Farms Road | East (SR 70) | 53.0% | EB | WB |
| | West (SR 70) | 53.0% | EB | WB |
| | North (CR 29) | 65.0% | SB | NB |
| | South (KW Farms Rd) | 70.0% | - | SB |
| Lonesome Island Road/JC Durrance Road | East (SR 70) | 55.0% | EB | EB |
| | West (SR 70) | 53.0% | EB | - |
| | North (Lonesome Island Road) | 70.0% | NB | NB |
| | South (JC Durrance Road) | 70.0% | SB | NB |
| CR 721 South | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 55.0% | EB | EB |
| | North (Driveway) | 60.0% | - | SB |
| | South (CR 721) | 70.0% | SB | NB |
| CR 721 North | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (CR 721) | 60.0% | SB | NB |
| Boney Lane/Fulmar Terrace | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Boney Lane) | 70.0% | SB | NB |
| | South (Fulmar Terr) | 60.0% | SB | NB |
| NW New Pine Ridge Road | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (New Pine Ridge Rd) | 60.0% | NB | SB |
| 175th Terrace | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (175th Terr) | 60.0% | SB | - |
| 172nd Terrace/SW Rucks Dairy Road | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (172nd Terr) | 60.0% | SB | NB |
| | South (SW Rucks Dairy Rd) | 70.0% | NB | SB |
| Riverside Road | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Riverside Rd) | 70.0% | SB | NB |

| SR 70 Intersection | Intersection Leg | Selected D-Factor | AM Direction | PM Direction |
|--------------------|---------------------------|-------------------|--------------|--------------|
| Shellcracker Loop | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Shellcracker Loop) | 60.0% | SB | NB |
| | South (Driveway) | 60.0% | SB | - |
| Bream Cove | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (Bream Cove) | 55.0% | - | NB |
| 144th Parkway | East (SR 70) | 58.0% | WB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | South (144th Pkwy) | 70.0% | NB | SB |
| 141st Avenue | East (SR 70) | 58.0% | EB | EB |
| | West (SR 70) | 58.0% | WB | EB |
| | North (141st Ave) | 60.0% | SB | SB |
| NW 128th Avenue | East (SR 70) | 58.0% | EB | EB |
| | West (SR 70) | 58.0% | EB | EB |
| | North (NW 128th Ave) | 70.0% | SB | NB |
| | South (SW 128th Ave) | 60.0% | - | - |

2.3.2 Truck Factors

Hourly and daily truck factors were gathered from counts conducted for this study, including the four-hour turning movement count (TMC) data and class count data, as well as from FTO. These truck factors were used to select hourly truck factors for the study roadways for the subsequent traffic analysis. Daily truck factors were selected for each roadway segment based on a review of FTO data, project classification counts, and TMC truck percentages during the peak periods (where no other data was available). More consideration was given to FTO data and classification count data. In locations where only TMC data was available, approximate average peak period truck percentages were calculated and then rounded. Design hour truck percentages are estimated to be half of the daily truck percentage. The measured and selected truck factors are listed in **Table 2-6**. The count data and information from FTO are included in **Appendix B**.

Table 2-6: Truck Factors

| SR 70 Intersection | Intersection Leg | AM Hourly T-Factor (Measured) | PM Hourly T-Factor (Measured) | Daily T-Factor (from FTO) | Hourly T-Factor (Selected) | Daily T-Factor (Selected) |
|----------------------------|----------------------------------|-------------------------------|-------------------------------|---------------------------|----------------------------|---------------------------|
| Highlands County Line Road | East (SR 70) | 24% | 13% | - | 16.0% | 32% |
| | West (SR 70) | 33% | 10% | - | 16.0% | 32% |
| | South (Highlands County Line Rd) | 67% | 0% | - | 15.0% | 30% |

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| SR 70 Intersection | Intersection Leg | AM Hourly T-Factor (Measured) | PM Hourly T-Factor (Measured) | Daily T-Factor (from FTO) | Hourly T-Factor (Selected) | Daily T-Factor (Selected) |
|--------------------------------|-----------------------------|-------------------------------|-------------------------------|---------------------------|----------------------------|---------------------------|
| Deer Run Road/Blue Head Street | East (SR 70) | 25% | 20% | - | 16.0% | 32% |
| | West (SR 70) | 36% | 10% | - | 16.0% | 32% |
| | North (Deer Run Road) | - | - | - | 15.0% | 30% |
| | South (Blue Head Street) | - | 0% | - | 15.0% | 30% |
| Robert McGee Road | East (SR 70) | 23% | 10% | - | 16.0% | 32% |
| | West (SR 70) | 33% | 13% | - | 16.0% | 32% |
| | North (Robert McGee Road) | - | 0% | - | 15.0% | 30% |
| Lightsey Ranch Road | East (SR 70) | 22% | 10% | - | 16.0% | 32% |
| | West (SR 70) | 32% | 13% | - | 16.0% | 32% |
| | South (Lightsey Ranch Rd) | 0% | 0% | - | 2.5% | 5% |
| Placid Lakes Boulevard | East (SR 70) | 26% | 8% | - | 16.0% | 32% |
| | West (SR 70) | 32% | 12% | 35% | 16.0% | 32% |
| | North (Placid Lakes Blvd) | 2% | 3% | 15% | 7.5% | 15% |
| | South (Jefferson Ave) | 9% | 18% | - | 7.5% | 15% |
| Park Land Drive | East (SR 70) | 25% | 9% | - | 16.0% | 32% |
| | West (SR 70) | 24% | 14% | - | 16.0% | 32% |
| | South (Park Land Dr) | 17% | 11% | - | 10.0% | 20% |
| Placid View Drive | East (SR 70) | 24% | 9% | - | 16.0% | 32% |
| | West (SR 70) | 24% | 13% | - | 16.0% | 32% |
| | North (Placid View Dr) | 5% | 0% | 15% | 7.5% | 15% |
| Old SR 8 North | East (SR 70) | 27% | 9% | - | 16.0% | 32% |
| | West (SR 70) | 22% | 14% | - | 16.0% | 32% |
| | North (Old SR 8) | 1% | 18% | 15% | 7.5% | 15% |
| Old SR 8 South | East (SR 70) | 26% | 10% | - | 16.0% | 32% |
| | West (SR 70) | 17% | 18% | - | 16.0% | 32% |
| | South (Old SR 8) | 16% | 9% | 15% | 7.5% | 15% |
| Distribution Boulevard | East (SR 70) | 25% | 10% | - | 16.0% | 32% |
| | West (SR 70) | 25% | 15% | - | 16.0% | 32% |
| | South (Distribution Blvd) | 71% | 25% | - | 40.0% | 80% |
| Glades Driveway | East (SR 70) | 25% | 12% | - | 16.0% | 32% |
| | West (SR 70) | 26% | 16% | - | 16.0% | 32% |
| | North (Glades Driveway) | 29% | 0% | - | 15.0% | 30% |
| Wedgeworth Driveway | East (SR 70) | 24% | 12% | - | 16.0% | 32% |
| | West (SR 70) | 26% | 15% | - | 16.0% | 32% |
| | South (Wedgeworth Driveway) | 60% | 0% | - | 30.0% | 60% |
| US 27 | East (SR 70) | 15% | 10% | 24% | 16.0% | 32% |
| | West (SR 70) | 24% | 16% | 32% | 16.0% | 32% |
| | North (US 27) | 24% | 20% | 35% | 16.5% | 33% |
| | South (US 27) | 34% | 18% | 30% | 16.5% | 33% |

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| SR 70 Intersection | Intersection Leg | AM Hourly T-Factor (Measured) | PM Hourly T-Factor (Measured) | Daily T-Factor (from FTO) | Hourly T-Factor (Selected) | Daily T-Factor (Selected) |
|---------------------------------------|------------------------------|-------------------------------|-------------------------------|---------------------------|----------------------------|---------------------------|
| Myers Road/Placid Pines Drive | East (SR 70) | 24% | 15% | - | 16.0% | 32% |
| | West (SR 70) | 21% | 13% | - | 16.0% | 32% |
| | North (Myers Rd) | 0% | 0% | - | 2.5% | 5% |
| | South (Placid Pines Dr) | 0% | 0% | - | 2.5% | 5% |
| Northedge Drive | East (SR 70) | 25% | 15% | - | 16.0% | 32% |
| | West (SR 70) | 21% | 15% | - | 16.0% | 32% |
| | North (North Edge Dr) | 11% | 0% | - | 5.0% | 10% |
| Broward Avenue | East (SR 70) | 26% | 15% | - | 16.0% | 32% |
| | West (SR 70) | 20% | 15% | - | 16.0% | 32% |
| | North (Broward Ave) | 9% | 0% | - | 5.0% | 10% |
| Highlands Boulevard | East (SR 70) | 30% | 15% | - | 16.0% | 32% |
| | West (SR 70) | 21% | 15% | - | 16.0% | 32% |
| | North (Highlands Blvd) | 3% | 5% | - | 4.0% | 8% |
| Citrus Boulevard | East (SR 70) | 31% | 15% | - | 16.0% | 32% |
| | West (SR 70) | 21% | 17% | - | 16.0% | 32% |
| | North (Citrus Blvd) | 0% | 0% | - | 2.5% | 5% |
| Bear Road | East (SR 70) | 31% | 15% | - | 16.0% | 32% |
| | West (SR 70) | 21% | 17% | - | 16.0% | 32% |
| | North (Bear Rd) | 0% | 0% | - | 2.5% | 5% |
| Hall Road/Turner Too Road | East (SR 70) | 33% | 16% | - | 16.0% | 32% |
| | West (SR 70) | 22% | 18% | - | 16.0% | 32% |
| | North (Hall Rd) | 50% | 0% | - | 15.0% | 30% |
| | South (Turner Too Rd) | 0% | 0% | - | 2.5% | 5% |
| CR 29/KW Farms Road | East (SR 70) | 33% | 15% | - | 16.0% | 32% |
| | West (SR 70) | 24% | 18% | - | 16.0% | 32% |
| | North (CR 29) | 5% | 0% | 15% | 7.5% | 15% |
| | South (KW Farms Rd) | 0% | 0% | - | 2.5% | 5% |
| Lonesome Island Road/JC Durrance Road | East (SR 70) | 30% | 14% | - | 16.0% | 32% |
| | West (SR 70) | 16% | 18% | - | 16.0% | 32% |
| | North (Lonesome Island Road) | - | - | - | 15.0% | 30% |
| | South (JC Durrance Road) | 50% | 0% | - | 15.0% | 30% |
| CR 721 South | East (SR 70) | 19% | 15% | - | 12.5% | 25% |
| | West (SR 70) | 17% | 20% | - | 16.0% | 32% |
| | North (Driveway) | 0% | 0% | - | 7.5% | 15% |
| | South (CR 721) | 0% | 2% | 15% | 7.5% | 15% |
| CR 721 North | East (SR 70) | 17% | 12% | 25% | 12.5% | 25% |
| | West (SR 70) | 17% | 17% | - | 12.5% | 25% |
| | North (CR 721) | 12% | 16% | 15% | 7.5% | 15% |

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| SR 70 Intersection | Intersection Leg | AM Hourly T-Factor (Measured) | PM Hourly T-Factor (Measured) | Daily T-Factor (from FTO) | Hourly T-Factor (Selected) | Daily T-Factor (Selected) |
|-----------------------------------|---------------------------|-------------------------------|-------------------------------|---------------------------|----------------------------|---------------------------|
| Boney Lane/Fulmar Terrace | East (SR 70) | 16% | 12% | - | 12.5% | 25% |
| | West (SR 70) | 17% | 15% | - | 12.5% | 25% |
| | North (Boney Lane) | 0% | - | - | 7.5% | 15% |
| | South (Fulmar Terr) | 0% | 0% | - | 7.5% | 15% |
| NW New Pine Ridge Road | East (SR 70) | 16% | 13% | - | 12.5% | 25% |
| | West (SR 70) | 17% | 15% | - | 12.5% | 25% |
| | North (New Pine Ridge Rd) | 0% | 0% | - | 12.5% | 25% |
| 175th Terrace | East (SR 70) | 12% | 12% | - | 12.5% | 25% |
| | West (SR 70) | 16% | 15% | - | 12.5% | 25% |
| | North (175th Terr) | 8% | 0% | - | 5.0% | 10% |
| 172nd Terrace/SW Rucks Dairy Road | East (SR 70) | 12% | 11% | - | 12.5% | 25% |
| | West (SR 70) | 16% | 15% | - | 12.5% | 25% |
| | North (172nd Terr) | 6% | 7% | - | 5.0% | 10% |
| | South (SW Rucks Dairy Rd) | 8% | 0% | - | 7.5% | 15% |
| Riverside Road | East (SR 70) | 12% | 11% | - | 12.5% | 25% |
| | West (SR 70) | 14% | 14% | - | 12.5% | 25% |
| | North (Riverside Rd) | 25% | 0% | - | 5.0% | 10% |
| Shellcracker Loop | East (SR 70) | 12% | 10% | - | 12.5% | 25% |
| | West (SR 70) | 15% | 15% | - | 12.5% | 25% |
| | North (Shellcracker Loop) | 0% | 0% | - | 5.0% | 10% |
| | South (Driveway) | 0% | 0% | - | 5.0% | 10% |
| Bream Cove | East (SR 70) | 12% | 10% | - | 12.5% | 25% |
| | West (SR 70) | 14% | 15% | - | 12.5% | 25% |
| | North (Bream Cove) | 20% | 0% | - | 5.0% | 10% |
| 144th Parkway | East (SR 70) | 14% | 10% | - | 12.5% | 25% |
| | West (SR 70) | 14% | 15% | 24% | 12.5% | 25% |
| | South (144th Pkwy) | 0% | 30% | - | 5.0% | 10% |
| 141 st Avenue | East (SR 70) | 12% | 10% | - | 12.5% | 25% |
| | West (SR 70) | 13% | 15% | - | 12.5% | 25% |
| | North (141st Ave) | 0% | 0% | - | 5.0% | 10% |
| NW 128th Avenue | East (SR 70) | 12% | 11% | - | 12.5% | 25% |
| | West (SR 70) | 13% | 16% | - | 12.5% | 25% |
| | North (NW 128th Ave) | 5% | 9% | 27% | 12.5% | 25% |
| | South (SW 128th Ave) | 0% | 0% | - | 10% | 20% |

2.3.3 K Factors

Peak hour-to-daily volume ratios (K factors) were evaluated based on the existing traffic volumes. These K factors and the standard K factor of 9.5 (from the FDOT Project Traffic Forecasting Handbook) were considered in the selection of K factors for traffic forecasting purposes, as documented in **Table 2-7**.

Table 2-7: K Factors

| SR 70 Intersection | Intersection Leg | AM K-Factor (Calculated) | PM K-Factor (Calculated) | K-Factor (Selected) |
|--------------------------------|----------------------------------|--------------------------|--------------------------|---------------------|
| Highlands County Line Road | East (SR 70) | 7.5% | 7.8% | 9.5% |
| | West (SR 70) | 6.6% | 6.8% | 9.5% |
| | South (Highlands County Line Rd) | - | - | 9.5% |
| Deer Run Road/Blue Head Street | East (SR 70) | 8.3% | 8.8% | 9.5% |
| | West (SR 70) | 7.5% | 7.8% | 9.5% |
| | North (Deer Run Road) | - | - | 9.5% |
| | South (Blue Head Street) | - | - | 9.5% |
| Robert McGee Road | East (SR 70) | 6.9% | 9.1% | 9.5% |
| | West (SR 70) | 6.9% | 9.0% | 9.5% |
| | North (Robert McGee Road) | - | - | 9.5% |
| Lightsey Ranch Road | East (SR 70) | 7.2% | 9.1% | 9.5% |
| | West (SR 70) | 7.1% | 9.1% | 9.5% |
| | South (Lightsey Ranch Rd) | - | - | 9.5% |
| Placid Lakes Boulevard | East (SR 70) | 6.4% | 8.4% | 9.5% |
| | West (SR 70) | 7.2% | 9.1% | 9.5% |
| | North (Placid Lakes Blvd) | 8.1% | 12.2% | 9.5% |
| | South (Jefferson Ave) | - | - | 9.5% |
| Park Land Drive | East (SR 70) | 6.6% | 8.6% | 9.5% |
| | West (SR 70) | 6.4% | 8.4% | 9.5% |
| | South (Park Land Dr) | - | - | 9.5% |
| Placid View Drive | East (SR 70) | 6.8% | 8.9% | 9.5% |
| | West (SR 70) | 6.5% | 8.5% | 9.5% |
| | North (Placid View Dr) | 9.7% | 9.4% | 9.5% |
| Old SR 8 North | East (SR 70) | 6.9% | 9.4% | 9.5% |
| | West (SR 70) | 6.8% | 8.9% | 9.5% |
| | North (Old SR 8) | 13.2% | 14.2% | 9.5% |
| Old SR 8 South | East (SR 70) | 6.4% | 8.2% | 9.5% |
| | West (SR 70) | 6.9% | 9.4% | 9.5% |
| | South (Old SR 8) | 15.0% | 16.3% | 9.5% |
| Distribution Boulevard | East (SR 70) | 6.6% | 8.4% | 9.5% |
| | West (SR 70) | 6.4% | 8.2% | 9.5% |
| | South (Distribution Blvd) | - | - | 9.5% |

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| SR 70 Intersection | Intersection Leg | AM K-Factor (Calculated) | PM K-Factor (Calculated) | K-Factor (Selected) |
|-------------------------------|-----------------------------|--------------------------|--------------------------|---------------------|
| Glades Driveway | East (SR 70) | 6.6% | 8.8% | 9.5% |
| | West (SR 70) | 6.5% | 8.5% | 9.5% |
| | North (Glades Driveway) | - | - | 9.5% |
| Wedgeworth Driveway | East (SR 70) | 6.8% | 8.9% | 9.5% |
| | West (SR 70) | 6.6% | 8.8% | 9.5% |
| | South (Wedgeworth Driveway) | - | - | 9.5% |
| US 27 | East (SR 70) | 7.3% | 10.2% | 9.5% |
| | West (SR 70) | 8.2% | 10.5% | 9.5% |
| | North (US 27) | 6.1% | 8.2% | 9.5% |
| | South (US 27) | 6.1% | 8.3% | 9.5% |
| Myers Road/Placid Pines Drive | East (SR 70) | 7.2% | 9.7% | 9.5% |
| | West (SR 70) | 7.3% | 10.2% | 9.5% |
| | North (Myers Rd) | - | - | 9.5% |
| | South (Placid Pines Dr) | - | - | 9.5% |
| Northedge Drive | East (SR 70) | 7.0% | 9.5% | 9.5% |
| | West (SR 70) | 7.2% | 9.7% | 9.5% |
| | North (North Edge Dr) | - | - | 9.5% |
| Broward Avenue | East (SR 70) | 6.7% | 9.1% | 9.5% |
| | West (SR 70) | 6.9% | 9.4% | 9.5% |
| | North (Broward Ave) | - | - | 9.5% |
| Highlands Boulevard | East (SR 70) | 6.1% | 8.3% | 9.5% |
| | West (SR 70) | 6.7% | 9.1% | 9.5% |
| | North (Highlands Blvd) | - | - | 9.5% |
| Citrus Boulevard | East (SR 70) | 5.9% | 8.0% | 9.5% |
| | West (SR 70) | 6.1% | 8.3% | 9.5% |
| | North (Citrus Blvd) | - | - | 9.5% |
| Bear Road | East (SR 70) | 5.8% | 7.8% | 9.5% |
| | West (SR 70) | 5.9% | 8.0% | 9.5% |
| | North (Bear Rd) | - | - | 9.5% |
| Hall Road/Turner Too Road | East (SR 70) | 5.8% | 7.7% | 9.5% |
| | West (SR 70) | 5.7% | 7.8% | 9.5% |
| | North (Hall Rd) | - | - | 9.5% |
| | South (Turner Too Rd) | - | - | 9.5% |
| CR 29/KW Farms Road | East (SR 70) | 5.8% | 7.8% | 9.5% |
| | West (SR 70) | 5.8% | 7.7% | 9.5% |
| | North (CR 29) | 4.5% | 3.6% | 9.5% |
| | South (KW Farms Rd) | - | - | 9.5% |

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| SR 70 Intersection | Intersection Leg | AM K-Factor (Calculated) | PM K-Factor (Calculated) | K-Factor (Selected) |
|---------------------------------------|------------------------------|--------------------------|--------------------------|---------------------|
| Lonesome Island Road/JC Durrance Road | East (SR 70) | 5.5% | 7.5% | 9.5% |
| | West (SR 70) | 5.6% | 7.6% | 9.5% |
| | North (Lonesome Island Road) | - | - | 9.5% |
| | South (JC Durrance Road) | - | - | 9.5% |
| CR 721 South | East (SR 70) | 7.3% | 9.9% | 9.5% |
| | West (SR 70) | 5.4% | 7.6% | 9.5% |
| | North (Driveway) | - | - | 9.5% |
| | South (CR 721) | 9.7% | 12.9% | 9.5% |
| CR 721 North | East (SR 70) | 6.9% | 9.0% | 9.5% |
| | West (SR 70) | 7.0% | 9.2% | 9.5% |
| | North (CR 721) | 8.7% | 10.8% | 9.5% |
| Boney Lane/Fulmar Terrace | East (SR 70) | 7.1% | 9.1% | 9.5% |
| | West (SR 70) | 6.7% | 8.6% | 9.5% |
| | North (Boney Lane) | - | - | 9.5% |
| | South (Fulmar Terr) | - | - | 9.5% |
| NW New Pine Ridge Road | East (SR 70) | 7.2% | 9.1% | 9.5% |
| | West (SR 70) | 7.0% | 8.7% | 9.5% |
| | North (New Pine Ridge Rd) | - | - | 9.5% |
| 175th Terrace | East (SR 70) | 7.7% | 9.6% | 9.5% |
| | West (SR 70) | 7.3% | 9.2% | 9.5% |
| | North (175th Terr) | - | - | 9.5% |
| 172nd Terrace/SW Rucks Dairy Road | East (SR 70) | 8.4% | 10.3% | 9.5% |
| | West (SR 70) | 7.4% | 9.3% | 9.5% |
| | North (172nd Terr) | - | - | 9.5% |
| | South (SW Rucks Dairy Rd) | - | - | 9.5% |
| Riverside Road | East (SR 70) | 8.6% | 10.4% | 9.5% |
| | West (SR 70) | 8.3% | 9.9% | 9.5% |
| | North (Riverside Rd) | - | - | 9.5% |
| Shellcracker Loop | East (SR 70) | 8.8% | 10.2% | 9.5% |
| | West (SR 70) | 8.3% | 10.0% | 9.5% |
| | North (Shellcracker Loop) | - | - | 9.5% |
| | South (Driveway) | - | - | 9.5% |
| Bream Cove | East (SR 70) | 8.9% | 10.3% | 9.5% |
| | West (SR 70) | 8.5% | 9.9% | 9.5% |
| | North (Bream Cove) | - | - | 9.5% |
| 144th Parkway | East (SR 70) | 7.3% | 9.5% | 9.5% |
| | West (SR 70) | 7.9% | 10.4% | 9.5% |
| | South (144th Pkwy) | - | - | 9.5% |

| SR 70 Intersection | Intersection Leg | AM K-Factor (Calculated) | PM K-Factor (Calculated) | K-Factor (Selected) |
|--------------------------|----------------------|--------------------------|--------------------------|---------------------|
| 141 st Avenue | East (SR 70) | 7.5% | 9.6% | 9.5% |
| | West (SR 70) | 7.3% | 9.5% | 9.5% |
| | North (141st Ave) | - | - | 9.5% |
| NW 128th Avenue | East (SR 70) | 7.4% | 9.8% | 9.5% |
| | West (SR 70) | 7.2% | 9.4% | 9.5% |
| | North (NW 128th Ave) | 7.6% | 8.0% | 9.5% |
| | South (SW 128th Ave) | - | - | 9.5% |

2.3.4 Selected Traffic Factors

Table 2-8 below summarizes the selected traffic factors for each roadway segment in the study area.

Table 2-8: Selected Traffic Factors

| SR 70 Intersection | Intersection Leg | D-Factor | AM Direction | PM Direction | Hourly T-Factor | K-Factor |
|--------------------------------|----------------------------------|----------|--------------|--------------|-----------------|----------|
| Highlands County Line Road | East (SR 70) | 58.0% | WB | WB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | South (Highlands County Line Rd) | 60.0% | SB | NB | 15.0% | 9.5% |
| Deer Run Road/Blue Head Street | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | North (Deer Run Road) | 60.0% | - | - | 15.0% | 9.5% |
| | South (Blue Head Street) | 60.0% | SB | SB | 15.0% | 9.5% |
| Robert McGee Road | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | North (Robert McGee Road) | 60.0% | - | SB | 15.0% | 9.5% |
| Lightsey Ranch Road | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | South (Lightsey Ranch Rd) | 60.0% | - | - | 2.5% | 9.5% |
| Placid Lakes Boulevard | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | North (Placid Lakes Blvd) | 75.0% | SB | NB | 7.5% | 9.5% |
| | South (Jefferson Ave) | 60.0% | NB | SB | 7.5% | 9.5% |
| Park Land Drive | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | South (Park Land Dr) | 75.0% | NB | SB | 10.0% | 9.5% |
| Placid View Drive | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | North (Placid View Dr) | 70.0% | SB | NB | 7.5% | 9.5% |

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| SR 70 Intersection | Intersection Leg | D-Factor | AM Direction | PM Direction | Hourly T-Factor | K-Factor |
|-------------------------------|-----------------------------|----------|--------------|--------------|-----------------|----------|
| Old SR 8 North | East (SR 70) | 58.0% | EB | WB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | North (Old SR 8) | 70.0% | SB | NB | 7.5% | 9.5% |
| Old SR 8 South | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | EB | WB | 16.0% | 9.5% |
| | South (Old SR 8) | 70.0% | SB | NB | 7.5% | 9.5% |
| Distribution Boulevard | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | South (Distribution Blvd) | 75.0% | SB | NB | 40.0% | 9.5% |
| Glades Driveway | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | North (Glades Driveway) | 60.0% | NB | SB | 15.0% | 9.5% |
| Wedgeworth Driveway | East (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | South (Wedgeworth Driveway) | 70.0% | NB | NB | 30.0% | 9.5% |
| US 27 | East (SR 70) | 53.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 16.0% | 9.5% |
| | North (US 27) | 60.0% | SB | NB | 16.5% | 9.5% |
| | South (US 27) | 60.0% | SB | NB | 16.5% | 9.5% |
| Myers Road/Placid Pines Drive | East (SR 70) | 53.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 53.0% | WB | EB | 16.0% | 9.5% |
| | North (Myers Rd) | 75.0% | NB | SB | 2.5% | 9.5% |
| | South (Placid Pines Dr) | 70.0% | NB | SB | 2.5% | 9.5% |
| Northedge Drive | East (SR 70) | 53.0% | WB | EB | 16.0% | 9.5% |
| | West (SR 70) | 53.0% | WB | EB | 16.0% | 9.5% |
| | North (North Edge Dr) | 75.0% | SB | NB | 5.0% | 9.5% |
| Broward Avenue | East (SR 70) | 53.0% | EB | EB | 16.0% | 9.5% |
| | West (SR 70) | 53.0% | EB | EB | 16.0% | 9.5% |
| | North (Broward Ave) | 70.0% | SB | NB | 5.0% | 9.5% |
| Highlands Boulevard | East (SR 70) | 53.0% | EB | EB | 16.0% | 9.5% |
| | West (SR 70) | 53.0% | EB | EB | 16.0% | 9.5% |
| | North (Highlands Blvd) | 75.0% | SB | NB | 4.0% | 9.5% |
| Citrus Boulevard | East (SR 70) | 53.0% | EB | EB | 16.0% | 9.5% |
| | West (SR 70) | 53.0% | EB | EB | 16.0% | 9.5% |
| | North (Citrus Blvd) | 70.0% | SB | NB | 2.5% | 9.5% |
| Bear Road | East (SR 70) | 53.0% | EB | - | 16.0% | 9.5% |
| | West (SR 70) | 53.0% | EB | EB | 16.0% | 9.5% |
| | North (Bear Rd) | 65.0% | SB | NB | 2.5% | 9.5% |

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| SR 70 Intersection | Intersection Leg | D-Factor | AM Direction | PM Direction | Hourly T-Factor | K-Factor |
|---------------------------------------|------------------------------|----------|--------------|--------------|-----------------|----------|
| Hall Road/Turner Too Road | East (SR 70) | 53.0% | EB | WB | 16.0% | 9.5% |
| | West (SR 70) | 53.0% | EB | WB | 16.0% | 9.5% |
| | North (Hall Rd) | 65.0% | - | SB | 15.0% | 9.5% |
| | South (Turner Too Rd) | 70.0% | - | NB | 2.5% | 9.5% |
| CR 29/KW Farms Road | East (SR 70) | 53.0% | EB | WB | 16.0% | 9.5% |
| | West (SR 70) | 53.0% | EB | WB | 16.0% | 9.5% |
| | North (CR 29) | 65.0% | SB | NB | 7.5% | 9.5% |
| | South (KW Farms Rd) | 70.0% | - | SB | 2.5% | 9.5% |
| Lonesome Island Road/JC Durrance Road | East (SR 70) | 55.0% | EB | EB | 16.0% | 9.5% |
| | West (SR 70) | 53.0% | EB | - | 16.0% | 9.5% |
| | North (Lonesome Island Road) | 70.0% | NB | NB | 15.0% | 9.5% |
| | South (JC Durrance Road) | 70.0% | SB | NB | 15.0% | 9.5% |
| CR 721 South | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 55.0% | EB | EB | 16.0% | 9.5% |
| | North (Driveway) | 60.0% | - | SB | 7.5% | 9.5% |
| | South (CR 721) | 70.0% | SB | NB | 7.5% | 9.5% |
| CR 721 North | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | North (CR 721) | 60.0% | SB | NB | 7.5% | 9.5% |
| Boney Lane/Fulmar Terrace | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | North (Boney Lane) | 70.0% | SB | NB | 7.5% | 9.5% |
| | South (Fulmar Terr) | 60.0% | SB | NB | 7.5% | 9.5% |
| NW New Pine Ridge Road | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | North (New Pine Ridge Rd) | 60.0% | NB | SB | 12.5% | 9.5% |
| 175th Terrace | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | North (175th Terr) | 60.0% | SB | - | 5.0% | 9.5% |
| 172nd Terrace/SW Rucks Dairy Road | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | North (172nd Terr) | 60.0% | SB | NB | 5.0% | 9.5% |
| | South (SW Rucks Dairy Rd) | 70.0% | NB | SB | 7.5% | 9.5% |
| Riverside Road | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | North (Riverside Rd) | 70.0% | SB | NB | 5.0% | 9.5% |
| Shellcracker Loop | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | North (Shellcracker Loop) | 60.0% | SB | NB | 5.0% | 9.5% |
| | South (Driveway) | 60.0% | SB | - | 5.0% | 9.5% |

| SR 70 Intersection | Intersection Leg | D-Factor | AM Direction | PM Direction | Hourly T-Factor | K-Factor |
|--------------------|----------------------|----------|--------------|--------------|-----------------|----------|
| Bream Cove | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | North (Bream Cove) | 55.0% | - | NB | 5.0% | 9.5% |
| 144th Parkway | East (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | South (144th Pkwy) | 70.0% | NB | SB | 5.0% | 9.5% |
| 141st Avenue | East (SR 70) | 58.0% | EB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | WB | EB | 12.5% | 9.5% |
| | North (141st Ave) | 60.0% | SB | SB | 5.0% | 9.5% |
| NW 128th Avenue | East (SR 70) | 58.0% | EB | EB | 12.5% | 9.5% |
| | West (SR 70) | 58.0% | EB | EB | 12.5% | 9.5% |
| | North (NW 128th Ave) | 70.0% | SB | NB | 12.5% | 9.5% |
| | South (SW 128th Ave) | 60.0% | - | - | 10% | 9.5% |

3 Future Traffic Forecasting

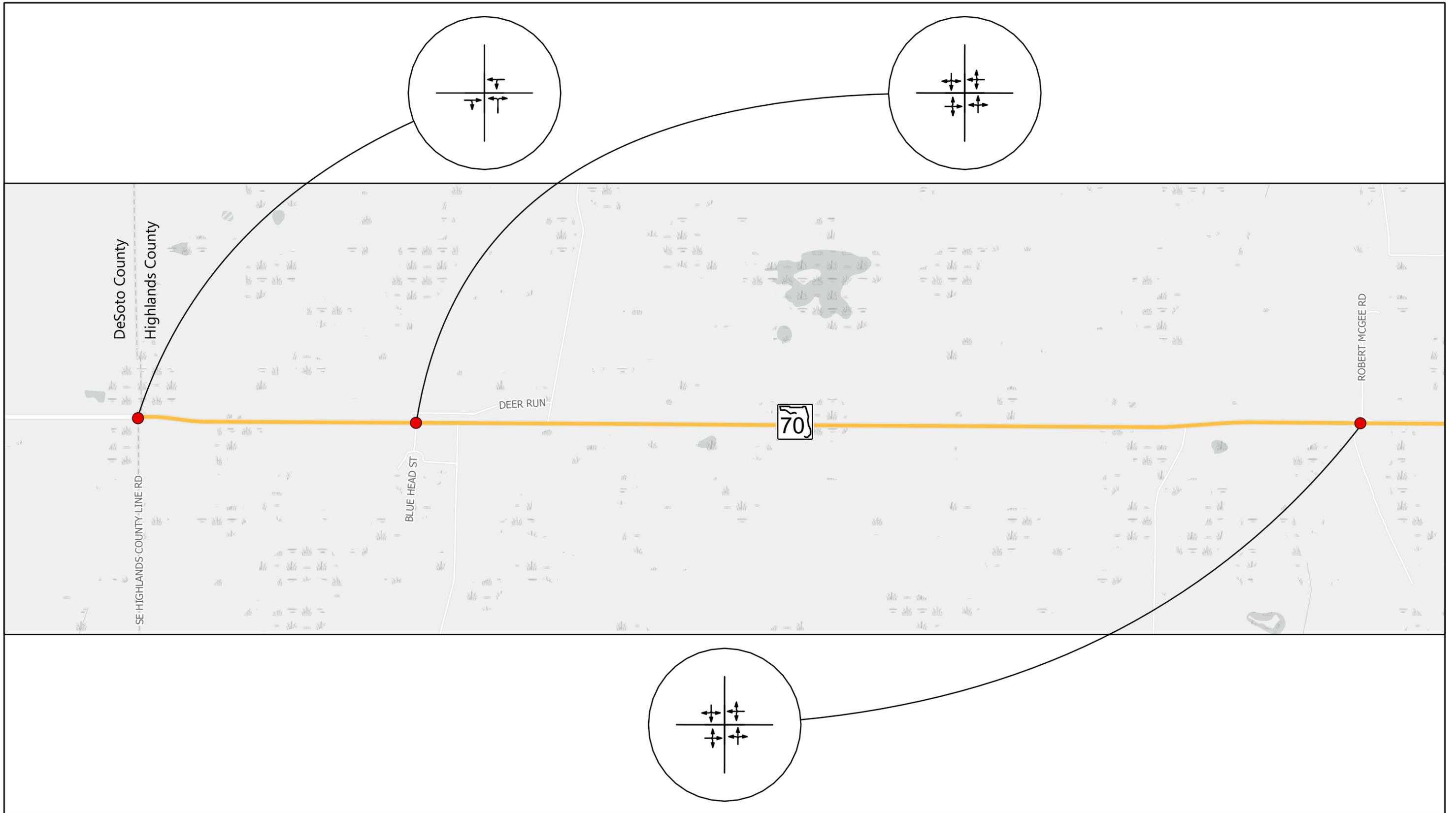
The following sections outline the future traffic forecasting conducted in support of the subsequent traffic analysis.

3.1 Travel Demand Model

The latest available future land use data was obtained as part of the travel demand forecasting process for this study. Anticipated socioeconomic and roadway network changes to the study subarea were incorporated into the modeling effort that is documented in the SR 70 Traffic Forecast Modeling Technical Memorandum completed in December 2022 (**Appendix C**). The modeling effort involved conducting a sub-area base year (2015) validation refinement for the study area, as well as development of refined horizon year (2045) models. The regional travel demand model applied for this study was based on the adopted District One 2045 Regional Planning Model (D1RPM v2.0), which was the current/latest model at the time in 2022. The D1RPM is a travel demand forecasting tool developed by FDOT District One, in conjunction with the six District Metropolitan Planning Organizations (MPO) and Transportation Planning Organizations (TPO) in support of their 2045 Long Range Transportation Plans (LRTP).

Following the development of the 2045 No-Build Model, which represents the traffic growth in the No-Build Alternative, a Build model was developed. The Base Year, No-Build, and Build Alternative model plots are also included in **Appendix C**. The 2045 No-Build Alternative only incorporates adjacent projects that are included in the respective LRTP Cost Feasible Plans. Two new developments are included in the No-Build scenario: a Recreational Vehicle Park and Mobile Home Park are expected to be constructed off SR 70 in the project limits. SR 70 remains a 2-lane undivided facility in the No-Build condition so full access will be permitted to these new

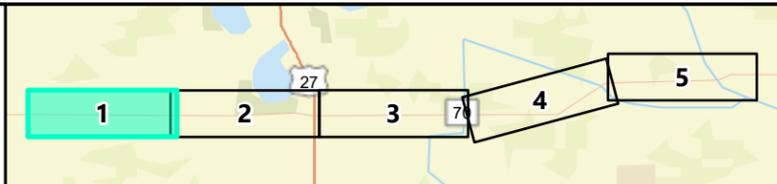
developments. The 2045 Build Alternative consists of SR 70 operating as a four-lane arterial from the DeSoto County line to the CR 559/NW 128th Avenue in Okeechobee County. In the Build scenario, conservative assumptions were made regarding access management. Directional median openings were assumed at all unsignalized intersections per direction from District One. Right turn lane recommendations were made based on the *FDOT Access Management Guidebook (2019)* criteria. The right turn lane lengths are based on the 95th percentile queue length and appropriate deceleration lane length based on assumed design speed. A table documenting the recommendations and preliminary right turn lane lengths is included in **Appendix F**. Further analysis during the individual PD&E studies will be used to develop the proposed access management plans. Lane configurations for No-Build and Build scenarios are shown in **Figure 3-1** and **Figure 3-2** respectively.



Legend

- Project Limits
- Unsignalized (3)

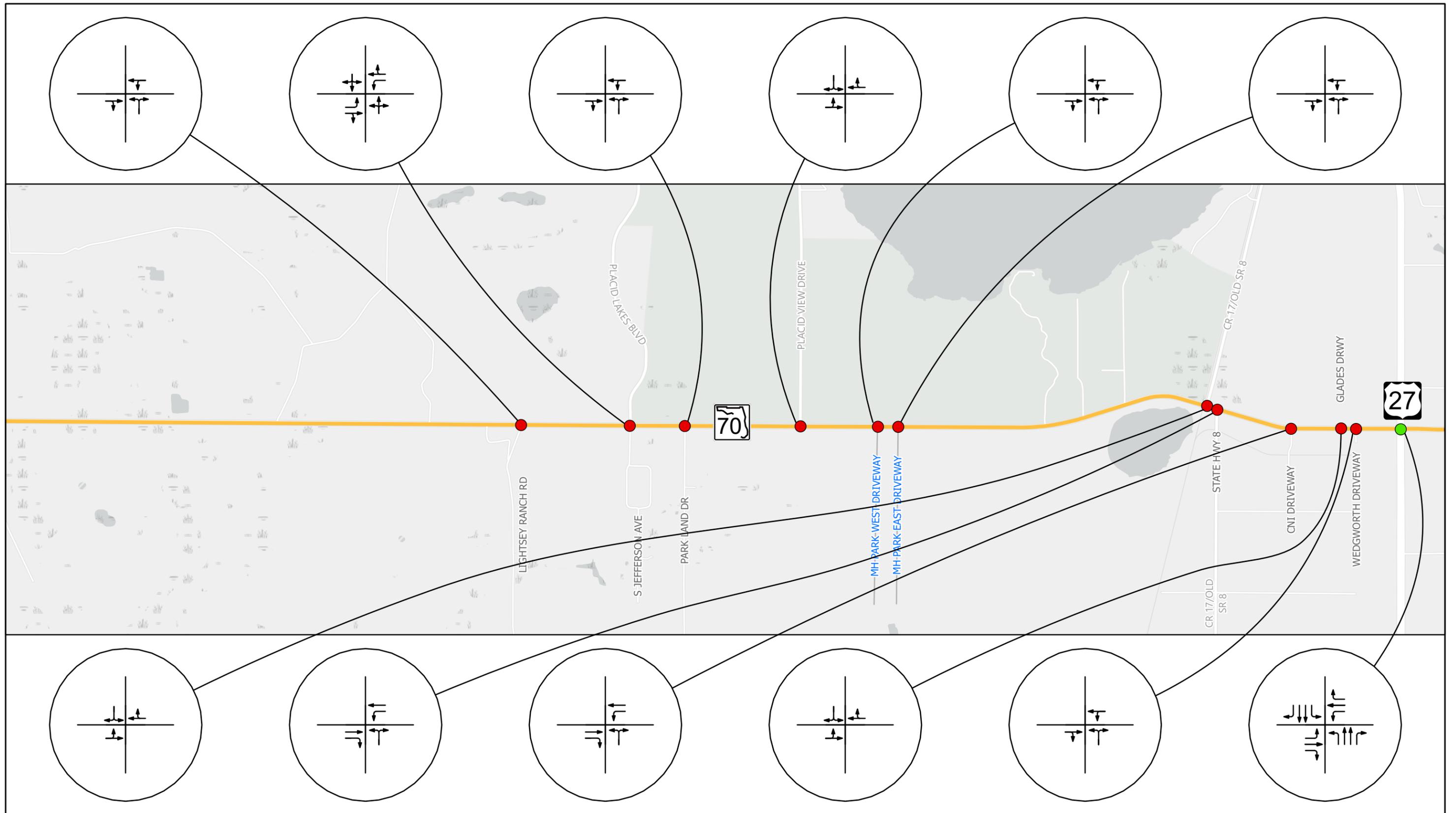
Lane Configuration



N

0 2,000 Feet

Figure 3-1: No-Build Lane Configuration
Sheet 1 of 5



Legend

- Project Limits
- Unsignalized (12)
- Signalized (1)

Lane Configuration

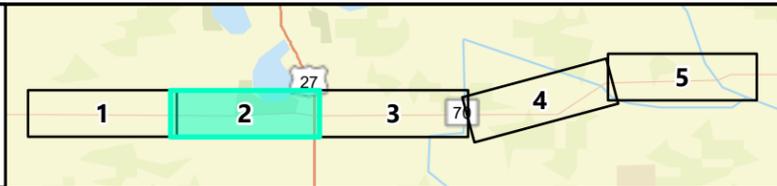
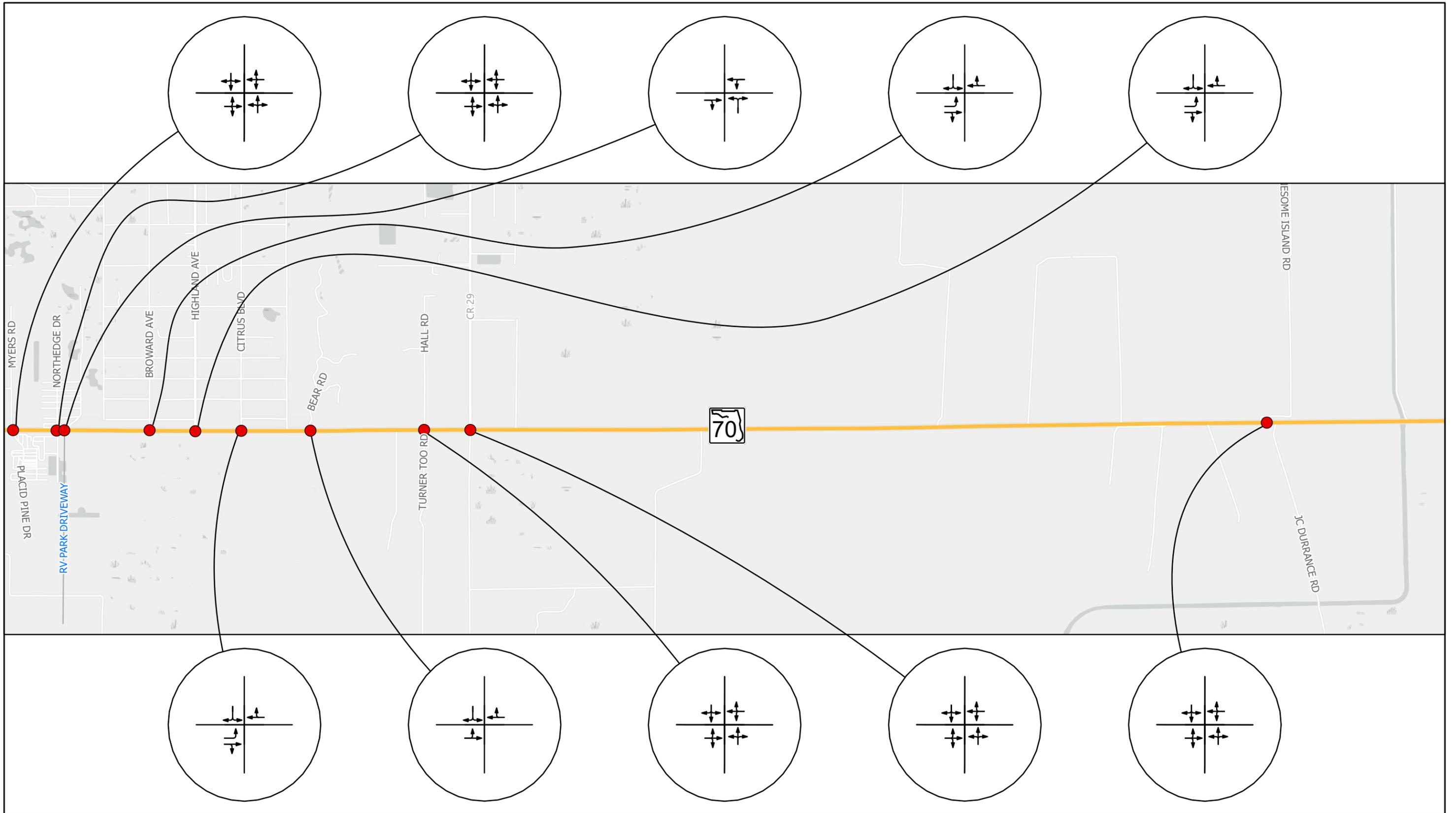


Figure 3-1: No-Build Lane Configuration
Sheet 2 of 5



Legend

- Project Limits
- Unsignalized (10)

Lane Configuration

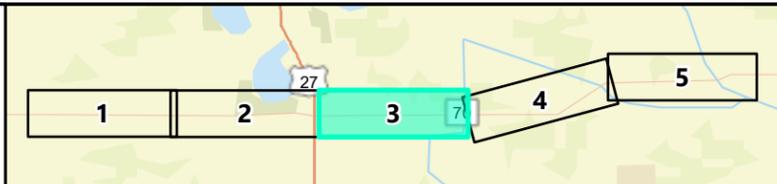
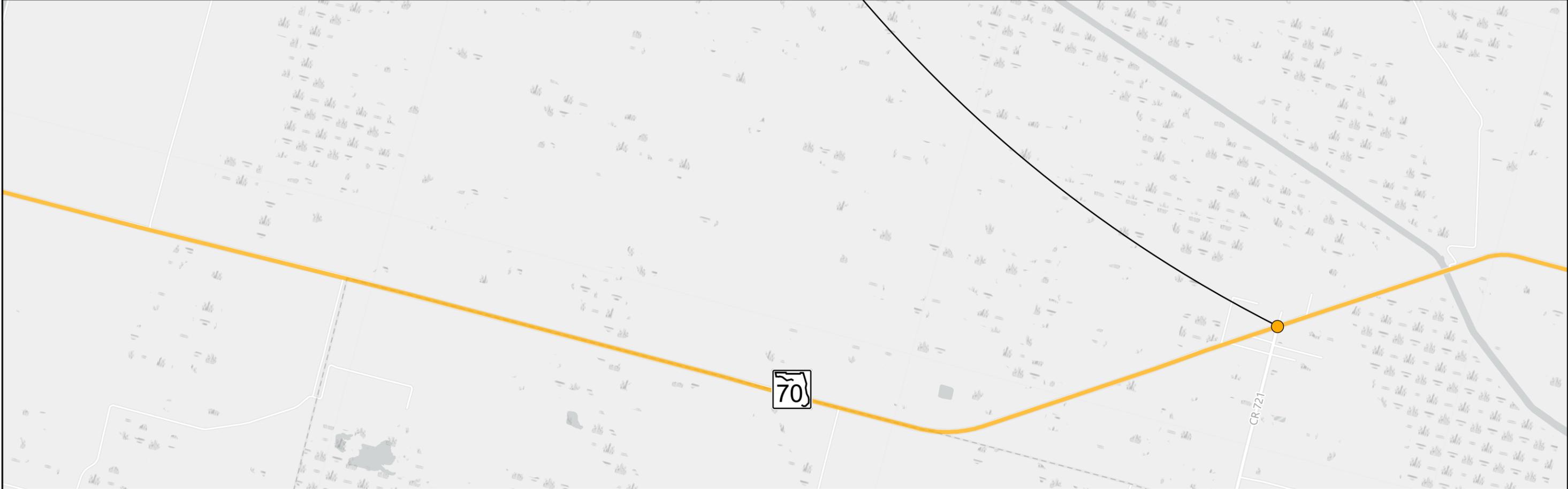
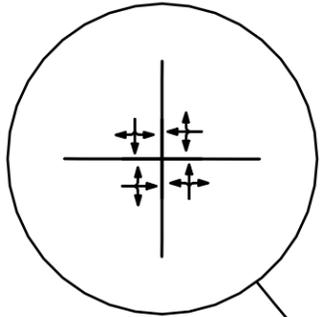


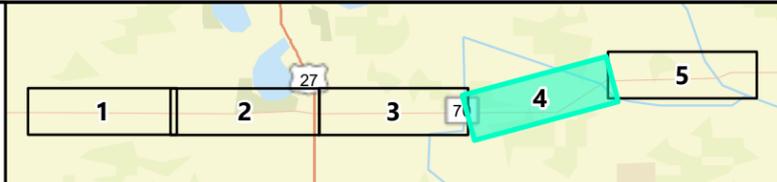
Figure 3-1: No-Build Lane Configuration
Sheet 3 of 5



Legend

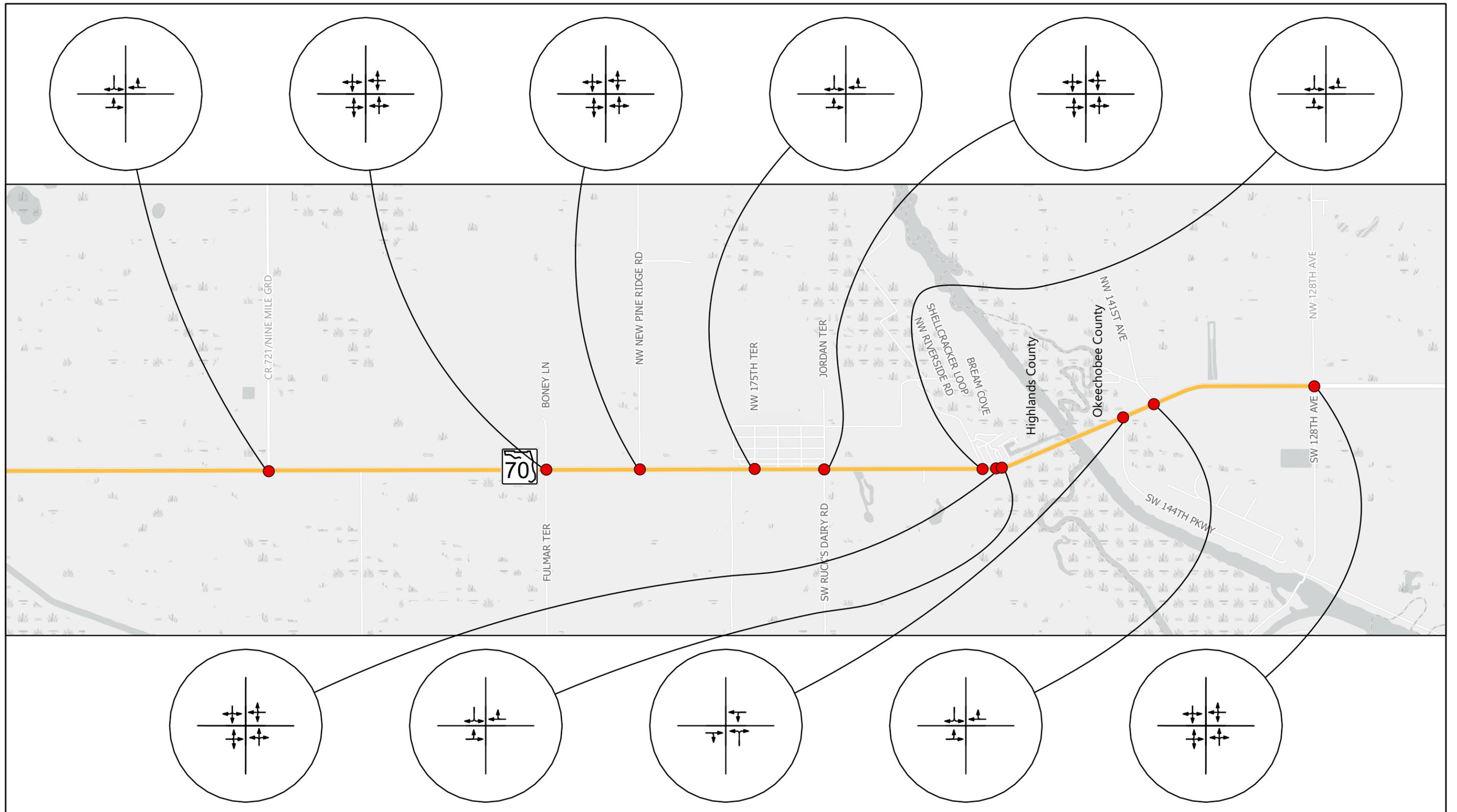
-  Project Limits
-  Flashing Yellow (1)

 Lane Configuration



0 2,000 Feet

Figure 3-1: No-Build Lane Configuration
Sheet 4 of 5



Legend
 — Project Limits
 ● Unsignalized (11)

↔ ↔ ↔ Lane Configuration

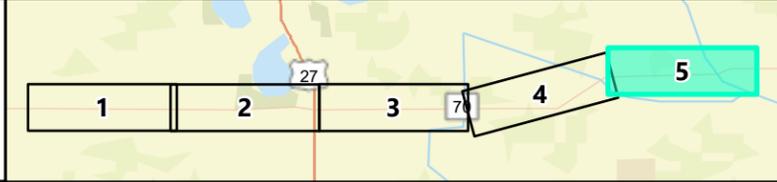
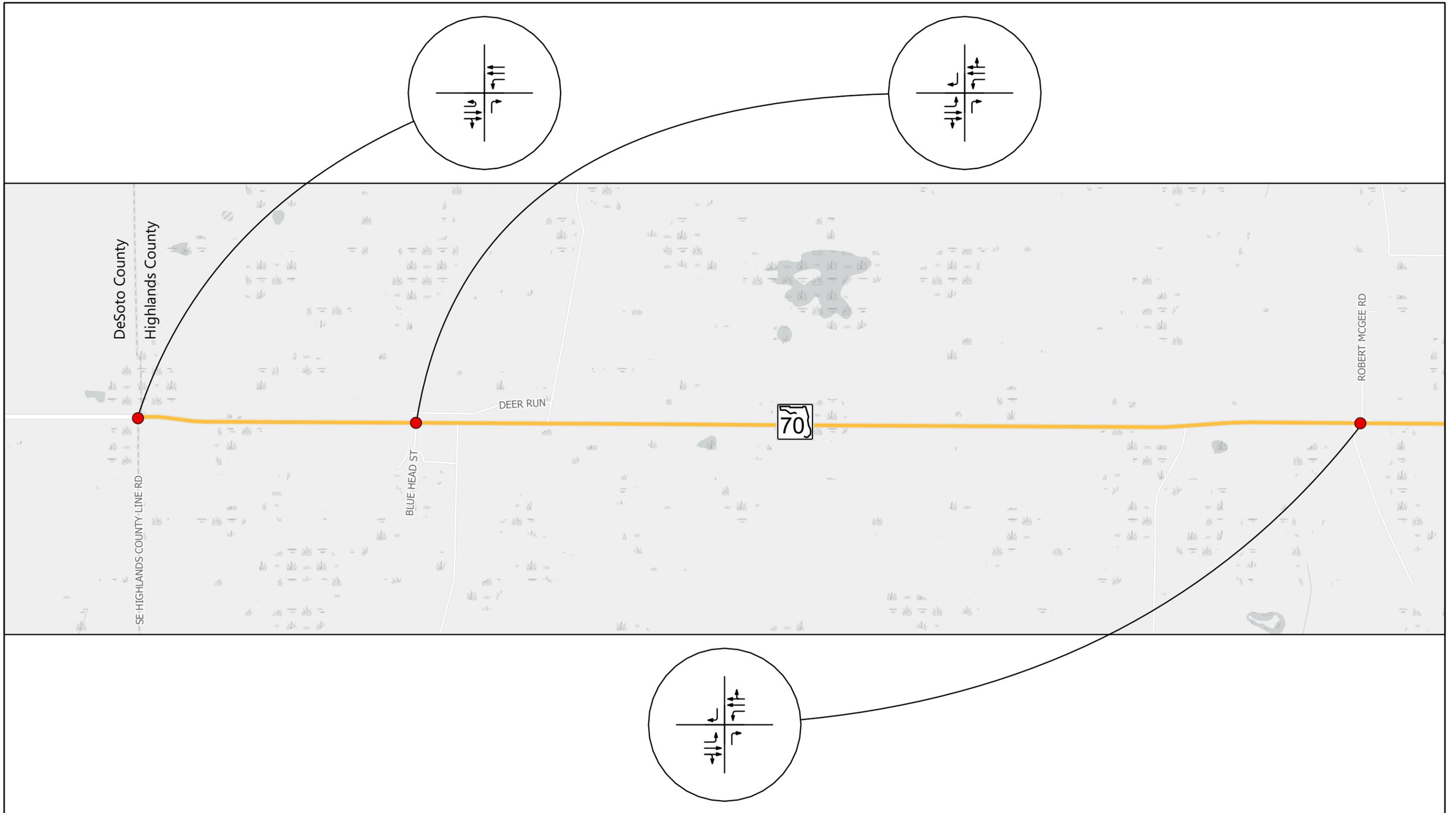


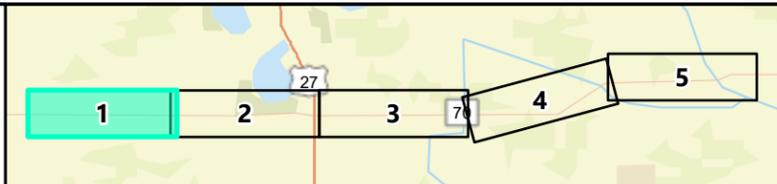
Figure 3-1: No-Build Lane Configuration
 Sheet 5 of 5



Legend

- Project Limits
- Unsignalized (3)

Lane Configuration

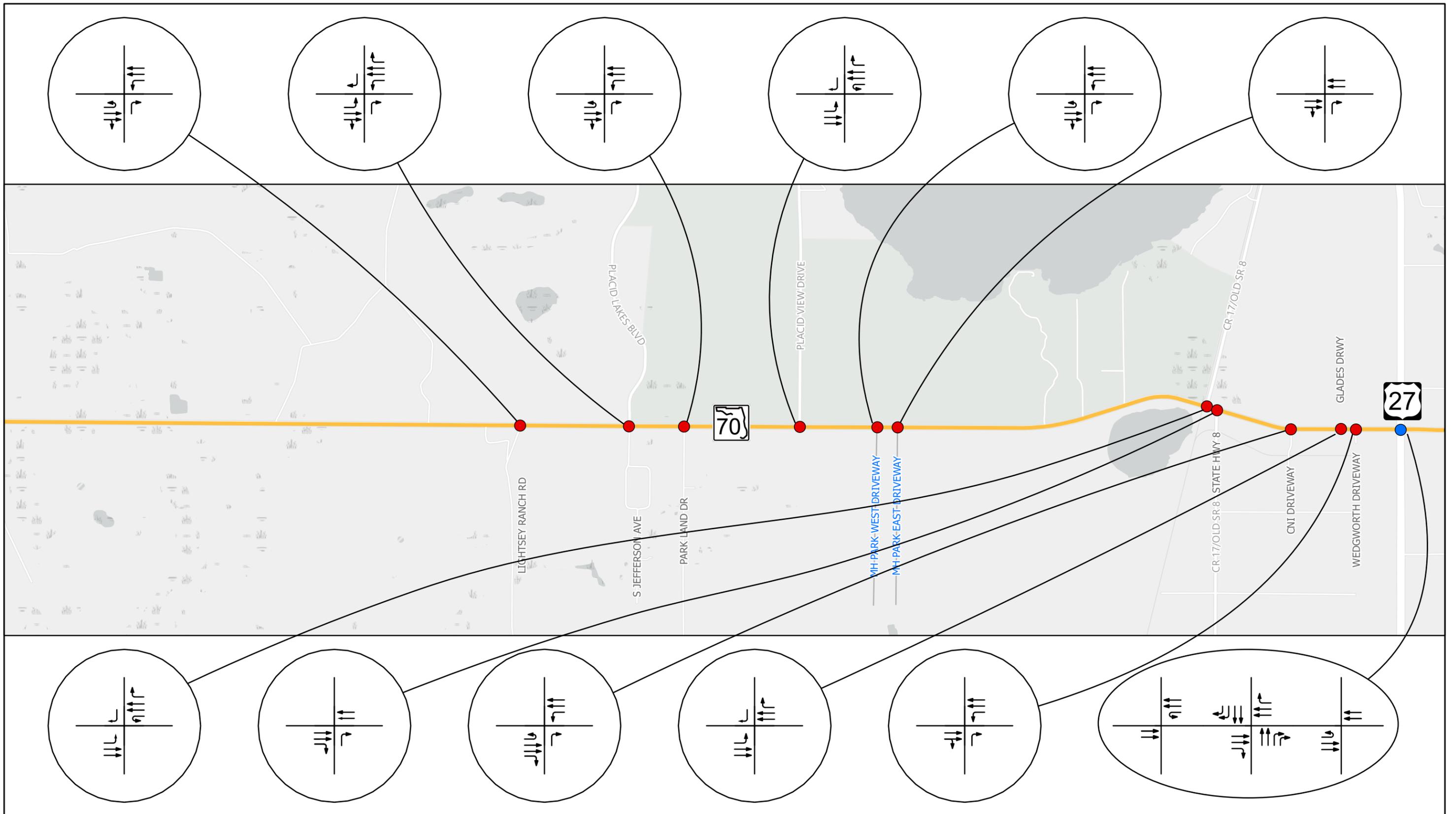


N

0 2,000 Feet

Figure 3-2: Build Lane Configuration

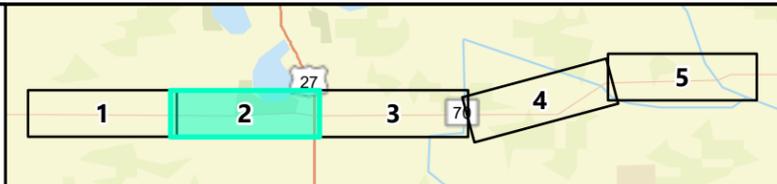
Sheet 1 of 5



Legend

- Project Limits
- Unsignalized (12)
- Median U-Turn (MUT) (1)

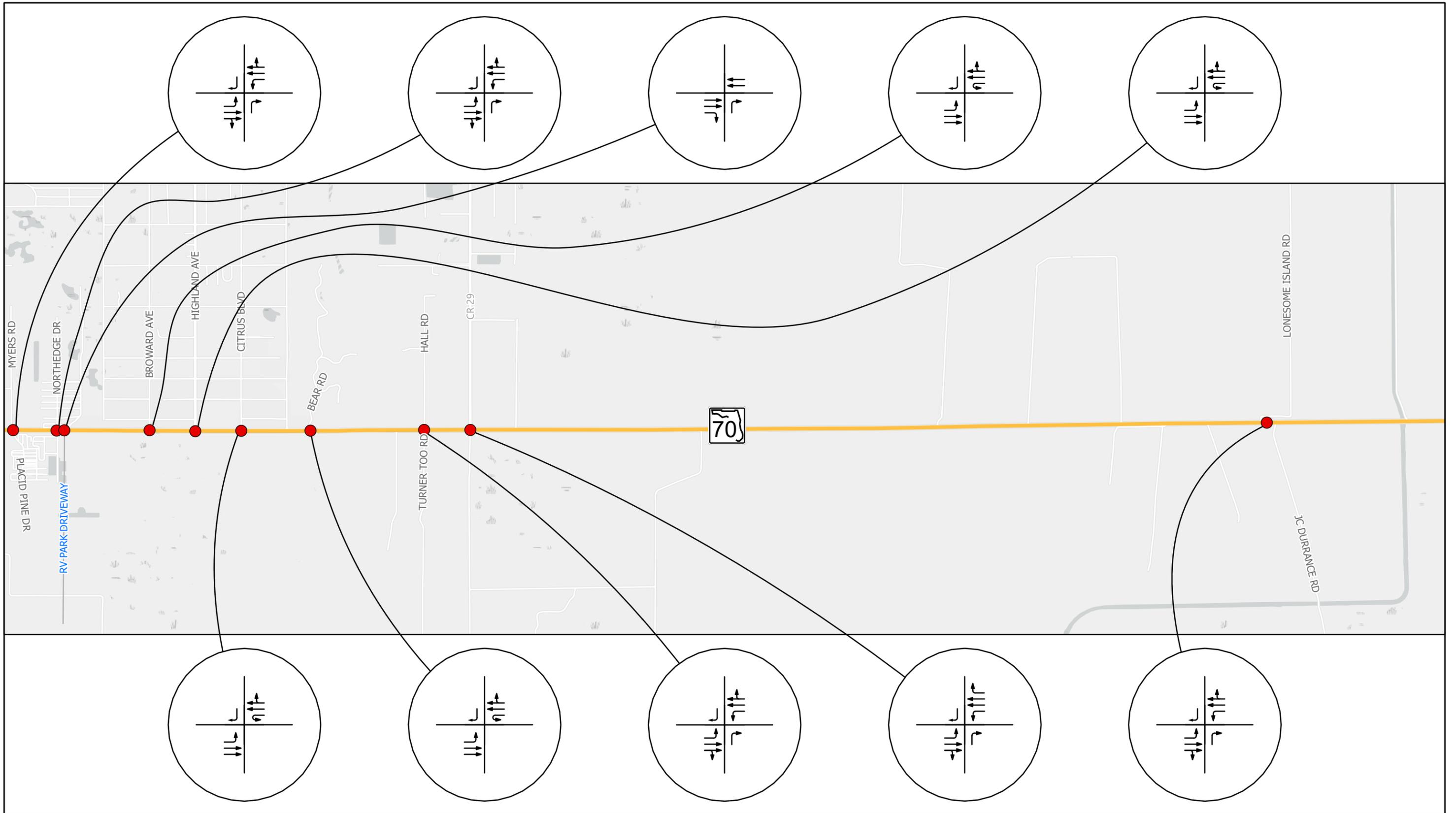
Lane Configuration



0 2,000 Feet

Figure 3-2: Build Lane Configuration

Sheet 2 of 5



Legend

- Project Limits
- Unsignalized (10)

Lane Configuration

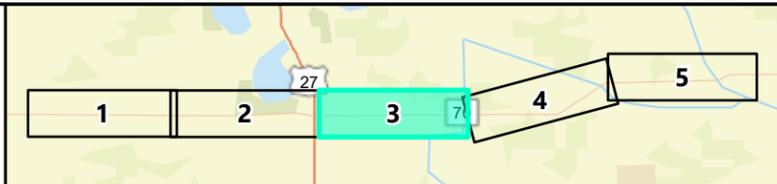
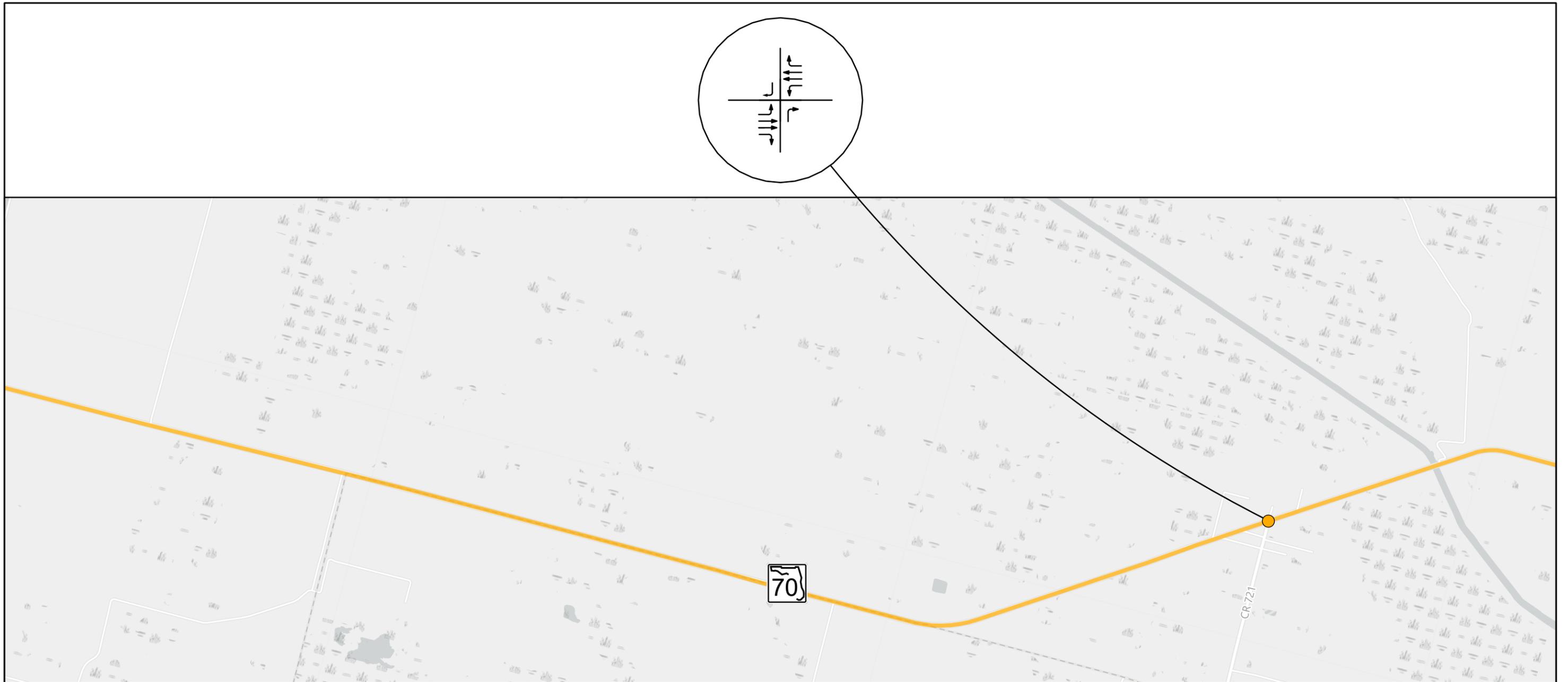


Figure 3-2: Build Lane Configuration

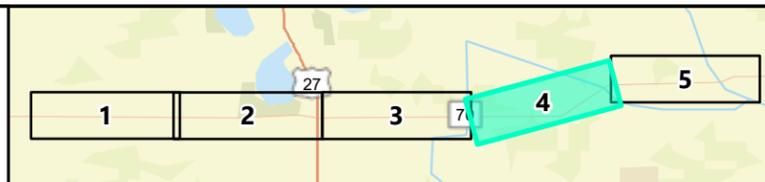
Sheet 3 of 5



Legend

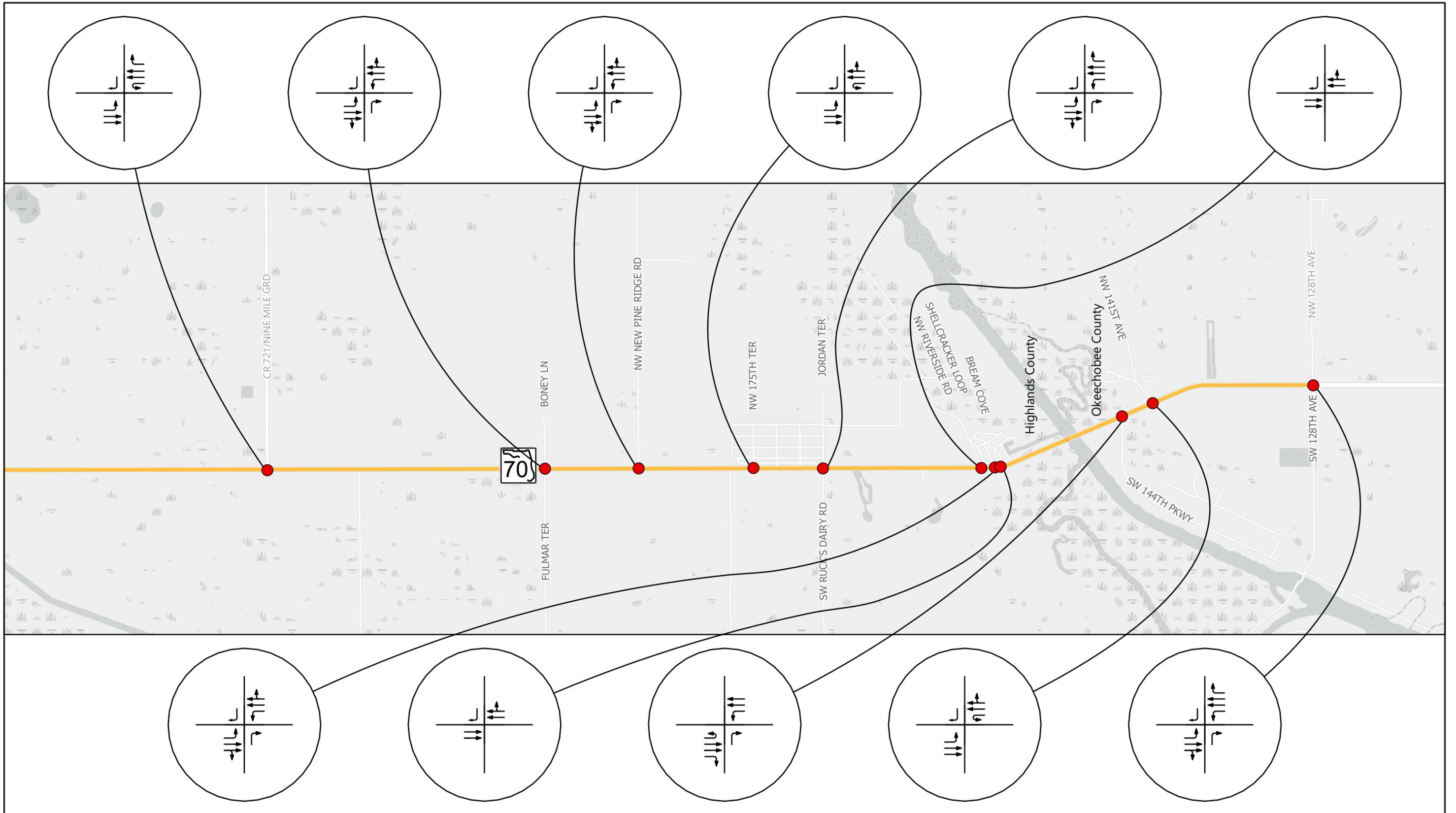
- Project Limits
- Flashing Yellow (1)

↔↔↔ Lane Configuration



0 2,000 Feet

Figure 3-2: Build Lane Configuration



Legend

- Project Limits
- Unsignalized (11)

Lane Configuration

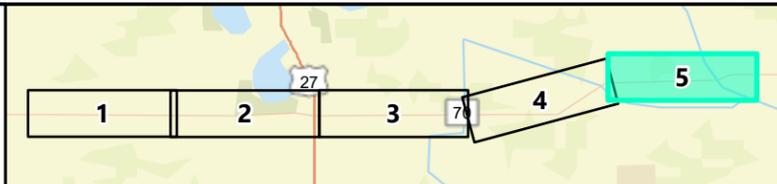


Figure 3-2: Build Lane Configuration

Sheet 5 of 5

3.2 Development of Design Year (2052) Traffic Volumes

The following subsections outline the development of the design year Annual Average Daily Traffic (AADT) and peak hour volumes.

3.2.1 Selection of Growth Rates

Both the TDM No-Build and Build volume forecasts have been reviewed for reasonableness by comparison to historical traffic trends analysis and population projections from the Bureau of Economic and Business Research (BEBR) where applicable. Based on this comparison, Build and No-Build Alternative growth rates for the study area have been developed and are presented in **Table 3-1**. After a review of model growth, historical trends, and population growth forecasts, the corridor was segmented based on anticipated growth rates. Growth rates for each segment were selected for each segment based primarily on average model growth estimates, with consideration given to other data sources where appropriate. On average, the Build scenario is expected to experience 1.0-1.5% more annual growth along SR 70 beyond the No Build scenario. Growth rates for minor side streets were based on regional historical trends, facility type, and network connection, with a minimum rate of 2% selected for side streets. The Highlands County BEBR Population Projection report, Florida Traffic Online (FTO) Historical AADT reports, and trends analysis are included in **Appendix D**.

Table 3-1: Design Year Effective Growth Rates

| Location | | Base Year TDM AADT (2015) | Future Year No-Build TDM AADT (2045) | No Build TDM Annual Growth Rate | Future Year Build TDM AADT (2045) | Build TDM Annual Growth Rate | Estimated Existing AADT Rounded | Historic Trends | R ² Value | BEER Low | BEER Medium | BEER High | Selected Growth Rate (No-Build) | Selected Growth Rate (Build) |
|--|---|---------------------------|--------------------------------------|---------------------------------|-----------------------------------|------------------------------|---------------------------------|-----------------|----------------------|----------|-------------|-----------|---------------------------------|------------------------------|
| SR 70 | East of County Line to Robert McGee Rd | 3,161 | 5,518 | 2.49% | 6,656 | 3.69% | | | | | | | 3.0% | 4.0% |
| | Between Robert McGee Rd and Lightsey Ranch Rd | 3,207 | 6,003 | 2.91% | 7,175 | 4.12% | | | | | | | | |
| | Between Lightsey Ranch Rd and Placid Lakes Blvd | 3,755 | 7,128 | 2.99% | 8,343 | 4.07% | | 4.20% | 65.89% | | | | | |
| | Between Placid Lakes Blvd and Placid View Dr | 2,688 | 5,579 | 3.59% | 6,744 | 5.03% | | | | | | | | |
| | Between Placid View Dr and Old SR 8 (West) | 2,338 | 5,165 | 4.03% | 6,290 | 5.63% | | | | | | | | |
| | Between Old SR 8 (West) and Old SR 8 (East) | 2,359 | 5,221 | 4.04% | 6,358 | 5.65% | | | | | | | | |
| | Between Old SR 8 (East) and Distribution Blvd | 2,335 | 5,156 | 4.03% | 6,287 | 5.64% | | | | | | | | |
| | Between Old SR 8 (East) and Distribution Blvd | 2,335 | 5,156 | 4.03% | 6,287 | 5.64% | | | | | | | | |
| | Between Distribution Blvd and US 27 | 2,544 | 5,500 | 3.87% | 6,624 | 5.35% | | 0.00% | 0.16% | | | | | |
| | Between US 27 and Highlands Blvd | 4,530 | 7,532 | 2.21% | 9,743 | 3.84% | | 0.31% | 3.08% | | | | | |
| | Between Highlands Blvd and CR 29 | 4,709 | 7,883 | 2.25% | 10,166 | 3.86% | | | | | | | | |
| | Between CR 29 and Denco Rd | 4,939 | 7,968 | 2.04% | 10,268 | 3.60% | | | | | | | | |
| | Between Denco Rd and Harney Pond Canal | 4,946 | 8,000 | 2.06% | 10,307 | 3.61% | | | | | | | | |
| | Between Harney Pond Canal and Greenbrier Ln | 4,890 | 7,945 | 2.08% | 10,254 | 3.66% | | | | | | | | |
| | Between Greenbrier Ln and CR 721 (West) | 4,818 | 7,820 | 2.08% | 10,131 | 3.68% | | | | | | | | |
| | Between CR 721 (West) and CR 721 (East) | 4,526 | 8,045 | 2.59% | 10,286 | 4.24% | | 0.83% | 13.92% | | | | | |
| | Between CR 721 (East) and Fulmar Terrace | 4,516 | 7,995 | 2.57% | 10,206 | 4.20% | | | | | | | | |
| | Between Fulmar Terrace and SW Rucks Dairy Rd | 4,507 | 8,195 | 2.73% | 10,364 | 4.33% | | | | | | | | |
| Between SW Rucks Dairy Rd and County Line | 4,636 | 8,647 | 2.89% | 10,766 | 4.41% | | | | | | | | | |
| Between County Line and NW 128 th Ave | 4,451 | 8,345 | 2.92% | 10,274 | 4.36% | 1.42% | 33.99% | | | | | | | |
| Side Streets | Highlands County Line Rd South of SR 70 | | | | | | 100 | | | -0.42% | 0.37% | 1.16% | 2.0% | 3.0% |
| | Deer Run Rd North of SR 70 | | | | | | 100 | | | | | | 2.0% | 3.0% |
| | Blue Head Street South of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Robert McGee Rd North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Lightsey Ranch Rd South of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |

| Location | | Base Year TDM AADT (2015) | Future Year No-Build TDM AADT (2045) | No Build TDM Annual Growth Rate | Future Year Build TDM AADT (2045) | Build TDM Annual Growth Rate | Estimated Existing AADT Rounded | Historic Trends | R ² Value | BEER Low | BEER Medium | BEER High | Selected Growth Rate (No-Build) | Selected Growth Rate (Build) |
|------------------------------|-------------------------------------|---------------------------|--------------------------------------|---------------------------------|-----------------------------------|------------------------------|---------------------------------|-----------------|----------------------|----------|-------------|-----------|---------------------------------|------------------------------|
| Side Streets | Placid Lakes Blvd North of SR 70 | 1,816 | 2,883 | 1.96% | 3,090 | 2.34% | 900 | 22.22% | 90.19% | -0.42% | 0.37% | 1.16% | 3.0% | 4.0% |
| | Jefferson Ave South of SR 70 | | | | | | 250 | | | | | | 3.0% | 4.0% |
| | Park Land Dr South of SR 70 | | | | | | 300 | | | | | | 3.0% | 4.0% |
| | Placid View Dr North of SR 70 | 812 | 1,225 | 1.70% | 1,310 | 2.04% | 1250 | 5.56% | 43.43% | | | | 3.0% | 4.0% |
| | Old SR 8 (West) North of SR 70 | 71 | 140 | 3.24% | 155 | 3.94% | 1100 | 4.94% | 48.76% | | | | | |
| | Old SR 8 (East) South of SR 70 | 24 | 86 | 8.61% | 91 | 9.31% | 900 | 11.11% | 28.25% | | | | 3.0% | 4.0% |
| | CNI Driveway South of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Glades Driveway North of SR 70 | | | | | | 150 | | | | | | 3.0% | 4.0% |
| | Wedgeworth Driveway South of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | US 27 North of SR 70 | 8,027 | 15,910 | 3.27% | 17,387 | 3.89% | 9400 | -0.81% | 15.42% | | | | 3.5% | 4.0% |
| | US 27 South of SR 70 | 7,072 | 14,464 | 3.48% | 14,889 | 3.68% | 8800 | 1.72% | 8.17% | | | | 3.0% | 4.0% |
| | Myers Rd North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Placid Pines Dr South of SR 70 | | | | | | 400 | | | | | | 3.0% | 4.0% |
| | North Edge Dr North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Broward Ave North of SR 70 | | | | | | 300 | | | | | | 3.0% | 4.0% |
| | Highland Ave North of SR 70 | | | | | | 500 | | | | | | 3.0% | 4.0% |
| | Citrus Blvd North of SR 70 | | | | | | 200 | | | | | | 3.0% | 4.0% |
| | Bear Rd North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Hall Rd North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Turner Too Rd South of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | CR 29 North of SR 70 | 371 | 581 | 1.89% | 693 | 2.89% | 750 | 13.89% | 75.76% | | | | 3.0% | 4.0% |
| | KW Farms Road South of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Lonesome Island Rd North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | JC Durrance Rd South of SR 70 | | | | | | 150 | | | | | | 3.0% | 4.0% |
| | Lykes Ranch Driveway North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | CR 721 (West) South of SR 70 | 864 | 815 | -0.19% | 935 | 0.27% | 1900 | -0.56% | 10.61% | | | | 3.0% | 4.0% |
| CR 721 (East) North of SR 70 | 79 | 151 | 3.04% | 178 | 4.18% | 700 | 1.85% | 63.64% | | | | | | |
| Boney Ln North of SR 70 | | | | | | 100 | | | 3.0% | 4.0% | | | | |

| Location | | Base Year TDM AADT (2015) | Future Year No-Build TDM AADT (2045) | No Build TDM Annual Growth Rate | Future Year Build TDM AADT (2045) | Build TDM Annual Growth Rate | Estimated Existing AADT Rounded | Historic Trends | R ² Value | BEER Low | BEER Medium | BEER High | Selected Growth Rate (No-Build) | Selected Growth Rate (Build) |
|--------------|---|---------------------------|--------------------------------------|---------------------------------|-----------------------------------|------------------------------|---------------------------------|-----------------|----------------------|----------|-------------|-----------|---------------------------------|------------------------------|
| Side Streets | Fulmar Terrace South of SR 70 | | | | | | 150 | | | -0.42% | 0.37% | 1.16% | 3.0% | 4.0% |
| | NW New Pine Ridge Rd North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | 175th Terrace North of SR 70 | | | | | | 250 | | | | | | 3.0% | 4.0% |
| | 172nd Terrace (Jordan Terrace) North of SR 70 | | | | | | 400 | | | | | | 3.0% | 4.0% |
| | SW Rucks Dairy Rd South of SR 70 | | | | | | 300 | | | | | | 3.0% | 4.0% |
| | Riverside Rd North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Shellcracker Loop North of SR 70 | | | | | | 150 | | | | | | 3.0% | 4.0% |
| | Driveway South of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | Bream Cove North of SR 70 | | | | | | 150 | | | | | | 3.0% | 4.0% |
| | 144th Pkwy South of SR 70 | | | | | | 300 | | | | | | 3.0% | 4.0% |
| | 141st Ave North of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |
| | NW 128th Ave North of SR 70 | 103 | 251 | 4.79% | 336 | 7.54% | 400 | 2.50% | 3.00% | | | | 3.0% | 4.0% |
| | SW 128th Ave South of SR 70 | | | | | | 100 | | | | | | 3.0% | 4.0% |

Selected average annual growth rates along SR 70 range from 2.5% to 4.0% for the No-Build scenario and 4.0% to 5.0% in the Build scenario. The selected growth rates for the cross streets in the study area range from 2.0% to 3.5% for the No-Build scenario and 3.0% to 4.0% for all cross streets in the Build scenario.

3.2.2 Design Year (2052) Annual Average Daily Traffic (AADT) Volumes

Future design year daily (AADT) volumes were developed for the No-Build and Build Alternatives by linearly growing the Existing (2022) AADTs by the respective selected growth rates to the design year of 2052. Two new developments will also be completed by the design year: a Recreational Vehicle Park and Mobile Home Park are expected to be constructed off SR 70 in the project limits. AADTs for the driveways accessing these developments were estimated using the ITE Trip Generation Handbook (11th Edition). The supporting trip generation documents can be found in **Appendix E**. In both the No-Build and Build scenarios, some manual adjustments of AADTs were required to maintain AADT balance. **Table 3-2** displays Design Year No-Build and Build AADT development.

Table 3-2: Design Year No-Build and Build AADT

| Location | | Existing | No-Build | | | Build | | | |
|---|--|--------------------|----------------------|------------------|---------------------------|----------------------|------------------|---------------------------|---------------|
| | | 2022 Existing AADT | Selected Growth Rate | Design Year AADT | Rounded AADT | Selected Growth Rate | Design Year AADT | Rounded AADT | |
| SR 70 | West of County Line to Robert McGee Rd | 5,800 | 3.0% | 11,020 | 11,000 | 4.0% | 12,760 | 13,000 | |
| | Between Robert McGee Rd and Lightsey Ranch Rd | 5,000 | | 9,500 | 9,500 | | 11,000 | 11,000 | |
| | West of Lightsey Ranch Rd to Placid Lakes Blvd | 4,500 | | 8,550 | 8,600 | | 9,900 | 9,900 | |
| | Between Lightsey Ranch Rd and Placid Lakes Blvd | | | | | | | | |
| | Between Placid Lakes Blvd and Park Land Dr | 5,100 | 4.0% | 10,500 | 10,500¹ | 5.0% | 12,000 | 12,000¹ | |
| | Between Park Land Dr and Placid View Dr | | | | | | | | |
| | Between Placid View Dr and Old SR 8 (West) | | | | | | | | |
| | Between Old SR 8 (West) and Old SR 8 (East) | | | | | | | | |
| | Between Old SR 8 (East) and Distribution Blvd | | | | 11,220 | | 11,000 | 12,750 | 13,000 |
| | Between Distribution Blvd and Glades Driveway | | | | | | | | |
| | Between Glades Driveway and Wedgeworth Driveway | | | | | | | | |
| | Between Wedgeworth Driveway and US 27 | | | | | | | | |
| | Between US 27 and Myers Rd/Placid Pines Dr | 5,600 | 2.5% | 9,800 | 9,800 | 4.0% | 12,320 | 12,500 | |
| | Between Myers Rd/Placid Pines Dr and North Edge Dr | | | | | | | | |
| | Between North Edge Dr and Broward Ave | | | | | | | | |
| | Between Broward Ave and Highlands Ave | | | | | | | | |
| | Between Highlands Ave and Citrus Blvd | | | | | | | | |
| | Between Citrus Blvd and Bear Rd | | | | | | | | |
| | Between Bear Rd and Hall Rd | 5,600 | 2.5% | 9,800 | 9,800 | 4.0% | 12,320 | 12,500 | |
| | Between Hall Rd and CR 29 | | | | | | | | |
| Between CR 29 and Lonesome Island Rd | | | | | | | | | |
| Between Lonesome Island Rd and CR 721 South | | | | | | | | | |
| Between CR 721 South and CR 721 North | 5,400 | 3.0% | 10,260 | 10,500 | 4.5% | 12,690 | 12,500 | | |
| Between CR 721 North and Boney Ln/Fulmar Terr | | | | | | | | | |
| Between Boney Ln/Fulmar Terr and NW New Pine Ridge Rd | | | | | | | | | |
| Between NW New Pine Ridge Rd and 175th Terr | | | | | | | | | |
| Between 175th Terr and 172nd Terr/SW Rucks Dairy Rd | | | | | | | | | |

| Location | | Existing | No-Build | | | Build | | |
|-----------------------------|---|--------------------|----------------------|------------------|---------------|----------------------|------------------|---------------|
| | | 2022 Existing AADT | Selected Growth Rate | Design Year AADT | Rounded AADT | Selected Growth Rate | Design Year AADT | Rounded AADT |
| SR 70 | Between 172nd Terr/SW Rucks Dairy Rd and Riverside Rd | 5,400 | 3.0% | 10,260 | 10,500 | 4.5% | 12,690 | 12,500 |
| | Between Riverside Rd and Shellcracker Loop | | | | | | | |
| | Between Shellcracker Loop and Bream Cove | | | | | | | |
| | Between Bream Cove and 144th Pkwy | | | | | | | |
| | Between 144th Pkwy and 141st Ave | 6,100 | | 11,590 | 11,500 | | 14,335 | 14,500 |
| | Between 141st Ave and NW 128th Ave | | | | | | | |
| | East of NW 128th Ave | | | | | | | |
| Side Streets | Highlands County Line Rd South of SR 70 | 100 | 2.0% | 160 | 150 | 3.0% | 190 | 200 |
| | Deer Run Rd North of SR 70 | 100 | 2.0% | 160 | 150 | 3.0% | 190 | 200 |
| | Blue Head Street South of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Robert McGee Rd North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Lightsey Ranch Rd South of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Placid Lakes Blvd North of SR 70 | 900 | 3.0% | 1,710 | 1,700 | 4.0% | 1,980 | 2,000 |
| | Jefferson Ave South of SR 70 | 250 | 3.0% | 475 | 500 | 4.0% | 550 | 550 |
| | Park Land Dr South of SR 70 | 300 | 3.0% | 570 | 550 | 4.0% | 660 | 650 |
| | Placid View Dr North of SR 70 | 350 | 3.0% | 665 | 650 | 4.0% | 770 | 750 |
| | Old SR 8 (West) North of SR 70 | 1,100 | 3.0% | 2,090 | 2,100 | 4.0% | 2,420 | 2,400 |
| | Old SR 8 (East) South of SR 70 | 900 | 3.0% | 1,710 | 1,700 | 4.0% | 1,980 | 2,000 |
| | Distribution Blvd (CNI Driveway) South of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Glades Driveway North of SR 70 | 150 | 3.0% | 285 | 300 | 4.0% | 330 | 350 |
| | Wedgeworth Driveway South of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | US 27 North of SR 70 | 9,400 | 3.5% | 19,270 | 19,000 | 4.0% | 20,680 | 20,500 |
| | US 27 South of SR 70 | 8,800 | 3.0% | 16,720 | 16,500 | 4.0% | 19,360 | 19,500 |
| | Myers Rd North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Placid Pines Dr South of SR 70 | 400 | 3.0% | 760 | 750 | 4.0% | 880 | 900 |
| | North Edge Dr North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Broward Ave North of SR 70 | 300 | 3.0% | 570 | 550 | 4.0% | 660 | 650 |
| Highland Ave North of SR 70 | 500 | 3.0% | 950 | 950 | 4.0% | 1,100 | 1,100 | |

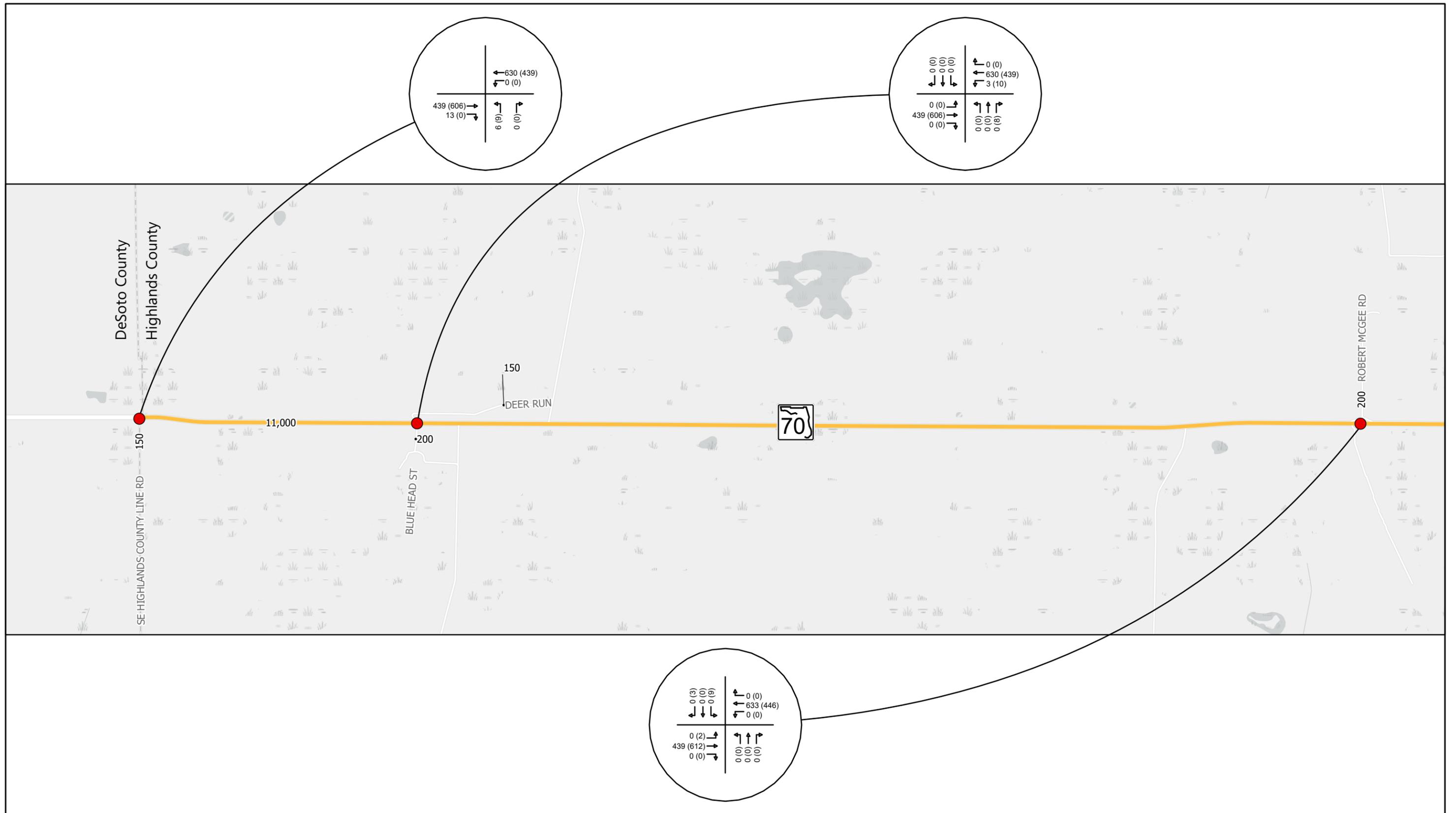
| Location | | Existing | No-Build | | | Build | | |
|-----------------------------|--|--------------------|----------------------|------------------|--------------|----------------------|------------------|--------------|
| | | 2022 Existing AADT | Selected Growth Rate | Design Year AADT | Rounded AADT | Selected Growth Rate | Design Year AADT | Rounded AADT |
| Side Streets | Citrus Blvd North of SR 70 | 200 | 3.0% | 380 | 400 | 4.0% | 440 | 450 |
| | Bear Rd North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Hall Rd North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Turner Too Rd South of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | CR 29 North of SR 70 | 750 | 3.0% | 1,425 | 1,400 | 4.0% | 1,650 | 1,700 |
| | KW Farms Road South of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Lonesome Island Rd North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | JC Durrance Rd South of SR 70 | 150 | 3.0% | 285 | 300 | 4.0% | 330 | 350 |
| | Lykes Ranch Driveway North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | CR 721 (West) South of SR 70 | 1,900 | 3.0% | 3,610 | 3,600 | 4.0% | 4,180 | 4,200 |
| | CR 721 (East) North of SR 70 | 700 | 3.0% | 1,330 | 1,300 | 4.0% | 1,540 | 1,500 |
| | Boney Ln North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Fulmar Terrace South of SR 70 | 150 | 3.0% | 285 | 300 | 4.0% | 330 | 350 |
| | NW New Pine Ridge Rd North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | 175th Terrace North of SR 70 | 250 | 3.0% | 475 | 500 | 4.0% | 550 | 550 |
| | 172nd Terrace (Jordan Terrace) North of SR 70 | 400 | 3.0% | 760 | 750 | 4.0% | 880 | 900 |
| | SW Rucks Dairy Rd South of SR 70 | 300 | 3.0% | 570 | 550 | 4.0% | 660 | 650 |
| | Riverside Rd North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| | Shellcracker Loop North of SR 70 | 150 | 3.0% | 285 | 300 | 4.0% | 330 | 350 |
| | Driveway (across from Shellcracker) South of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 |
| Bream Cove North of SR 70 | 150 | 3.0% | 285 | 300 | 4.0% | 330 | 350 | |
| 144th Pkwy South of SR 70 | 300 | 3.0% | 570 | 550 | 4.0% | 660 | 650 | |
| 141st Ave North of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 | |
| NW 128th Ave North of SR 70 | 400 | 3.0% | 760 | 750 | 4.0% | 880 | 900 | |
| SW 128th Ave South of SR 70 | 100 | 3.0% | 190 | 200 | 4.0% | 220 | 200 | |

Notes:
¹AADT adjusted for balancing between intersections as needed.

3.2.3 Design Year (2052) Directional Design Hourly Volumes (DDHVs) and Turning Movement Volumes

The design year (2052) directional design hourly volumes (DDHVs) were developed in accordance with FDOT's Project Traffic Forecasting Handbook (2019) by applying selected K and D factors to the 2052 AADT values. Peak hour turning movement volumes were developed at study intersections by applying the existing turning movement percentages to the DDHVs. The resulting volume distribution was smoothed to replicate logical corridor distribution, ensuring that calculated values are not lower than existing values and accounting for volume imbalances between intersections (where appropriate). **Table 2-8** in Section 2.3.4 documents the K and D factors used in developing peak hour volumes for both the No-Build and Build scenarios. Also included in **Table 2-8** are the T-factors used in the No-Build and Build analysis.

For both the No-Build and Build scenarios, some manual adjustments were necessary to achieve better balance and proper traffic growth. No-Build AADTs and Hourly Volumes are shown in **Figure 3-3**. Build AADTs and Hourly Volumes are shown in **Figure 3-4**. SR 70 AADTs are only shown on **Figure 3-3** and **Figure 3-4** where counts were collected, but AADT volumes were estimated for the remaining segments to develop DDHVs.



| Legend | |
|---------|--------------------------|
| | Project Limits |
| | Unsignalized (3) |
| XX (XX) | AM(PM) Peak Hour Volumes |
| X,XXX | AADT |
| | Turning Movements |

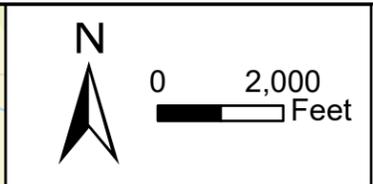
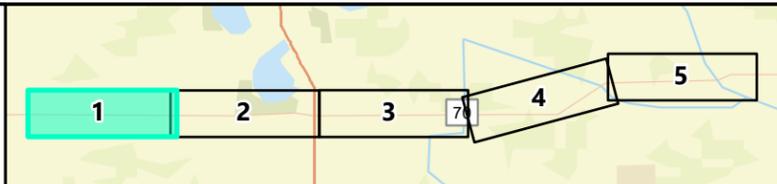
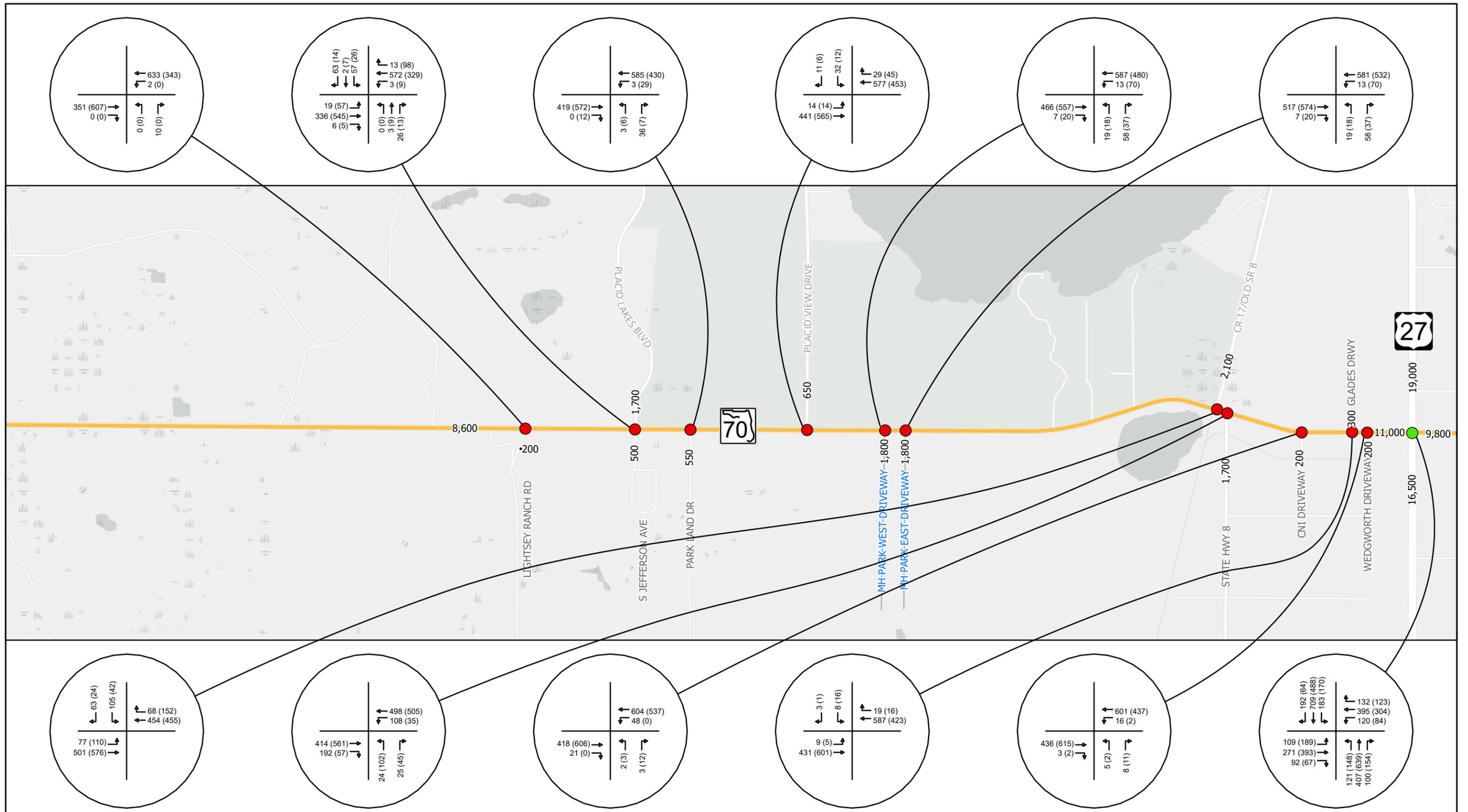


Figure 3-3: Design Year (2052) No-Build AADT and AM (PM) Turning Movement Volumes
Sheet 1 of 5



Legend

- Project Limits
- Unsignalized (12)
- Signalized (1)
- XX (XX) AM(PM) Peak Hour Counts
- X,XXX AADT
- ↑↑↑ Turning Movements

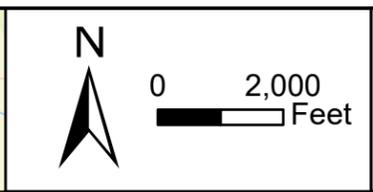
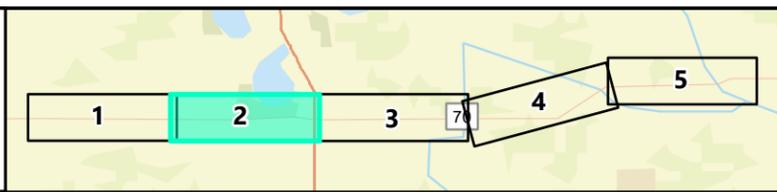
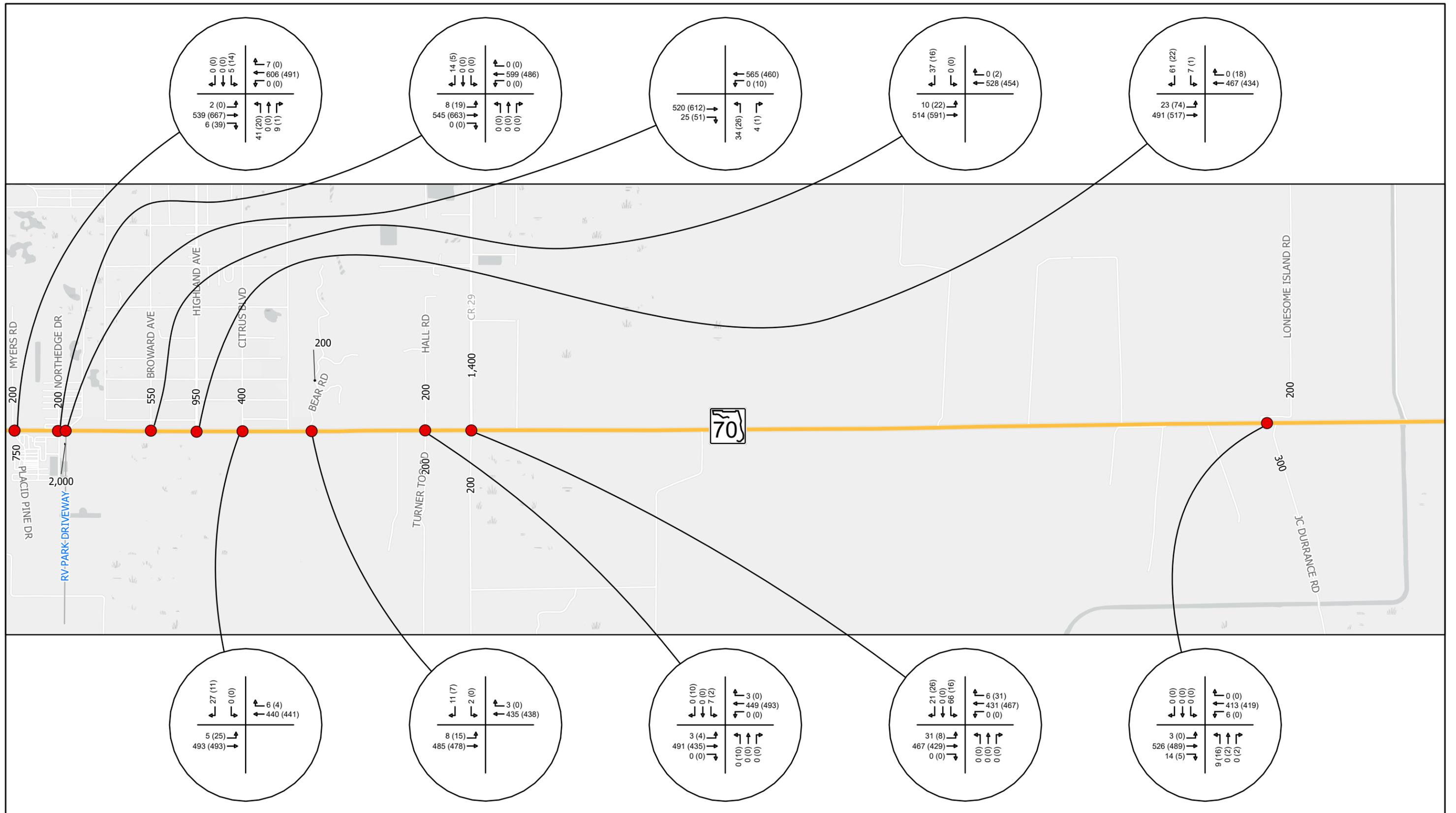


Figure 3-3: Design Year (2052) No-Build AADT and AM (PM) Turning Movement Volumes
Sheet 2 of 5



Legend

- Project Limits
- Unsignalized (10)
- XX (XX) AM(PM) Peak Hour Counts
- X,XXX AADT
- ↑↑↑ Turning Movements

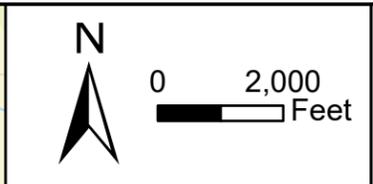
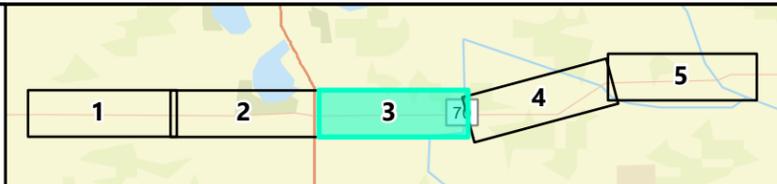
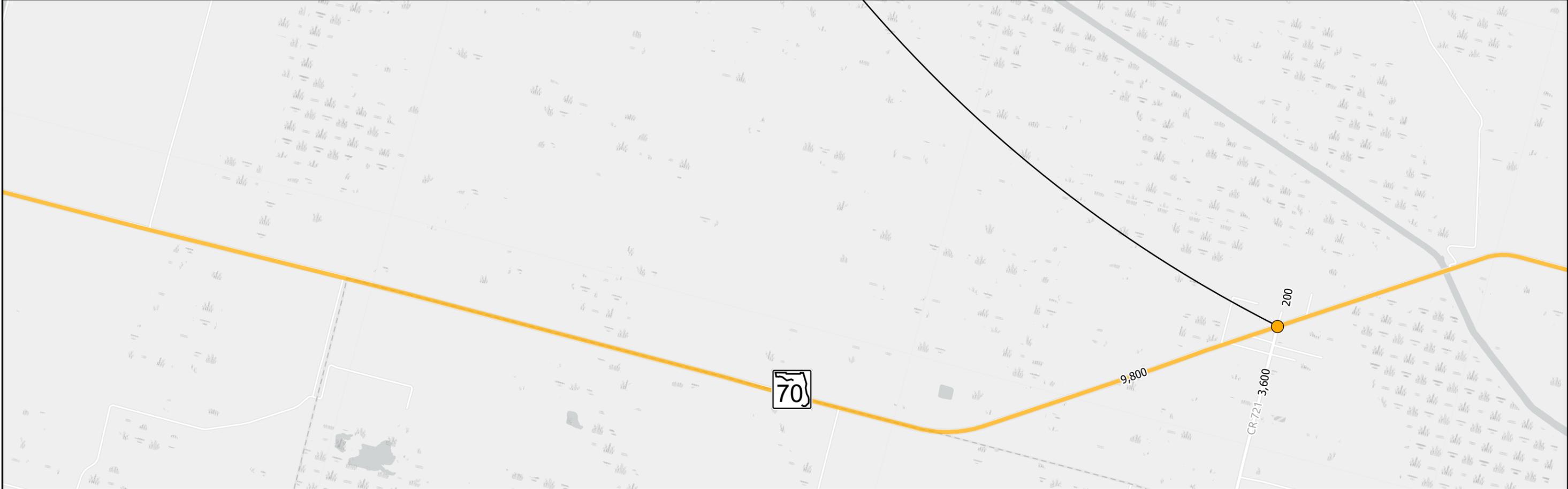
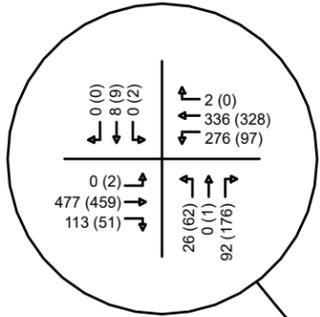


Figure 3-3: Design Year (2052) No-Build AADT and AM (PM) Turning Movement Volumes
Sheet 3 of 5



Legend

- Project Limits
- Flashing Yellow (1)

XX (XX) AM(PM) Peak Hour Counts
 X,XXX AADT
 ↑↑↑ Turning Movements

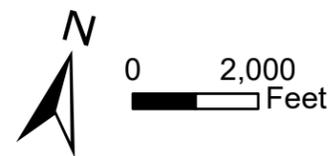
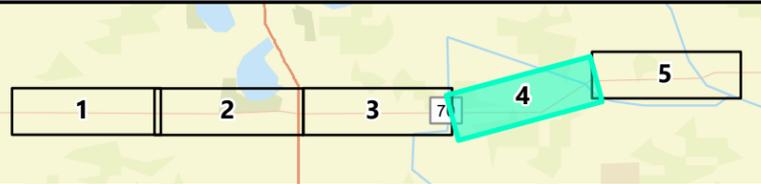
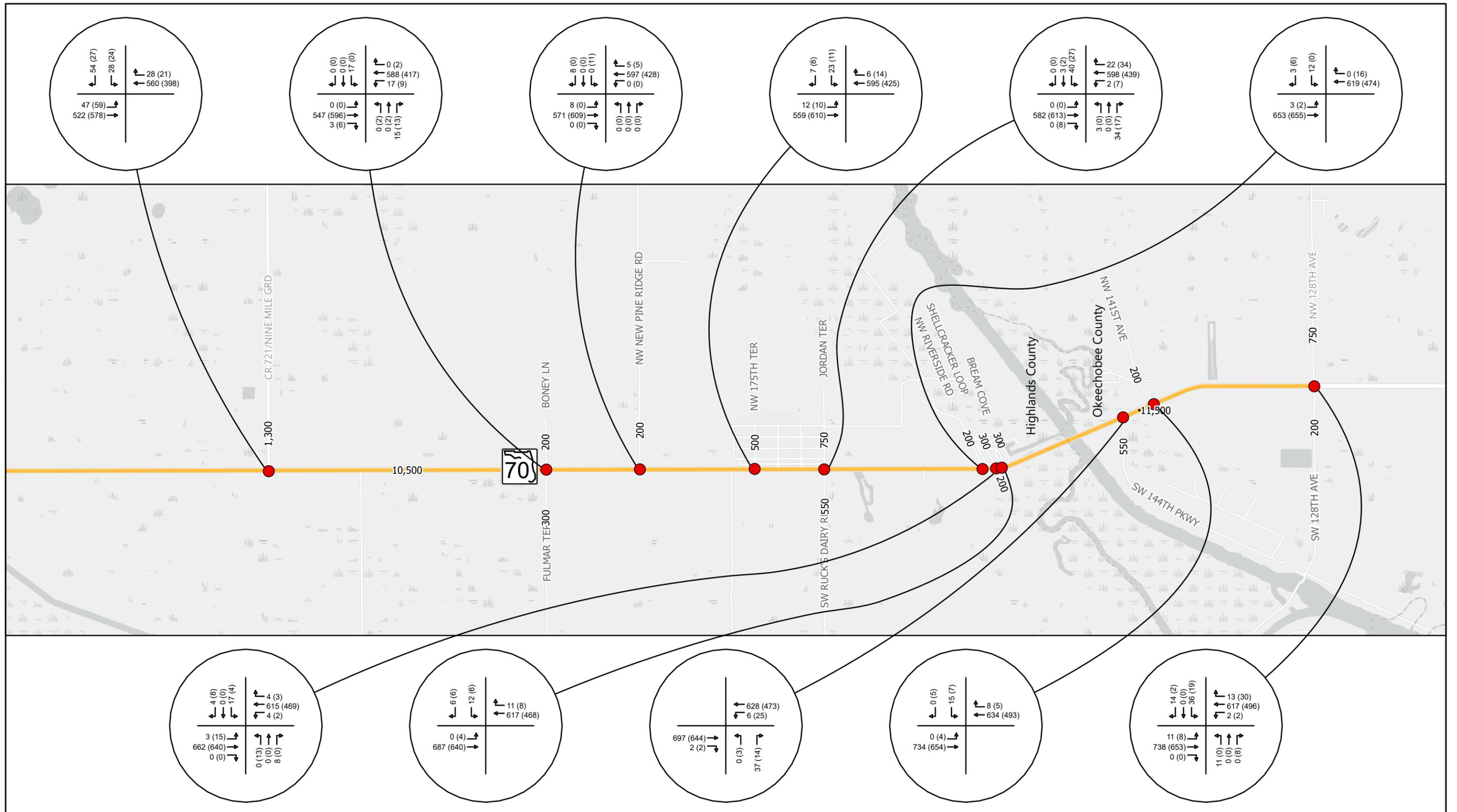


Figure 3-3: Design Year (2052) No-Build AADT and AM (PM) Turning Movement Volumes
 Sheet 4 of 5



Legend

- Project Limits
- Unsignalized (11)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- ↑↑↑ Turning Movements

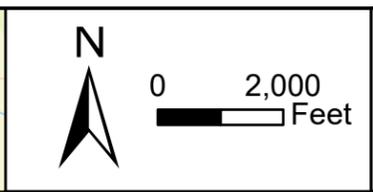
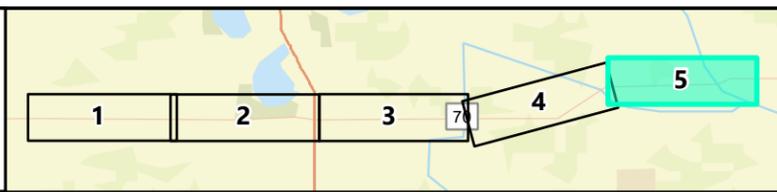
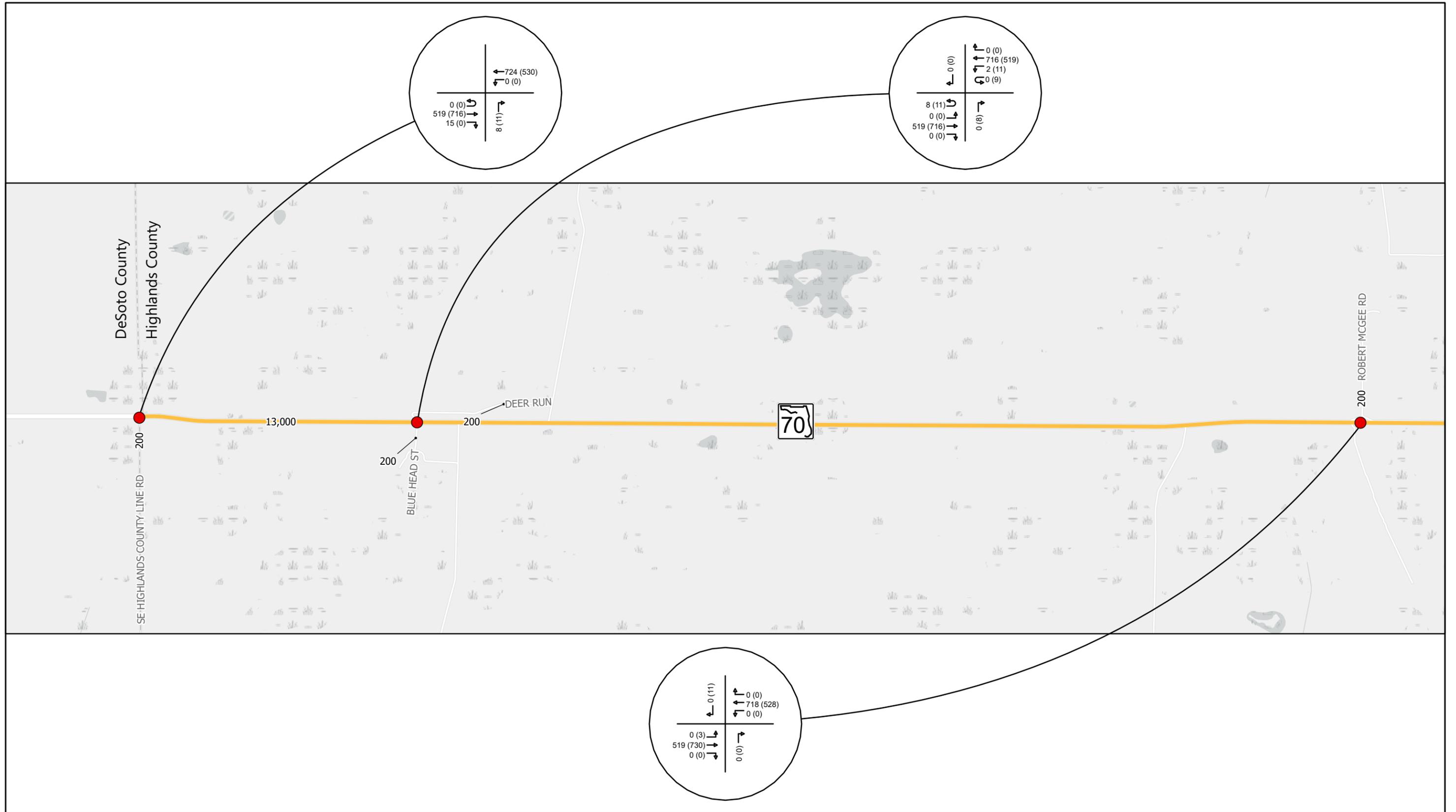


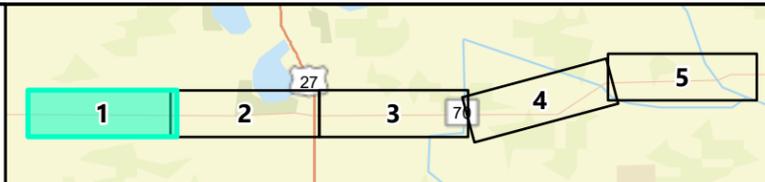
Figure 3-3: Design Year (2052) No-Build AADT and AM (PM) Turning Movement Volumes
Sheet 5 of 5



Legend

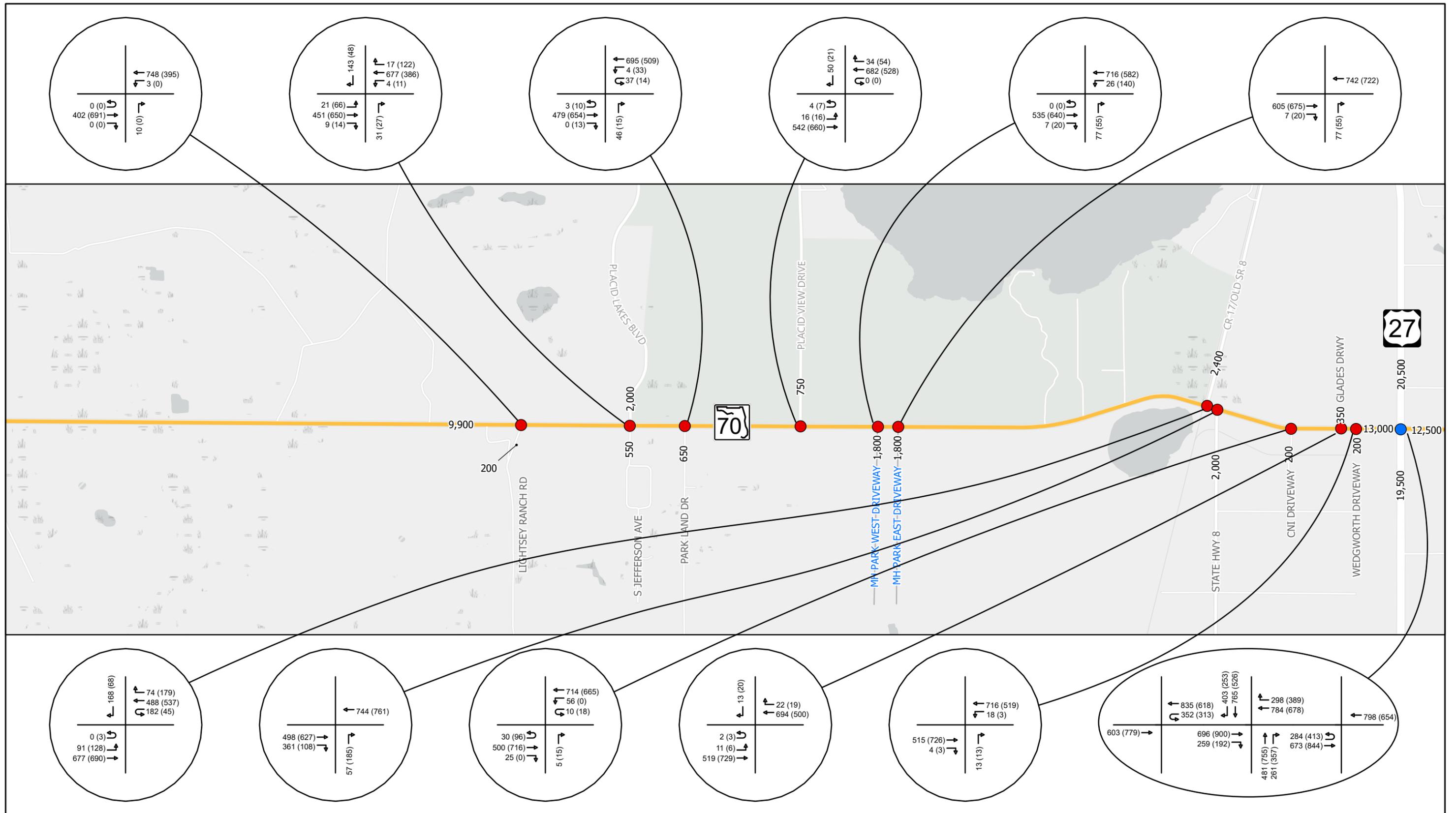
- Project Limits
- Unsignalized (3)

XX (XX) AM (PM) Peak Hour Volumes
 X,XXX AADT
 ↑↑↑ Turning Movements



0 2,000 Feet

Figure 3-4: Design Year (2052) Build AADT and AM (PM) Turning Movement Volumes
 Sheet 1 of 5



Legend

- Project Limits
- Unsignalized (12)
- Median U-Turn (MUT) (1)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- Turning Movements

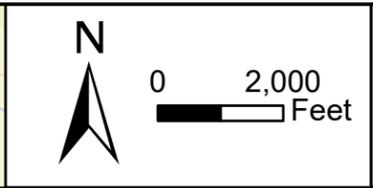
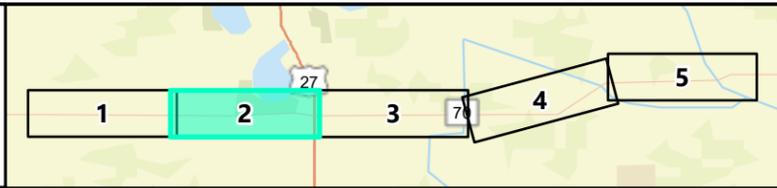
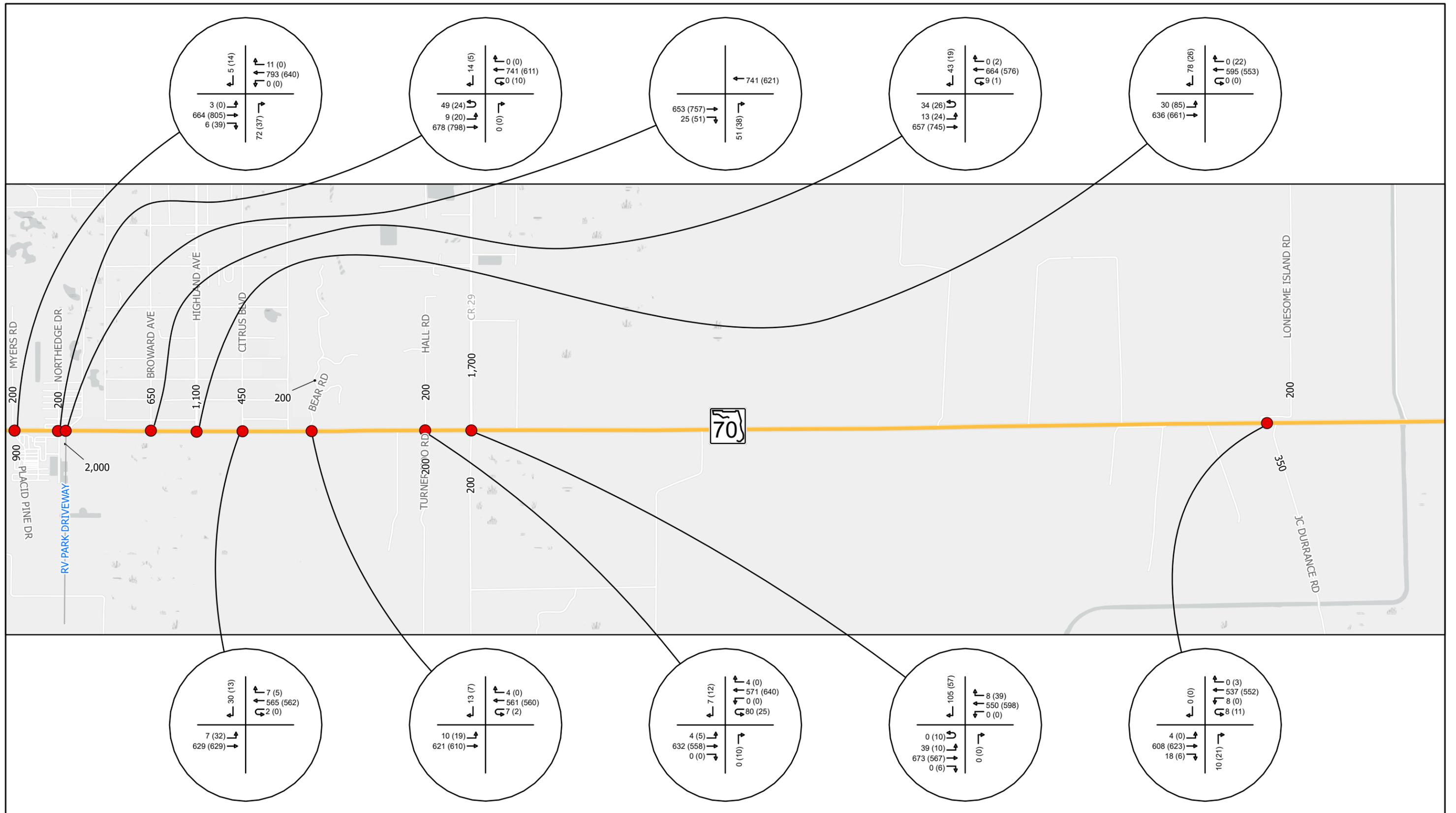


Figure 3-4: Design Year (2052) Build AADT and AM (PM) Turning Movement Volumes
Sheet 2 of 5



Legend

- Project Limits
- Unsignalized (10)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- ↑↑↑ Turning Movements

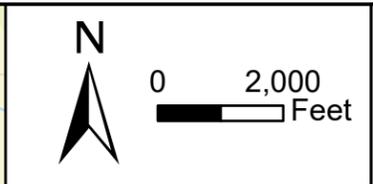
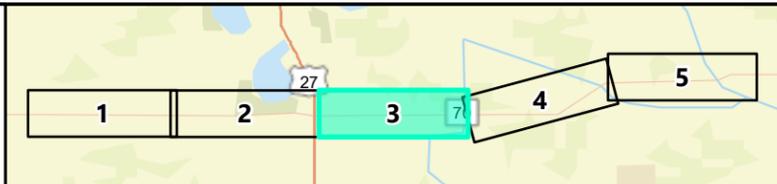
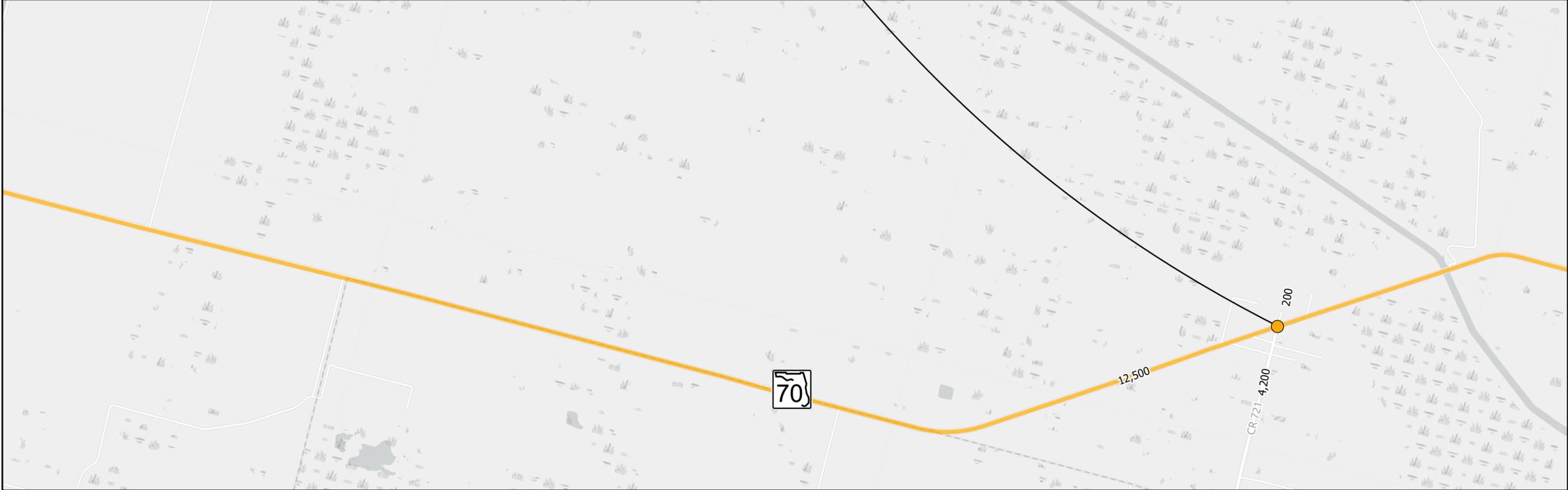
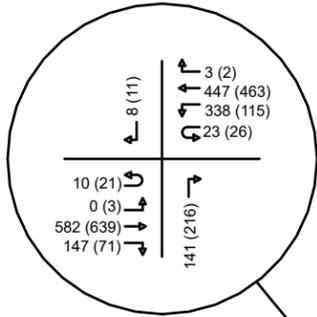


Figure 3-4: Design Year (2052) Build AADT and AM (PM) Turning Movement Volumes
Sheet 3 of 5



Legend

- Project Limits
- Flashing Yellow (1)

- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- ↖ ↗ ↘ Turning Movements

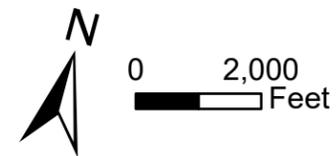
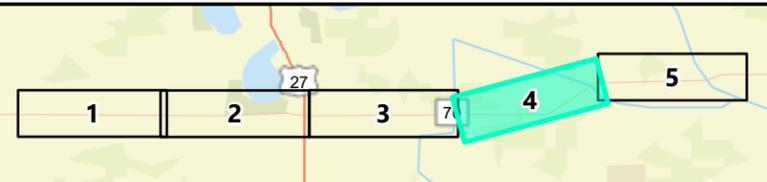
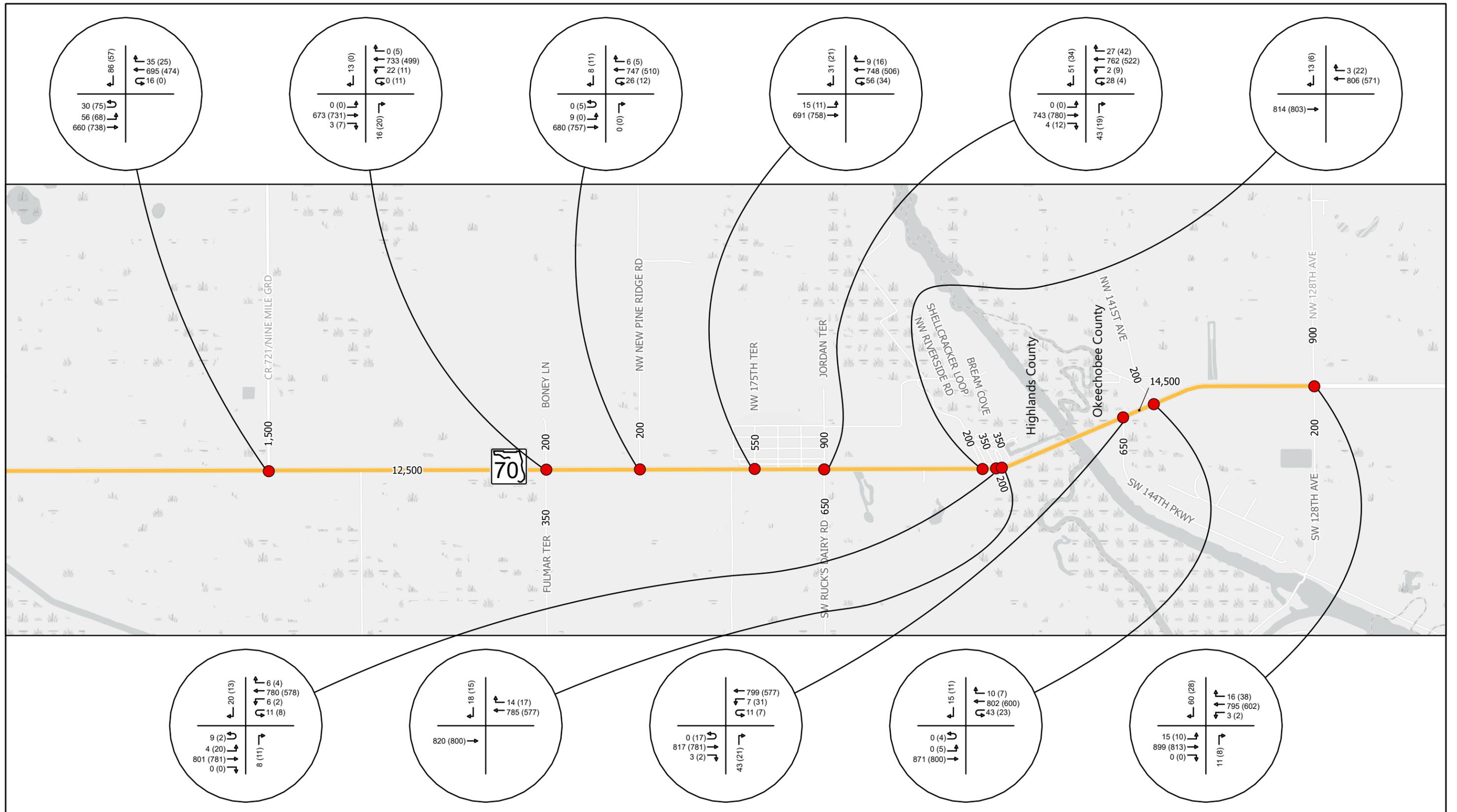


Figure 3-4: Design Year (2052) Build
AADT and AM (PM) Turning Movement
Volumes
Sheet 4 of 5



Legend

- Project Limits
- Unsignalized (11)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- ↑↑↑ Turning Movements

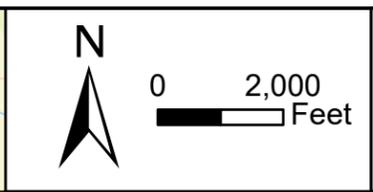
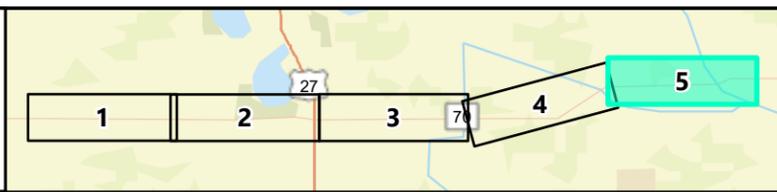


Figure 3-4: Design Year (2052) Build AADT and AM (PM) Turning Movement Volumes
Sheet 5 of 5

3.3 Development of Opening Year (2032) Traffic Volumes

The following sections document the development of the daily and peak hour opening year traffic volumes.

3.3.1 Opening Year (2032) AADTs

Opening year daily (AADT) volumes were developed for the No-Build and Build Alternatives through linear interpolation. The Existing (2022) AADTs and the Design Year (2052) AADTs were used to calculate AADTs for an opening year of 2032. Two new developments will also be completed by the opening year: a Recreational Vehicle Park and Mobile Home Park are expected to be constructed off SR 70 in the project limits. AADTs for the driveways accessing these developments were estimated using the ITE Trip Generation Handbook (11th Edition). The supporting trip generation documents can be found in **Appendix E**. In both the No-Build and Build scenarios, some manual adjustments of AADTs were required to maintain AADT balance. **Table 3-3** shows Opening Year No-Build and Build AADT development.

Table 3-3: Opening Year No-Build and Build AADT

| Location | | Existing | No-Build | | | Build | | | |
|---|--|--------------------|----------------------|-------------------|---------------------------|----------------------|-------------------|---------------------------|--|
| | | 2022 Existing AADT | Selected Growth Rate | Opening Year AADT | Rounded Opening Year AADT | Selected Growth Rate | Opening Year AADT | Rounded Opening Year AADT | |
| SR 70 | West of County Line to Robert McGee Rd | 5,800 | 3.0% | 7,540 | 7,500 | 4.0% | 8,120 | 8,100 | |
| | Between Robert McGee Rd and Lightsey Ranch Rd | 5,000 | | 6,500 | 6,500 | | 7,000 | 7,000 | |
| | West of Lightsey Ranch Rd to Placid Lakes Blvd | 4,500 | | 5,850 | 5,900 | | 6,300 | 6,300 | |
| | Between Lightsey Ranch Rd and Placid Lakes Blvd | | | | | | | | |
| | Between Placid Lakes Blvd and Park Land Dr | | | | | | | | |
| | Between Park Land Dr and Placid View Dr | | | | | | | | |
| | Between Placid View Dr and Old SR 8 (West) | | | | | | | | |
| | Between Old SR 8 (West) and Old SR 8 (East) | 5,100 | 4.0% | 7,140 | 7,100 | 5.0% | 7,650 | 7,700 | |
| | Between Old SR 8 (East) and Distribution Blvd | | | | | | | | |
| | Between Distribution Blvd and Glades Driveway | | | | | | | | |
| | Between Glades Driveway and Wedgeworth Driveway | | | | | | | | |
| | Between Wedgeworth Driveway and US 27 | | | | | | | | |
| | Between US 27 and Myers Rd/Placid Pines Dr | | | | | | | | |
| | Between Myers Rd/Placid Pines Dr and North Edge Dr | | | | | | | | |
| | Between North Edge Dr and Broward Ave | 5,600 | 2.5% | 7,000 | 7,000 | 4.0% | 7,840 | 7,800 | |
| | Between Broward Ave and Highlands Ave | | | | | | | | |
| | Between Highlands Ave and Citrus Blvd | | | | | | | | |
| | Between Citrus Blvd and Bear Rd | | | | | | | | |
| | Between Bear Rd and Hall Rd | | | | | | | | |
| | Between Hall Rd and CR 29 | 5,600 | 2.5% | 7,000 | 7,000 | 4.0% | 7,840 | 7,800 | |
| Between CR 29 and Lonesome Island Rd | | | | | | | | | |
| Between Lonesome Island Rd and CR 721 South | | | | | | | | | |
| Between CR 721 South and CR 721 North | | | | | | | | | |
| Between CR 721 North and Boney Ln/Fulmar Terr | | | | | | | | | |
| Between Boney Ln/Fulmar Terr and NW New Pine Ridge Rd | 5,400 | 3.0% | 7,020 | 7,000 | 4.5% | 7,830 | 7,800 | | |
| Between NW New Pine Ridge Rd and 175th Terr | | | | | | | | | |
| Between 175th Terr and 172nd Terr/SW Rucks Dairy Rd | | | | | | | | | |

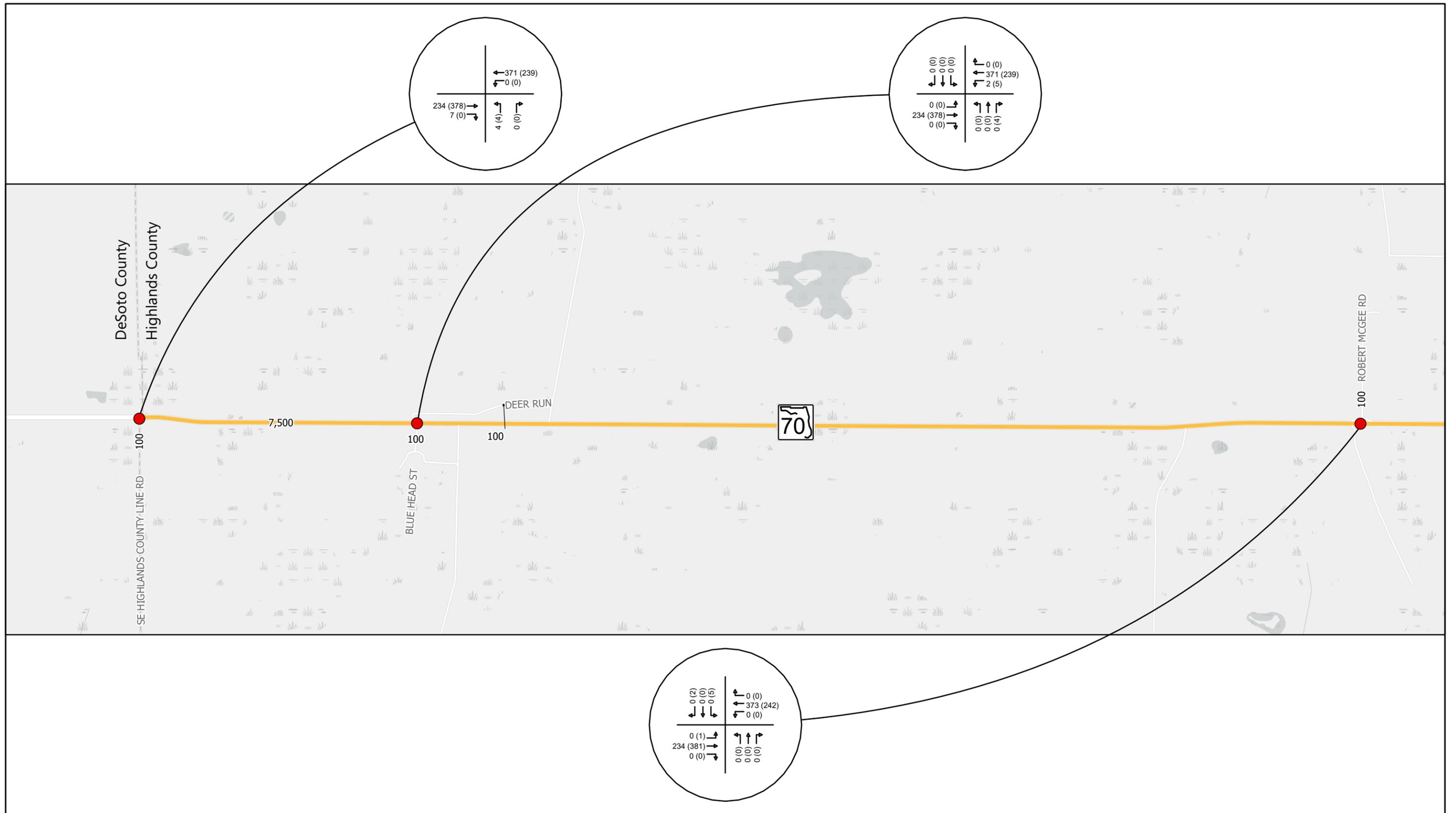
| Location | | Existing | No-Build | | | Build | | |
|-----------------------------|---|--------------------|----------------------|-------------------|---------------------------|----------------------|-------------------|---------------------------|
| | | 2022 Existing AADT | Selected Growth Rate | Opening Year AADT | Rounded Opening Year AADT | Selected Growth Rate | Opening Year AADT | Rounded Opening Year AADT |
| SR 70 | Between 172nd Terr/SW Rucks Dairy Rd and Riverside Rd | 5,400 | 3.0% | 7,020 | 7,000 | 4.5% | 7,830 | 7,800 |
| | Between Riverside Rd and Shellcracker Loop | | | | | | | |
| | Between Shellcracker Loop and Bream Cove | | | | | | | |
| | Between Bream Cove and 144th Pkwy | 6,100 | | 7,930 | 7,900 | | 8,845 | 8,800 |
| | Between 144th Pkwy and 141st Ave | | | | | | | |
| | Between 141st Ave and NW 128th Ave | | | | | | | |
| | East of NW 128th Ave | | | | | | | |
| Side Streets | Highlands County Line Rd South of SR 70 | 100 | 2.0% | 120 | 100 | 3.0% | 130 | 150 |
| | Deer Run Rd North of SR 70 | 100 | 2.0% | 120 | 100 | 3.0% | 130 | 150 |
| | Blue Head Street South of SR 70 | 100 | 3.0% | 130 | 100 | 4.0% | 140 | 150 |
| | Robert McGee Rd North of SR 70 | 100 | 3.0% | 130 | 100 | 4.0% | 140 | 150 |
| | Lightsey Ranch Rd South of SR 70 | 100 | 3.0% | 130 | 100 | 4.0% | 140 | 150 |
| | Placid Lakes Blvd North of SR 70 | 900 | 3.0% | 1,170 | 1,200 | 4.0% | 1,260 | 1,300 |
| | Jefferson Ave South of SR 70 | 250 | 3.0% | 325 | 350 | 4.0% | 350 | 350 |
| | Park Land Dr South of SR 70 | 300 | 3.0% | 390 | 400 | 4.0% | 420 | 400 |
| | Placid View Dr North of SR 70 | 350 | 3.0% | 455 | 450 | 4.0% | 490 | 500 |
| | Old SR 8 (West) North of SR 70 | 1,100 | 3.0% | 1,430 | 1,400 | 4.0% | 1,540 | 1,500 |
| | Old SR 8 (East) South of SR 70 | 900 | 3.0% | 1,170 | 1,200 | 4.0% | 1,260 | 1,300 |
| | Distribution Blvd (CNI Driveway) South of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | Glades Driveway North of SR 70 | 150 | 3.0% | 195 | 200 | 4.0% | 210 | 200 |
| | Wedgeworth Driveway South of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | US 27 North of SR 70 | 9,400 | 3.5% | 12,690 | 12,500 | 4.0% | 13,160 | 13,000 |
| | US 27 South of SR 70 | 8,800 | 3.0% | 11,440 | 11,500 | 4.0% | 12,320 | 12,500 |
| | Myers Rd North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | Placid Pines Dr South of SR 70 | 400 | 3.0% | 520 | 500 | 4.0% | 560 | 550 |
| | North Edge Dr North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | Broward Ave North of SR 70 | 300 | 3.0% | 390 | 400 | 4.0% | 420 | 400 |
| Highland Ave North of SR 70 | 500 | 3.0% | 650 | 650 | 4.0% | 700 | 700 | |

| Location | | Existing | No-Build | | | Build | | |
|-----------------------------|--|--------------------|----------------------|-------------------|---------------------------|----------------------|-------------------|---------------------------|
| | | 2022 Existing AADT | Selected Growth Rate | Opening Year AADT | Rounded Opening Year AADT | Selected Growth Rate | Opening Year AADT | Rounded Opening Year AADT |
| Side Streets | Citrus Blvd North of SR 70 | 200 | 3.0% | 260 | 250 | 4.0% | 280 | 300 |
| | Bear Rd North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | Hall Rd North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | Turner Too Rd South of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | CR 29 North of SR 70 | 750 | 3.0% | 975 | 1,000 | 4.0% | 1,050 | 1,100 |
| | KW Farms Road South of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | Lonesome Island Rd North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | JC Durrance Rd South of SR 70 | 150 | 3.0% | 195 | 200 | 4.0% | 210 | 200 |
| | Lykes Ranch Driveway North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | CR 721 (West) South of SR 70 | 1,900 | 3.0% | 2,470 | 2,500 | 4.0% | 2,660 | 2,700 |
| | CR 721 (East) North of SR 70 | 700 | 3.0% | 910 | 900 | 4.0% | 980 | 1,000 |
| | Boney Ln North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | Fulmar Terrace South of SR 70 | 150 | 3.0% | 195 | 200 | 4.0% | 210 | 200 |
| | NW New Pine Ridge Rd North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | 175th Terrace North of SR 70 | 250 | 3.0% | 325 | 350 | 4.0% | 350 | 350 |
| | 172nd Terrace (Jordan Terrace) North of SR 70 | 400 | 3.0% | 520 | 500 | 4.0% | 560 | 550 |
| | SW Rucks Dairy Rd South of SR 70 | 300 | 3.0% | 390 | 400 | 4.0% | 420 | 400 |
| | Riverside Rd North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| | Shellcracker Loop North of SR 70 | 150 | 3.0% | 195 | 200 | 4.0% | 210 | 200 |
| | Driveway (across from Shellcracker) South of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 |
| Bream Cove North of SR 70 | 150 | 3.0% | 195 | 200 | 4.0% | 210 | 200 | |
| 144th Pkwy South of SR 70 | 300 | 3.0% | 390 | 400 | 4.0% | 420 | 400 | |
| 141st Ave North of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 | |
| NW 128th Ave North of SR 70 | 400 | 3.0% | 520 | 500 | 4.0% | 560 | 550 | |
| SW 128th Ave South of SR 70 | 100 | 3.0% | 130 | 150 | 4.0% | 140 | 150 | |

3.3.2 Opening Year (2032) Directional Design Hourly Volumes (DDHVs) and Turning Movement Volumes

Opening year (2032) directional design hourly volumes (DDHVs) were developed slightly differently for the No-Build and Build scenarios due to differences in access points along the corridor. The Opening Year No-Build turning movement volumes were linearly interpolated between Existing and Design Year No-Build turning movement volumes. The Opening Year Build DDHVs were linearly interpolated between Existing and Design Year Build DDHVs. Design Year Build turning movement percentages were then applied to develop Opening Year turning movement volumes. The resulting volume distribution was smoothed to replicate logical corridor distribution, ensuring that calculated values are not lower than existing values and accounting for volume imbalances between intersections (where appropriate).

For both the No-Build and Build scenarios, some manual adjustments were necessary to achieve better balance and appropriate traffic growth. Opening Year No-Build AADTs and Hourly Volumes are shown in **Figure 3-5**. Opening Year Build AADTs and Hourly Volumes are shown in **Figure 3-6**. SR 70 AADTs are only shown on **Figure 3-5** and **Figure 3-6** where counts were collected, but AADT volumes were estimated for the remaining segments to develop DDHVs.



Legend

- Project Limits
- Unsignalized (3)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- Turning Movements

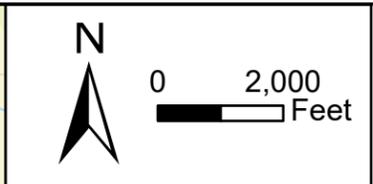
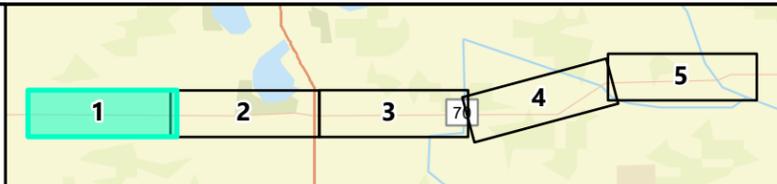
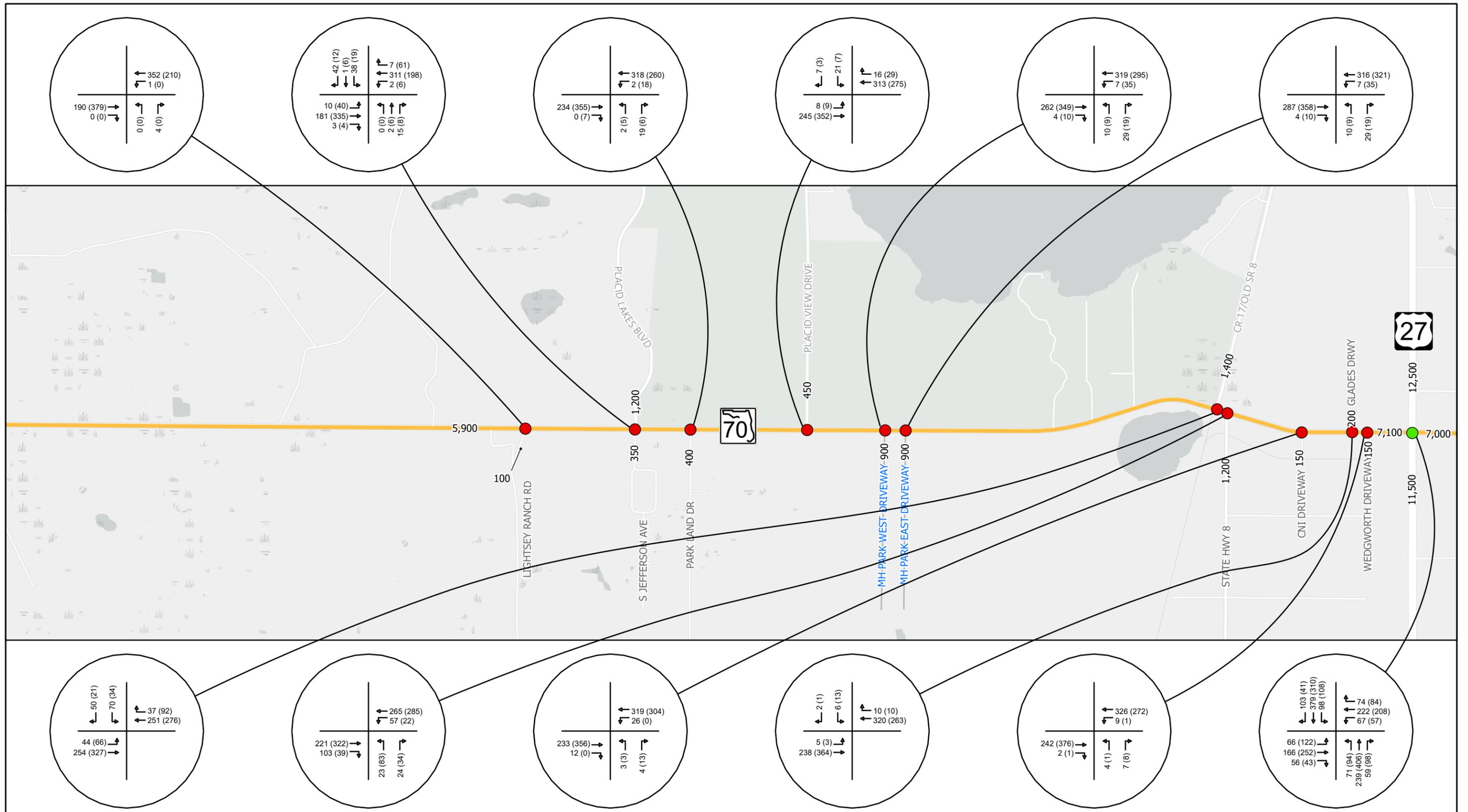


Figure 3-5: Opening Year (2032) No-Build AADT and AM (PM) Turning Movement Volumes
Sheet 1 of 5



Legend

- Project Limits
- Unsignalized (12)
- Signalized (1)

XX (XX) AM(PM) Peak Hour Volumes
 X,XXX AADT
 ↑↑↑ Turning Movements

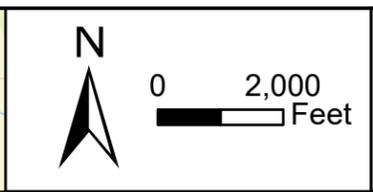
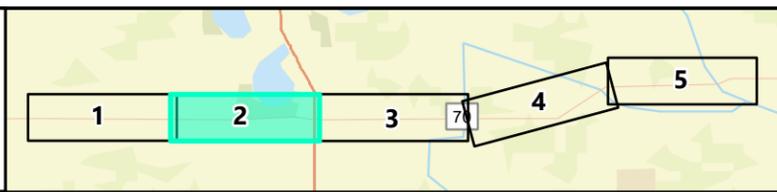
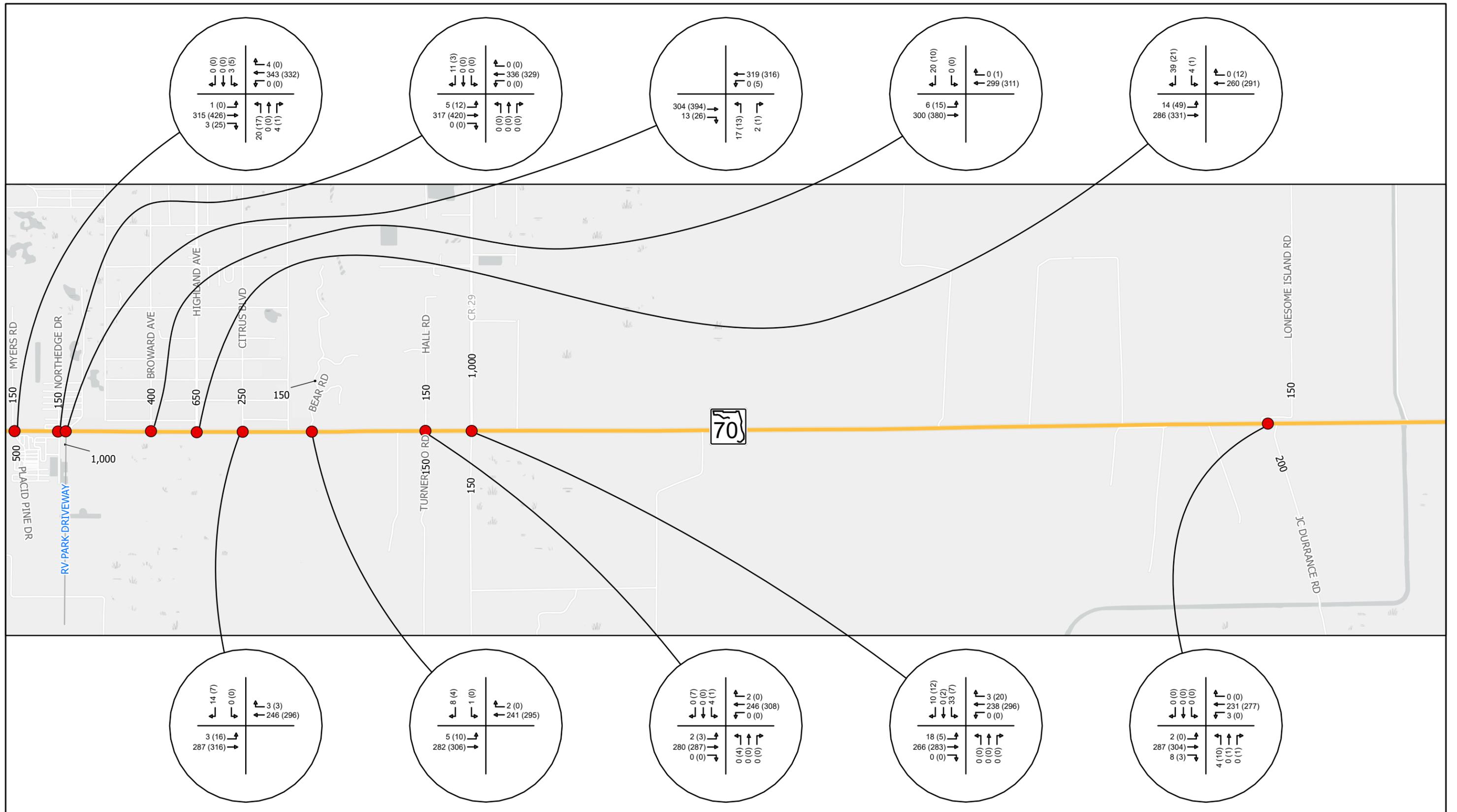


Figure 3-5: Opening Year (2032) No-Build AADT and AM (PM) Turning Movement Volumes
 Sheet 2 of 5



Legend

- Project Limits
- Unsignalized (10)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- Turning Movements

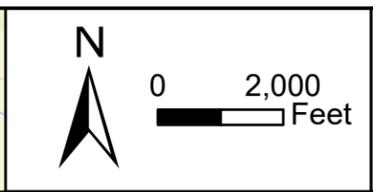
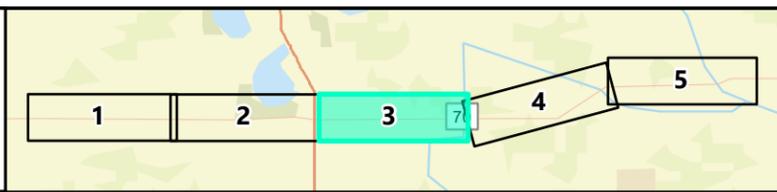
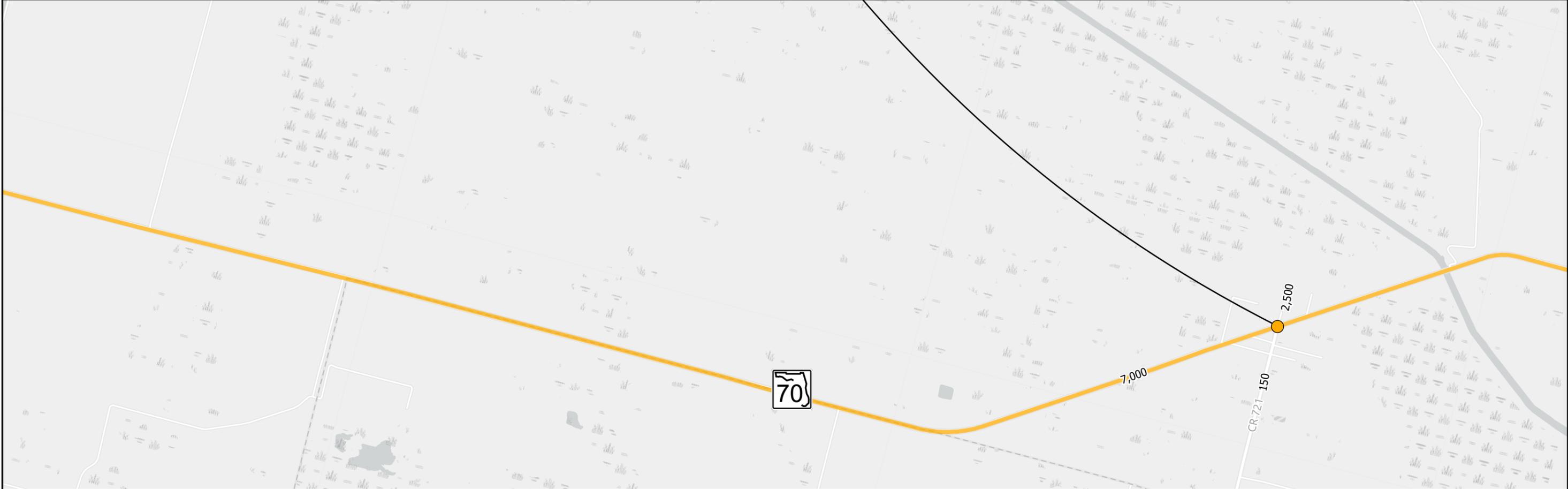
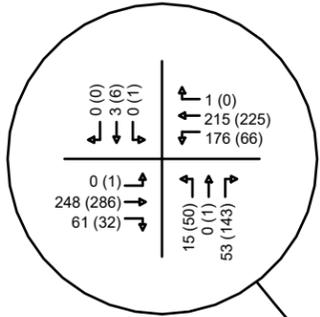


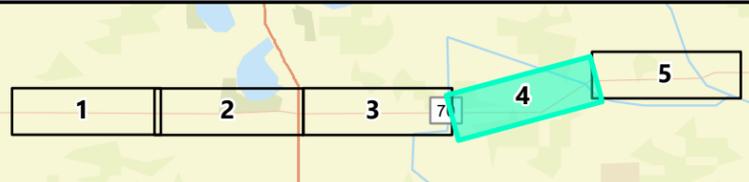
Figure 3-5: Opening Year (2032) No-Build AADT and AM (PM) Turning Movement Volumes
Sheet 3 of 5



Legend

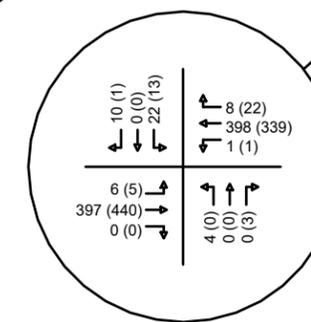
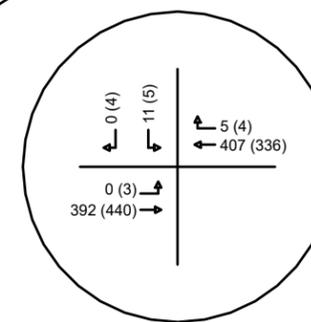
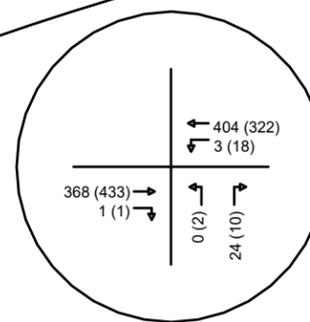
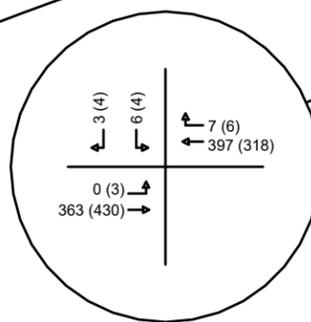
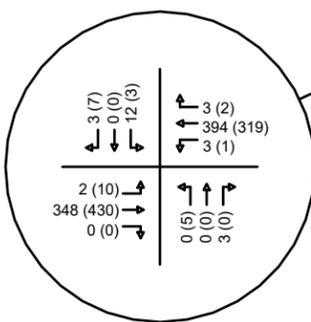
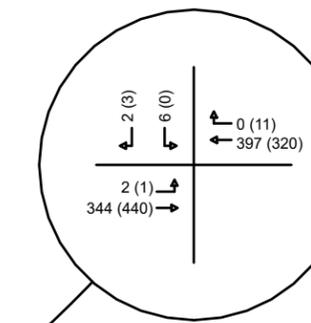
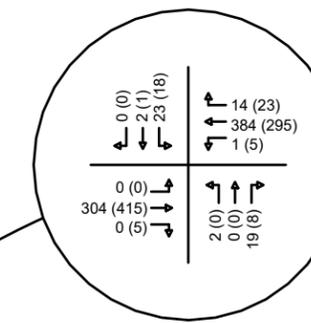
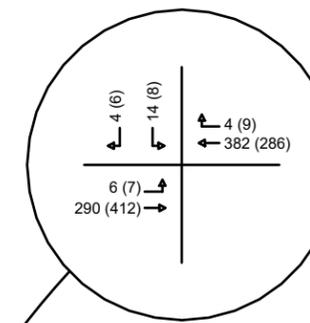
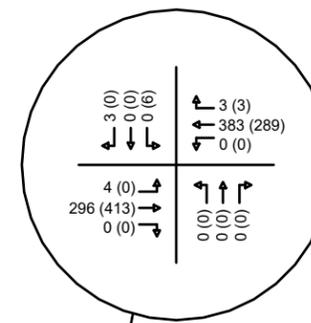
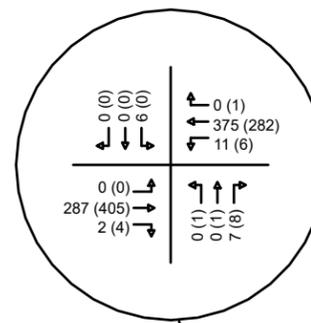
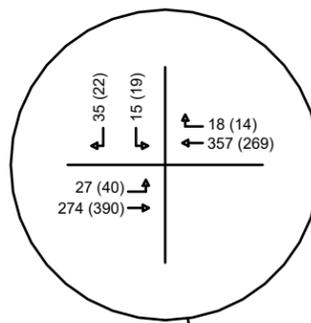
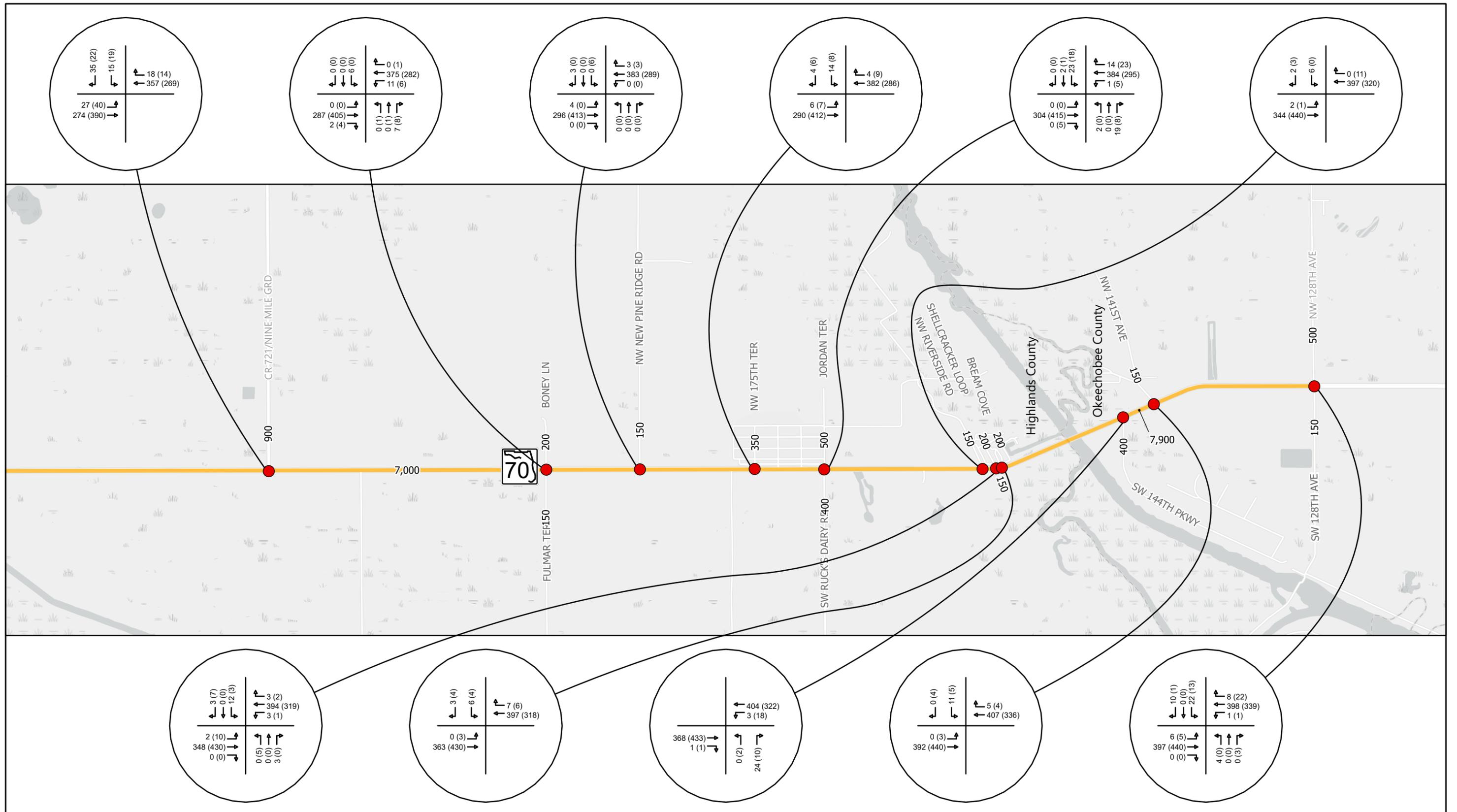
- Project Limits
- Flashing Yellow (1)

XX (XX) AM(PM) Peak Hour Volumes
 X,XXX AADT
 Turning Movements



0 2,000 Feet

Figure 3-5: Opening Year (2032) No-Build AADT and AM (PM) Turning Movement Volumes
 Sheet 4 of 5



Legend
 Project Limits
 Unsignalized (11)

XX (XX) AM(PM) Peak Hour Volumes
 X,XXX AADT
 Turning Movements

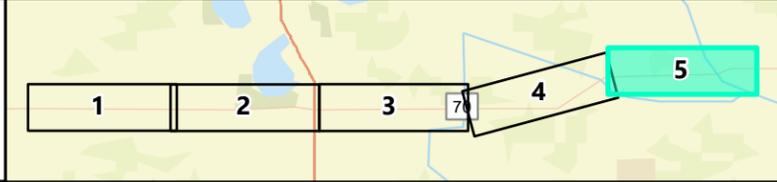
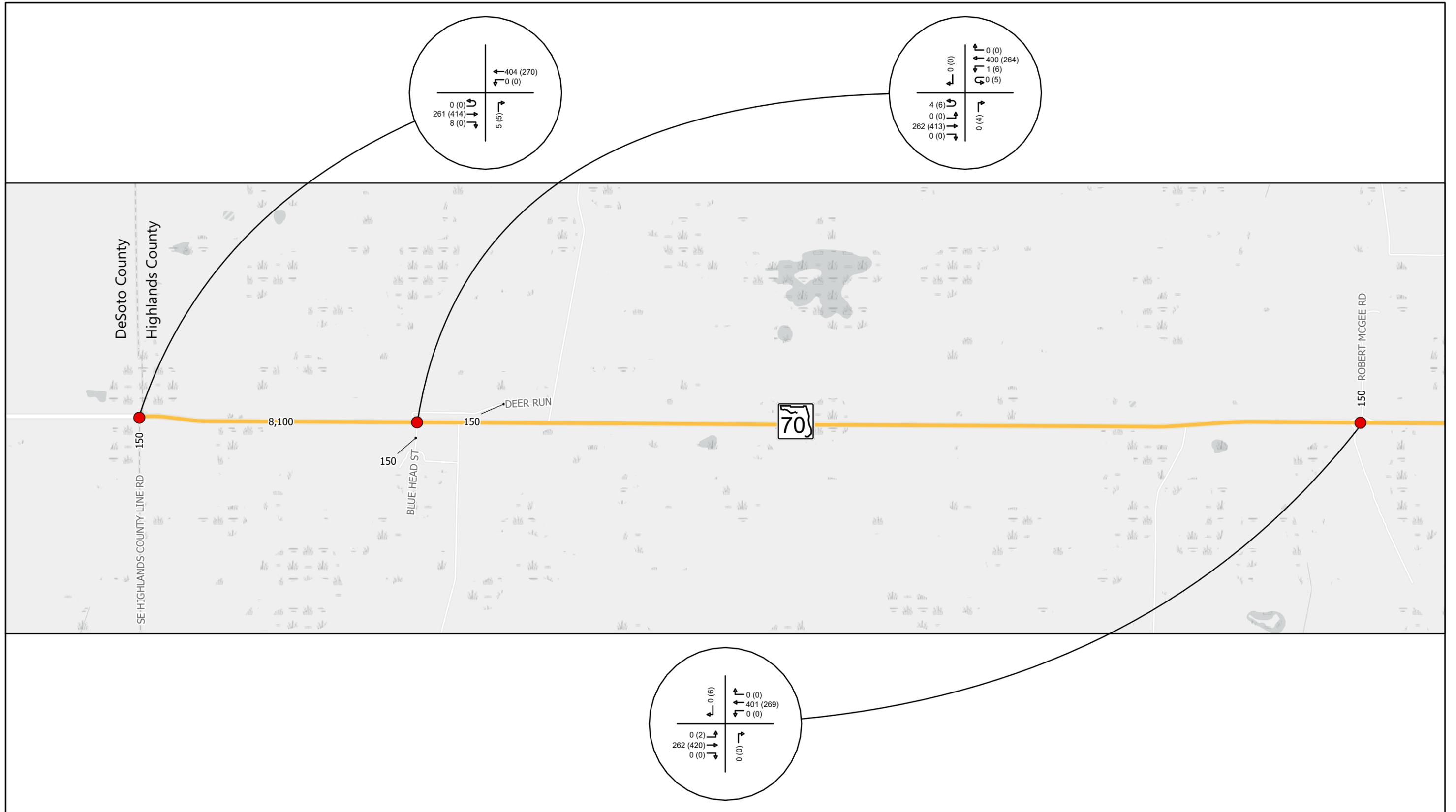


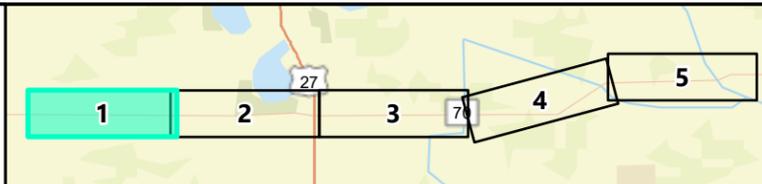
Figure 3-5: Opening Year (2032) No-Build AADT and AM (PM) Turning Movement Volumes
 Sheet 5 of 5



Legend

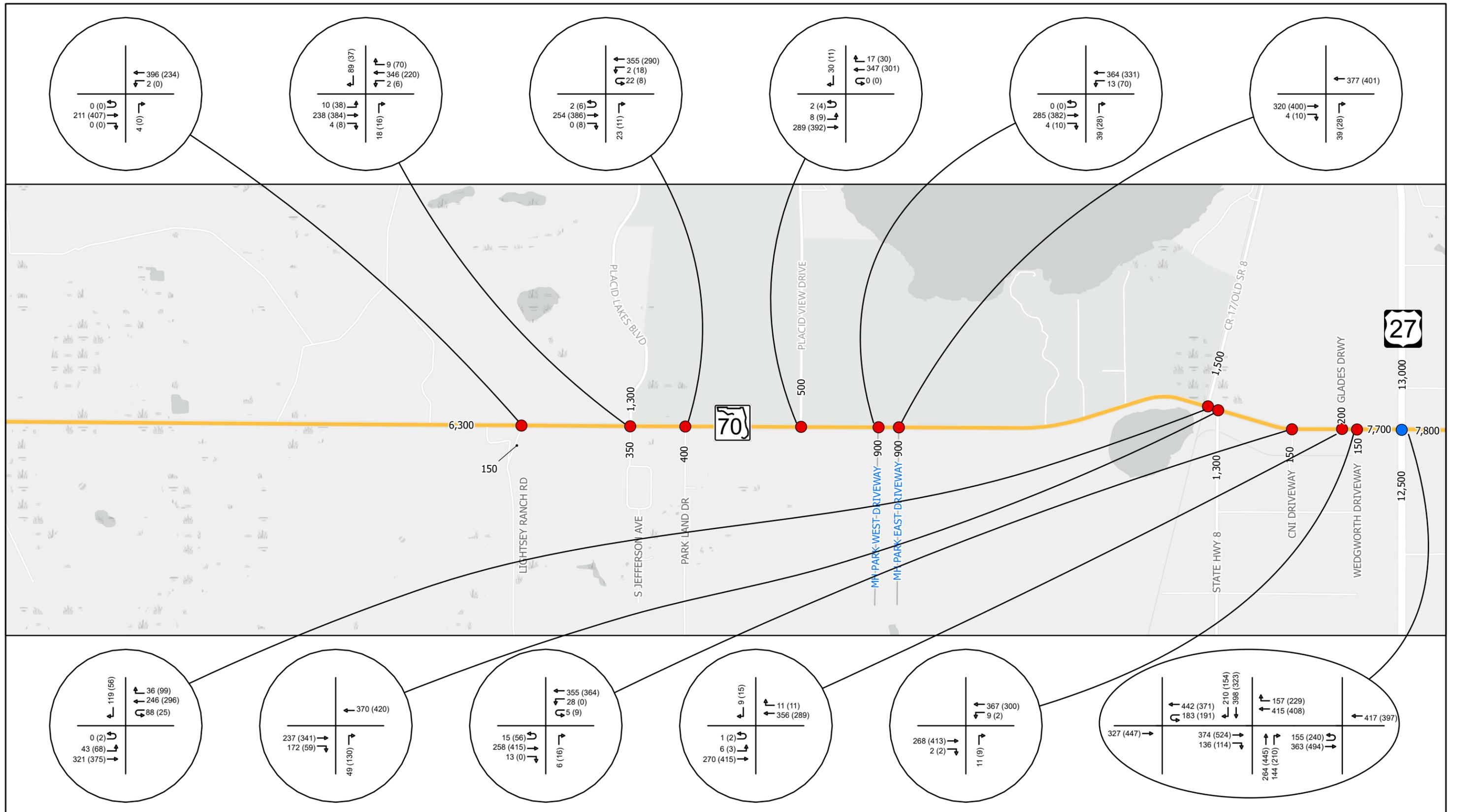
- Project Limits
- Unsignalized (3)

- XX (XX) AM (PM) Peak Hour Volumes
- X,XXX AADT
- ↑↑↑ Turning Movements



0 2,000 Feet

Figure 3-6: Opening Year (2032) Build AADT and AM (PM) Turning Movement Volumes
Sheet 1 of 5



Legend

- Project Limits
- Unsignalized (12)
- Median U-Turn (MUT) (1)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- ↑↑↑ Turning Movements

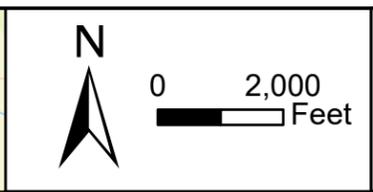
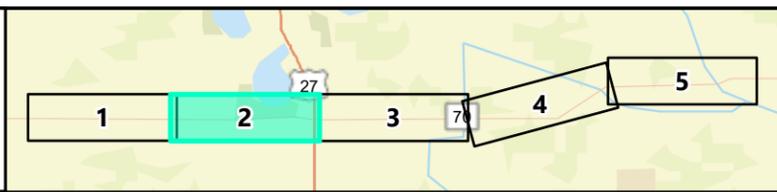
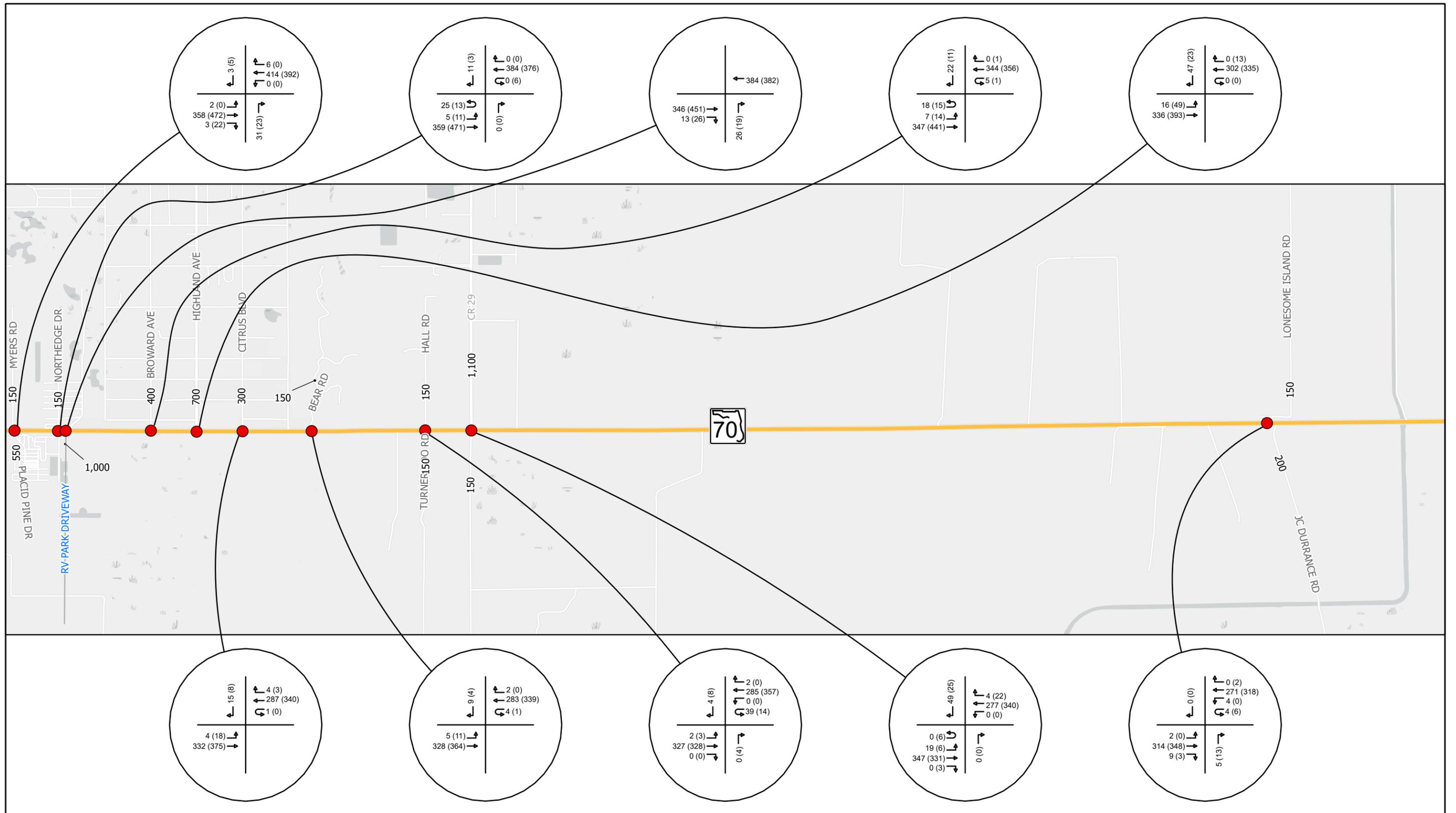


Figure 3-6: Opening Year (2032) Build AADT and AM (PM) Turning Movement Volumes
Sheet 2 of 5



Legend

- Project Limits
- Unsignalized (10)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- Turning Movements

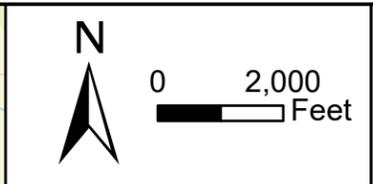
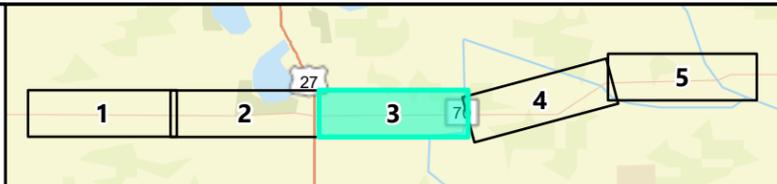
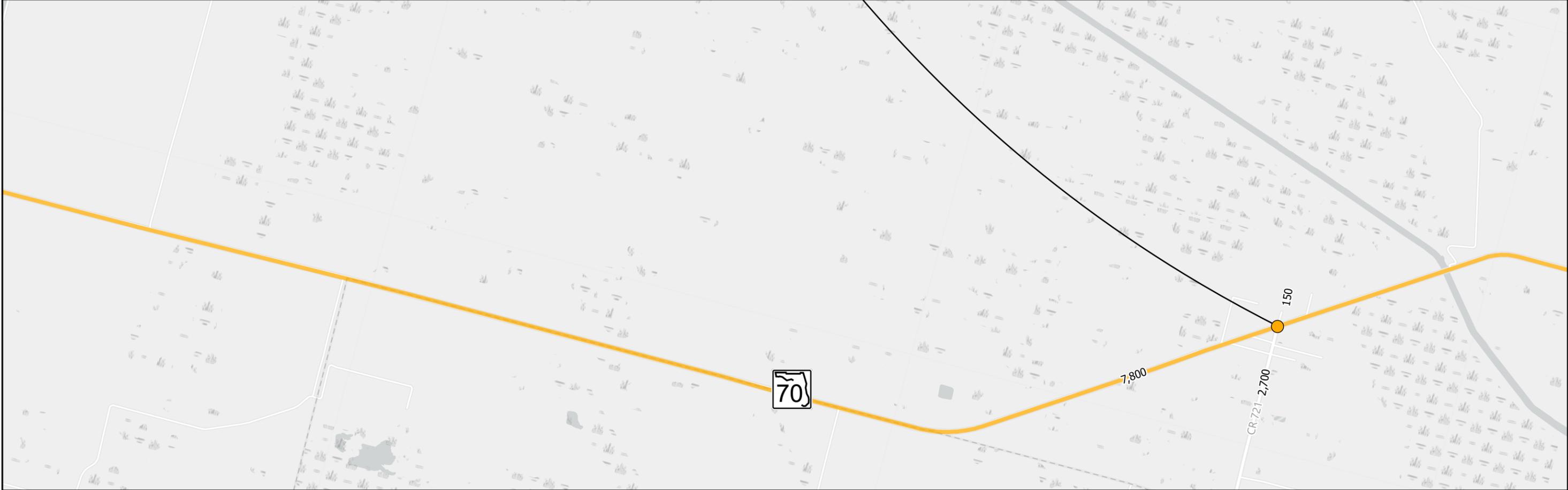
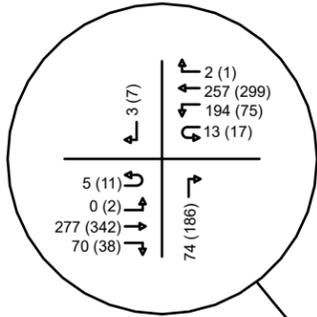


Figure 3-6: Opening Year (2032) Build AADT and AM (PM) Turning Movement Volumes
Sheet 3 of 5



Legend

- Project Limits
- Flashing Yellow (1)

- XX (XX) AM(PM) Peak Hour Counts
- X,XXX AADT
- ↑↑↑ Turning Movements

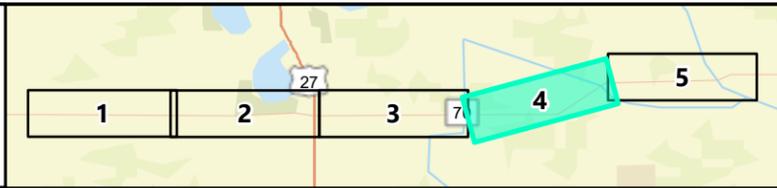
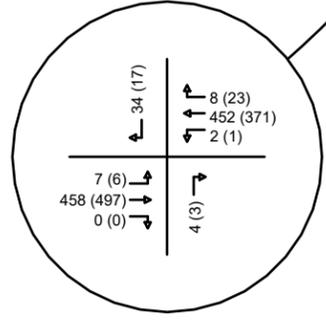
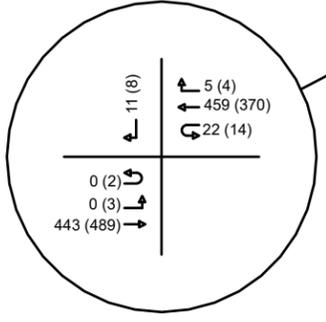
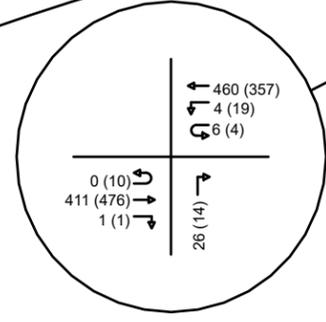
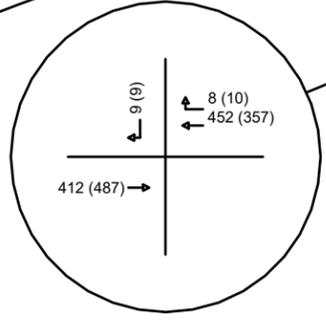
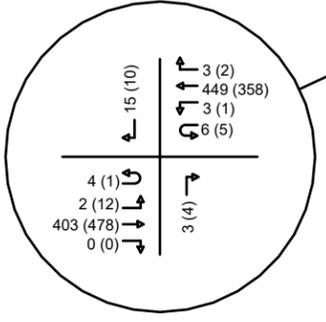
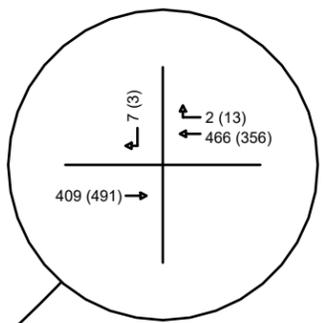
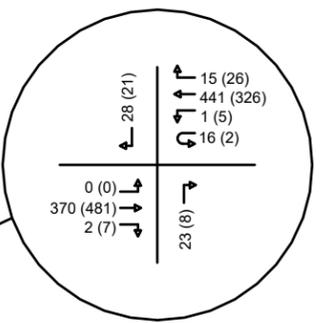
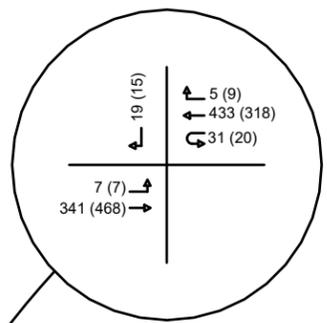
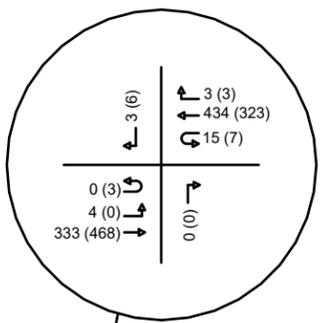
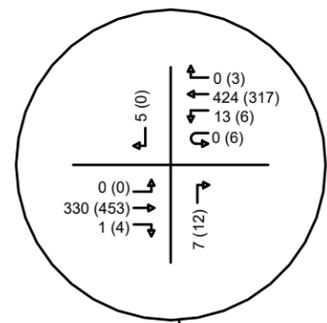
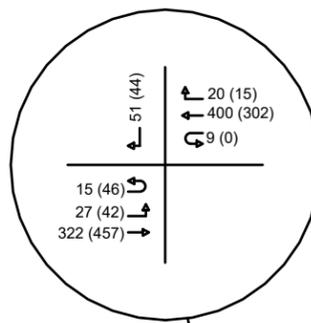
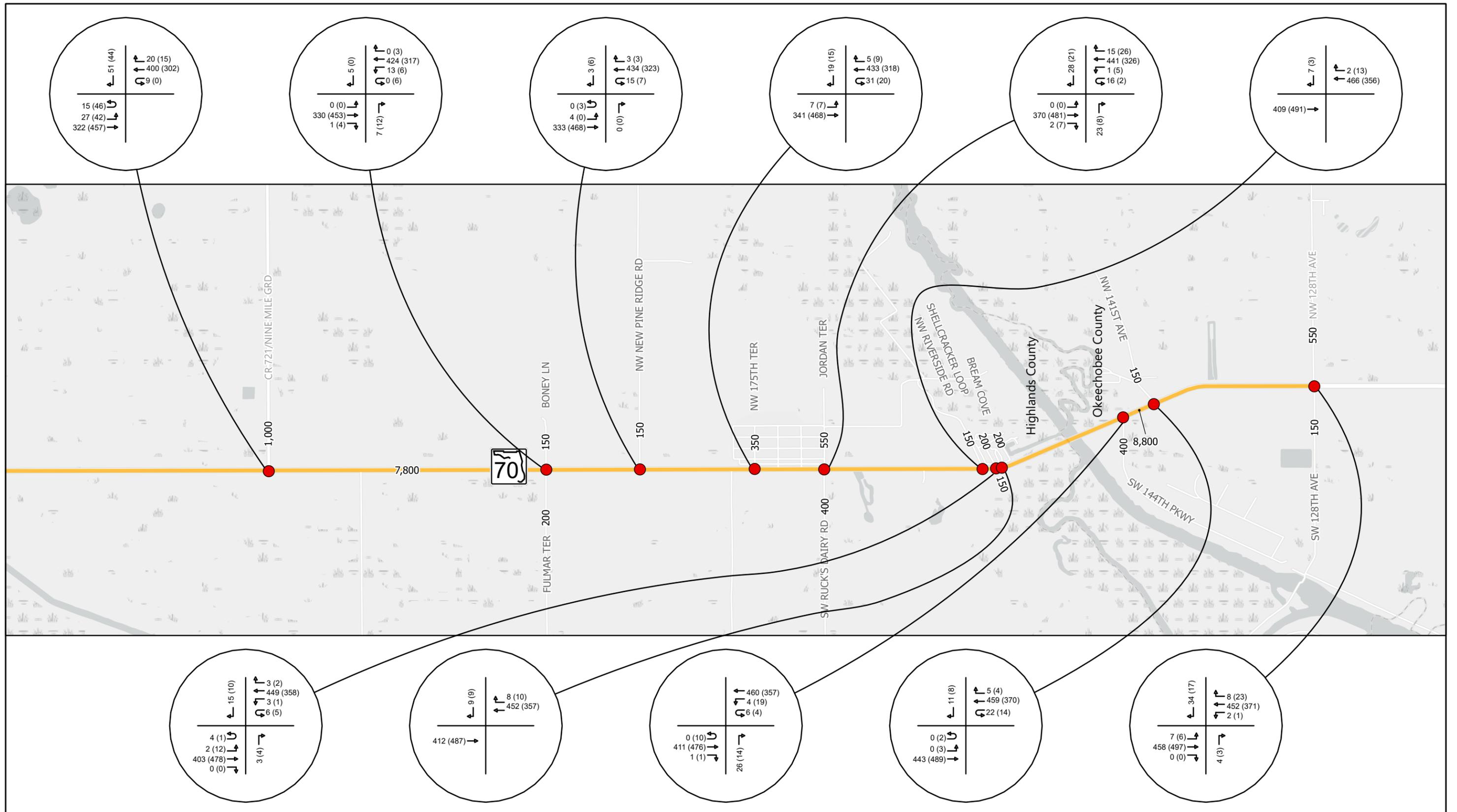


Figure 3-6: Opening Year (2032) Build AADT and AM (PM) Turning Movement Volumes
Sheet 4 of 5



Legend

- Project Limits
- Unsignalized (11)
- XX (XX) AM(PM) Peak Hour Volumes
- X,XXX AADT
- ↑↑↑ Turning Movements

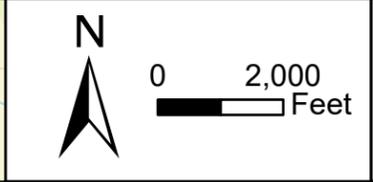
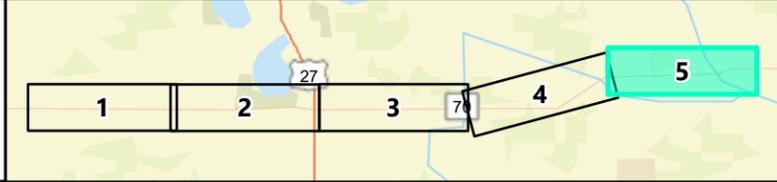


Figure 3-6: Opening Year (2032) Build AADT and AM (PM) Turning Movement Volumes
Sheet 5 of 5

APPENDIX C: Manual Turning Movement Counts

Intersection Turning Movement Count

City/County: Lake Placid/Highlands
 Weather: Clear
 Comments:

File Name : SR70&LonesomeIsland
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 1

Groups Printed- Passenger Vehicles - Heavy Vehicles - UTurns

| Start Time | LONESOME ISLAND ROAD Southbound | | | | SR 70 Westbound | | | | JC DURRANCE ROAD DRIVEWAYS Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|----------------------|---------------------------------|----------|----------|------------|-----------------|------------|----------|------------|---------------------------------------|----------|----------|------------|-----------------|------------|-----------|------------|-------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 1 | 31 | 0 | 32 | 2 | 0 | 0 | 2 | 0 | 44 | 1 | 45 | 79 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 35 | 0 | 35 | 0 | 0 | 0 | 0 | 1 | 48 | 1 | 50 | 85 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 37 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 40 | 2 | 42 | 79 |
| 07:45 AM | 0 | 0 | 0 | 0 | 1 | 37 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 35 | 1 | 36 | 74 |
| Total | 0 | 0 | 0 | 0 | 2 | 140 | 0 | 142 | 2 | 0 | 0 | 2 | 1 | 167 | 5 | 173 | 317 |
| 08:00 AM | 0 | 0 | 0 | 0 | 1 | 34 | 0 | 35 | 0 | 0 | 0 | 0 | 0 | 35 | 1 | 36 | 71 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 51 | 0 | 51 | 1 | 0 | 1 | 2 | 0 | 40 | 0 | 40 | 93 |
| 08:30 AM | 0 | 0 | 0 | 0 | 2 | 40 | 0 | 42 | 1 | 0 | 0 | 1 | 0 | 39 | 1 | 40 | 83 |
| 08:45 AM | 0 | 0 | 0 | 0 | 1 | 37 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 36 | 2 | 38 | 76 |
| Total | 0 | 0 | 0 | 0 | 4 | 162 | 0 | 166 | 2 | 0 | 1 | 3 | 0 | 150 | 4 | 154 | 323 |
| *** BREAK *** | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 48 | 0 | 48 | 0 | 0 | 1 | 1 | 0 | 41 | 0 | 41 | 90 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 45 | 0 | 45 | 1 | 1 | 0 | 2 | 0 | 57 | 0 | 57 | 104 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 55 | 0 | 55 | 1 | 0 | 1 | 2 | 0 | 61 | 0 | 61 | 118 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 59 | 0 | 59 | 1 | 0 | 0 | 1 | 0 | 53 | 0 | 53 | 113 |
| Total | 0 | 0 | 0 | 0 | 0 | 207 | 0 | 207 | 3 | 1 | 2 | 6 | 0 | 212 | 0 | 212 | 425 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 47 | 0 | 47 | 4 | 0 | 0 | 4 | 0 | 40 | 2 | 42 | 93 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 54 | 0 | 54 | 1 | 0 | 2 | 3 | 0 | 43 | 1 | 44 | 101 |
| 05:30 PM | 0 | 1 | 0 | 1 | 0 | 61 | 0 | 61 | 0 | 0 | 1 | 1 | 0 | 47 | 0 | 47 | 110 |
| 05:45 PM | 0 | 0 | 1 | 1 | 0 | 53 | 0 | 53 | 1 | 0 | 0 | 1 | 0 | 46 | 0 | 46 | 101 |
| Total | 0 | 1 | 1 | 2 | 0 | 215 | 0 | 215 | 6 | 0 | 3 | 9 | 0 | 176 | 3 | 179 | 405 |
| Grand Total | 0 | 1 | 1 | 2 | 6 | 724 | 0 | 730 | 13 | 1 | 6 | 20 | 1 | 705 | 12 | 718 | 1470 |
| Apprch % | 0 | 50 | 50 | | 0.8 | 99.2 | 0 | | 65 | 5 | 30 | | 0.1 | 98.2 | 1.7 | | |
| Total % | 0 | 0.1 | 0.1 | 0.1 | 0.4 | 49.3 | 0 | 49.7 | 0.9 | 0.1 | 0.4 | 1.4 | 0.1 | 48 | 0.8 | 48.8 | |
| Passenger Vehicles % | 0 | 1 | 1 | 2 | 4 | 591 | 0 | 595 | 12 | 1 | 5 | 18 | 1 | 566 | 11 | 578 | 1193 |
| Passenger Vehicles | 0 | 100 | 100 | 100 | 66.7 | 81.6 | 0 | 81.5 | 92.3 | 100 | 83.3 | 90 | 100 | 80.3 | 91.7 | 80.5 | 81.2 |
| Heavy Vehicles | 0 | 0 | 0 | 0 | 2 | 133 | 0 | 135 | 1 | 0 | 1 | 2 | 0 | 139 | 1 | 140 | 277 |
| % Heavy Vehicles | 0 | 0 | 0 | 0 | 33.3 | 18.4 | 0 | 18.5 | 7.7 | 0 | 16.7 | 10 | 0 | 19.7 | 8.3 | 19.5 | 18.8 |
| UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| Start Time | LONESOME ISLAND ROAD Southbound | | | | SR 70 Westbound | | | | JC DURRANCE ROAD DRIVEWAYS Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--|---------------------------------|----------|----------|------------|-----------------|------------|----------|------------|---------------------------------------|----------|----------|------------|-----------------|------------|----------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 0 | 0 | 0 | 1 | 34 | 0 | 35 | 0 | 0 | 0 | 0 | 0 | 35 | 1 | 36 | 71 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 51 | 0 | 51 | 1 | 0 | 1 | 2 | 0 | 40 | 0 | 40 | 93 |
| 08:30 AM | 0 | 0 | 0 | 0 | 2 | 40 | 0 | 42 | 1 | 0 | 0 | 1 | 0 | 39 | 1 | 40 | 83 |
| 08:45 AM | 0 | 0 | 0 | 0 | 1 | 37 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 36 | 2 | 38 | 76 |
| Total Volume | 0 | 0 | 0 | 0 | 4 | 162 | 0 | 166 | 2 | 0 | 1 | 3 | 0 | 150 | 4 | 154 | 323 |
| % App. Total | 0 | 0 | 0 | | 2.4 | 97.6 | 0 | | 66.7 | 0 | 33.3 | | 0 | 97.4 | 2.6 | | |
| PHF | .000 | .000 | .000 | .000 | .500 | .794 | .000 | .814 | .500 | .000 | .250 | .375 | .000 | .938 | .500 | .963 | .868 |

Intersection Turning Movement Count

| | | | | | | | | | | | | | | | | | |
|--------------------|---|---|---|---|------|------|---|------|-----|---|-----|------|---|------|------|------|------|
| Passenger Vehicles | 0 | 0 | 0 | 0 | 2 | 133 | 0 | 135 | 2 | 0 | 0 | 2 | 0 | 110 | 3 | 113 | 250 |
| % | | | | | | | | | | | | | | | | | |
| Passenger Vehicles | 0 | 0 | 0 | 0 | 50.0 | 82.1 | 0 | 81.3 | 100 | 0 | 0 | 66.7 | 0 | 73.3 | 75.0 | 73.4 | 77.4 |
| Heavy Vehicles | 0 | 0 | 0 | 0 | 2 | 29 | 0 | 31 | 0 | 0 | 1 | 1 | 0 | 40 | 1 | 41 | 73 |
| % Heavy Vehicles | 0 | 0 | 0 | 0 | 50.0 | 17.9 | 0 | 18.7 | 0 | 0 | 100 | 33.3 | 0 | 26.7 | 25.0 | 26.6 | 22.6 |
| UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1
 Peak Hour for Each Approach Begins at:

| | | | | | | | | | | | | | | | | |
|--------------------|----------|------|------|------|----------|------|------|------|----------|------|------|------|----------|------|------|------|
| | 07:00 AM | | | | 07:45 AM | | | | 07:45 AM | | | | 07:00 AM | | | |
| +0 mins. | 0 | 0 | 0 | 0 | 1 | 37 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 44 | 1 | 45 |
| +15 mins. | 0 | 0 | 0 | 0 | 1 | 34 | 0 | 35 | 0 | 0 | 0 | 0 | 1 | 48 | 1 | 50 |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 51 | 0 | 51 | 1 | 0 | 1 | 2 | 0 | 40 | 2 | 42 |
| +45 mins. | 0 | 0 | 0 | 0 | 2 | 40 | 0 | 42 | 1 | 0 | 0 | 1 | 0 | 35 | 1 | 36 |
| Total Volume | 0 | 0 | 0 | 0 | 4 | 162 | 0 | 166 | 2 | 0 | 1 | 3 | 1 | 167 | 5 | 173 |
| % App. Total | 0 | 0 | 0 | 0 | 2.4 | 97.6 | 0 | | 66.7 | 0 | 33.3 | | 0.6 | 96.5 | 2.9 | |
| PHF | .000 | .000 | .000 | .000 | .500 | .794 | .000 | .814 | .500 | .000 | .250 | .375 | .250 | .870 | .625 | .865 |
| Passenger Vehicles | 0 | 0 | 0 | 0 | 2 | 130 | 0 | 132 | 2 | 0 | 0 | 2 | 1 | 139 | 5 | 145 |
| % | | | | | | | | | | | | | | | | |
| Passenger Vehicles | 0 | 0 | 0 | 0 | 50 | 80.2 | 0 | 79.5 | 100 | 0 | 0 | 66.7 | 100 | 83.2 | 100 | 83.8 |
| Heavy Vehicles | 0 | 0 | 0 | 0 | 2 | 32 | 0 | 34 | 0 | 0 | 1 | 1 | 0 | 28 | 0 | 28 |
| % Heavy Vehicles | 0 | 0 | 0 | 0 | 50 | 19.8 | 0 | 20.5 | 0 | 0 | 100 | 33.3 | 0 | 16.8 | 0 | 16.2 |
| UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1
 Peak Hour for Entire Intersection Begins at 04:15 PM

| | | | | | | | | | | | | | | | | | |
|--------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 45 | 0 | 45 | 1 | 1 | 0 | 2 | 0 | 57 | 0 | 57 | 104 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 55 | 0 | 55 | 1 | 0 | 1 | 2 | 0 | 61 | 0 | 61 | 118 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 59 | 0 | 59 | 1 | 0 | 0 | 1 | 0 | 53 | 0 | 53 | 113 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 47 | 0 | 47 | 4 | 0 | 0 | 4 | 0 | 40 | 2 | 42 | 93 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 206 | 0 | 206 | 7 | 1 | 1 | 9 | 0 | 211 | 2 | 213 | 428 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 100 | 0 | | 77.8 | 11.1 | 11.1 | | 0 | 99.1 | 0.9 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .873 | .000 | .873 | .438 | .250 | .250 | .563 | .000 | .865 | .250 | .873 | .907 |
| Passenger Vehicles | 0 | 0 | 0 | 0 | 0 | 178 | 0 | 178 | 7 | 1 | 1 | 9 | 0 | 173 | 2 | 175 | 362 |
| % | | | | | | | | | | | | | | | | | |
| Passenger Vehicles | 0 | 0 | 0 | 0 | 0 | 86.4 | 0 | 86.4 | 100 | 100 | 100 | 100 | 0 | 82.0 | 100 | 82.2 | 84.6 |
| Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 28 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 38 | 0 | 38 | 66 |
| % Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 13.6 | 0 | 13.6 | 0 | 0 | 0 | 0 | 0 | 18.0 | 0 | 17.8 | 15.4 |
| UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1
 Peak Hour for Each Approach Begins at:

| | | | | | | | | | | | | | | | | |
|--------------------|----------|------|------|------|----------|------|------|------|----------|------|------|------|----------|------|------|------|
| | 05:00 PM | | | | 04:45 PM | | | | 04:30 PM | | | | 04:15 PM | | | |
| +0 mins. | 0 | 0 | 0 | 0 | 0 | 59 | 0 | 59 | 1 | 0 | 1 | 2 | 0 | 57 | 0 | 57 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 47 | 0 | 47 | 1 | 0 | 0 | 1 | 0 | 61 | 0 | 61 |
| +30 mins. | 0 | 1 | 0 | 1 | 0 | 54 | 0 | 54 | 4 | 0 | 0 | 4 | 0 | 53 | 0 | 53 |
| +45 mins. | 0 | 0 | 1 | 1 | 0 | 61 | 0 | 61 | 1 | 0 | 2 | 3 | 0 | 40 | 2 | 42 |
| Total Volume | 0 | 1 | 1 | 2 | 0 | 221 | 0 | 221 | 7 | 0 | 3 | 10 | 0 | 211 | 2 | 213 |
| % App. Total | 0 | 50 | 50 | | 0 | 100 | 0 | | 70 | 0 | 30 | | 0 | 99.1 | 0.9 | |
| PHF | .000 | .250 | .250 | .500 | .000 | .906 | .000 | .906 | .438 | .000 | .375 | .625 | .000 | .865 | .250 | .873 |
| Passenger Vehicles | 0 | 1 | 1 | 2 | 0 | 194 | 0 | 194 | 7 | 0 | 3 | 10 | 0 | 173 | 2 | 175 |

Intersection Turning Movement Count

| | | | | | | | | | | | | | | | | |
|----------------------|---|-----|-----|-----|---|------|---|------|-----|---|-----|-----|---|----|-----|------|
| % Passenger Vehicles | 0 | 100 | 100 | 100 | 0 | 87.8 | 0 | 87.8 | 100 | 0 | 100 | 100 | 0 | 82 | 100 | 82.2 |
| Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 27 | 0 | 27 | 0 | 0 | 0 | 0 | 0 | 38 | 0 | 38 |
| % Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 12.2 | 0 | 12.2 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 17.8 |
| UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Intersection Turning Movement Count

City/County: Lake Placid/Highlands
 Weather: Clear
 Comments:

File Name : SR70&LonesomeIsland
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 1

Groups Printed- Passenger Vehicles

| Start Time | LONESOME ISLAND ROAD Southbound | | | | SR 70 Westbound | | | | JC DURRANCE ROAD DRIVEWAYS Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--------------------|---------------------------------|------|-------|------------|-----------------|------|-------|------------|---------------------------------------|------|-------|------------|-----------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 1 | 24 | 0 | 25 | 1 | 0 | 0 | 1 | 0 | 39 | 1 | 40 | 66 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 20 | 0 | 0 | 0 | 0 | 1 | 41 | 1 | 43 | 63 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 36 | 2 | 38 | 63 |
| 07:45 AM | 0 | 0 | 0 | 0 | 1 | 29 | 0 | 30 | 0 | 0 | 0 | 0 | 0 | 23 | 1 | 24 | 54 |
| Total | 0 | 0 | 0 | 0 | 2 | 98 | 0 | 100 | 1 | 0 | 0 | 1 | 1 | 139 | 5 | 145 | 246 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 27 | 0 | 27 | 53 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 43 | 0 | 43 | 1 | 0 | 0 | 1 | 0 | 35 | 0 | 35 | 79 |
| 08:30 AM | 0 | 0 | 0 | 0 | 1 | 32 | 0 | 33 | 1 | 0 | 0 | 1 | 0 | 19 | 1 | 20 | 54 |
| 08:45 AM | 0 | 0 | 0 | 0 | 1 | 32 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 29 | 2 | 31 | 64 |
| Total | 0 | 0 | 0 | 0 | 2 | 133 | 0 | 135 | 2 | 0 | 0 | 2 | 0 | 110 | 3 | 113 | 250 |
| *** BREAK *** | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 37 | 0 | 37 | 0 | 0 | 1 | 1 | 0 | 28 | 0 | 28 | 66 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 38 | 0 | 38 | 1 | 1 | 0 | 2 | 0 | 43 | 0 | 43 | 83 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 45 | 0 | 45 | 1 | 0 | 1 | 2 | 0 | 50 | 0 | 50 | 97 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 53 | 0 | 53 | 1 | 0 | 0 | 1 | 0 | 45 | 0 | 45 | 99 |
| Total | 0 | 0 | 0 | 0 | 0 | 173 | 0 | 173 | 3 | 1 | 2 | 6 | 0 | 166 | 0 | 166 | 345 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 42 | 0 | 42 | 4 | 0 | 0 | 4 | 0 | 35 | 2 | 37 | 83 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 50 | 1 | 0 | 2 | 3 | 0 | 37 | 1 | 38 | 91 |
| 05:30 PM | 0 | 1 | 0 | 1 | 0 | 49 | 0 | 49 | 0 | 0 | 1 | 1 | 0 | 39 | 0 | 39 | 90 |
| 05:45 PM | 0 | 0 | 1 | 1 | 0 | 46 | 0 | 46 | 1 | 0 | 0 | 1 | 0 | 40 | 0 | 40 | 88 |
| Total | 0 | 1 | 1 | 2 | 0 | 187 | 0 | 187 | 6 | 0 | 3 | 9 | 0 | 151 | 3 | 154 | 352 |
| Grand Total | 0 | 1 | 1 | 2 | 4 | 591 | 0 | 595 | 12 | 1 | 5 | 18 | 1 | 566 | 11 | 578 | 1193 |
| Apprch % | 0 | 50 | 50 | | 0.7 | 99.3 | 0 | | 66.7 | 5.6 | 27.8 | | 0.2 | 97.9 | 1.9 | | |
| Total % | 0 | 0.1 | 0.1 | 0.2 | 0.3 | 49.5 | 0 | 49.9 | 1 | 0.1 | 0.4 | 1.5 | 0.1 | 47.4 | 0.9 | 48.4 | |

| Start Time | LONESOME ISLAND ROAD Southbound | | | | SR 70 Westbound | | | | JC DURRANCE ROAD DRIVEWAYS Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--|---------------------------------|------|-------|------------|-----------------|------|-------|------------|---------------------------------------|------|-------|------------|-----------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 27 | 0 | 27 | 53 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 43 | 0 | 43 | 1 | 0 | 0 | 1 | 0 | 35 | 0 | 35 | 79 |
| 08:30 AM | 0 | 0 | 0 | 0 | 1 | 32 | 0 | 33 | 1 | 0 | 0 | 1 | 0 | 19 | 1 | 20 | 54 |
| 08:45 AM | 0 | 0 | 0 | 0 | 1 | 32 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 29 | 2 | 31 | 64 |
| Total Volume | 0 | 0 | 0 | 0 | 2 | 133 | 0 | 135 | 2 | 0 | 0 | 2 | 0 | 110 | 3 | 113 | 250 |
| % App. Total | 0 | 0 | 0 | | 1.5 | 98.5 | 0 | | 100 | 0 | 0 | | 0 | 97.3 | 2.7 | | |
| PHF | .000 | .000 | .000 | .000 | .500 | .773 | .000 | .785 | .500 | .000 | .000 | .500 | .000 | .786 | .375 | .807 | .791 |

Intersection Turning Movement Count

File Name : SR70&LonesomeIsland
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 2

| Start Time | LONESOME ISLAND ROAD Southbound | | | | SR 70 Westbound | | | | JC DURRANCE ROAD DRIVEWAYS Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|------------|------------------------------------|------|-------|------------|--------------------|------|-------|------------|---|------|-------|------------|--------------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 07:00 AM | | | | 08:00 AM | | | | 07:45 AM | | | | 07:00 AM | | | |
|--------------|----------|------|------|------|----------|-----------|------|-----------|----------|------|------|----------|----------|-----------|----------|-----------|
| +0 mins. | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 39 | 1 | 40 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 43 | 0 | 43 | 0 | 0 | 0 | 0 | 1 | 41 | 1 | 43 |
| +30 mins. | 0 | 0 | 0 | 0 | 1 | 32 | 0 | 33 | 1 | 0 | 0 | 1 | 0 | 36 | 2 | 38 |
| +45 mins. | 0 | 0 | 0 | 0 | 1 | 32 | 0 | 33 | 1 | 0 | 0 | 1 | 0 | 23 | 1 | 24 |
| Total Volume | 0 | 0 | 0 | 0 | 2 | 133 | 0 | 135 | 2 | 0 | 0 | 2 | 1 | 139 | 5 | 145 |
| % App. Total | 0 | 0 | 0 | | 1.5 | 98.5 | 0 | | 100 | 0 | 0 | | 0.7 | 95.9 | 3.4 | |
| PHF | .000 | .000 | .000 | .000 | .500 | .773 | .000 | .785 | .500 | .000 | .000 | .500 | .250 | .848 | .625 | .843 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 04:30 PM

| | | | | | | | | | | | | | | | | | |
|--------------|------|------|------|------|------|-----------|------|-----------|----------|------|----------|----------|------|-----------|----------|-----------|-----------|
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 45 | 0 | 45 | 1 | 0 | 1 | 2 | 0 | 50 | 0 | 50 | 97 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 53 | 0 | 53 | 1 | 0 | 0 | 1 | 0 | 45 | 0 | 45 | 99 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 42 | 0 | 42 | 4 | 0 | 0 | 4 | 0 | 35 | 2 | 37 | 83 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 50 | 1 | 0 | 2 | 3 | 0 | 37 | 1 | 38 | 91 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 190 | 0 | 190 | 7 | 0 | 3 | 10 | 0 | 167 | 3 | 170 | 370 |
| % App. Total | 0 | 0 | 0 | | 0 | 100 | 0 | | 70 | 0 | 30 | | 0 | 98.2 | 1.8 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .896 | .000 | .896 | .438 | .000 | .375 | .625 | .000 | .835 | .375 | .850 | .934 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 05:00 PM | | | | 04:45 PM | | | | 04:30 PM | | | | 04:15 PM | | | |
|--------------|----------|----------|----------|----------|----------|-----------|------|-----------|----------|------|----------|----------|----------|-----------|----------|-----------|
| +0 mins. | 0 | 0 | 0 | 0 | 0 | 53 | 0 | 53 | 1 | 0 | 1 | 2 | 0 | 43 | 0 | 43 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 42 | 0 | 42 | 1 | 0 | 0 | 1 | 0 | 50 | 0 | 50 |
| +30 mins. | 0 | 1 | 0 | 1 | 0 | 50 | 0 | 50 | 4 | 0 | 0 | 4 | 0 | 45 | 0 | 45 |
| +45 mins. | 0 | 0 | 1 | 1 | 0 | 49 | 0 | 49 | 1 | 0 | 2 | 3 | 0 | 35 | 2 | 37 |
| Total Volume | 0 | 1 | 1 | 2 | 0 | 194 | 0 | 194 | 7 | 0 | 3 | 10 | 0 | 173 | 2 | 175 |
| % App. Total | 0 | 50 | 50 | | 0 | 100 | 0 | | 70 | 0 | 30 | | 0 | 98.9 | 1.1 | |
| PHF | .000 | .250 | .250 | .500 | .000 | .915 | .000 | .915 | .438 | .000 | .375 | .625 | .000 | .865 | .250 | .875 |

Intersection Turning Movement Count

City/County: Lake Placid/Highlands
 Weather: Clear
 Comments:

File Name : SR70&LonesomeIsland
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 1

Groups Printed- Heavy Vehicles

| Start Time | LONESOME ISLAND ROAD Southbound | | | | SR 70 Westbound | | | | JC DURRANCE ROAD DRIVEWAYS Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--------------------|---------------------------------|------|-------|------------|-----------------|------|-------|------------|---------------------------------------|------|-------|------------|-----------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 1 | 0 | 0 | 1 | 0 | 5 | 0 | 5 | 13 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 22 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 16 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 12 | 20 |
| Total | 0 | 0 | 0 | 0 | 0 | 42 | 0 | 42 | 1 | 0 | 0 | 1 | 0 | 28 | 0 | 28 | 71 |
| 08:00 AM | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 1 | 9 | 18 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 1 | 1 | 0 | 5 | 0 | 5 | 14 |
| 08:30 AM | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 20 | 29 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 12 |
| Total | 0 | 0 | 0 | 0 | 2 | 29 | 0 | 31 | 0 | 0 | 1 | 1 | 0 | 40 | 1 | 41 | 73 |
| *** BREAK *** | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 13 | 24 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 14 | 21 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 11 | 21 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 14 |
| Total | 0 | 0 | 0 | 0 | 0 | 34 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 46 | 0 | 46 | 80 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 10 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 10 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 20 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 13 |
| Total | 0 | 0 | 0 | 0 | 0 | 28 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 25 | 53 |
| Grand Total | 0 | 0 | 0 | 0 | 2 | 133 | 0 | 135 | 1 | 0 | 1 | 2 | 0 | 139 | 1 | 140 | 277 |
| Apprch % | 0 | 0 | 0 | | 1.5 | 98.5 | 0 | | 50 | 0 | 50 | | 0 | 99.3 | 0.7 | | |
| Total % | 0 | 0 | 0 | | 0.7 | 48 | 0 | 48.7 | 0.4 | 0 | 0.4 | 0.7 | 0 | 50.2 | 0.4 | 50.5 | |

| Start Time | LONESOME ISLAND ROAD Southbound | | | | SR 70 Westbound | | | | JC DURRANCE ROAD DRIVEWAYS Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--|---------------------------------|------|-------|------------|-----------------|----------|-------|------------|---------------------------------------|------|-------|------------|-----------------|-----------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:45 AM | | | | | | | | | | | | | | | | | |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 12 | 20 |
| 08:00 AM | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 1 | 9 | 18 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 1 | 1 | 0 | 5 | 0 | 5 | 14 |
| 08:30 AM | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 20 | 29 |
| Total Volume | 0 | 0 | 0 | 0 | 2 | 32 | 0 | 34 | 0 | 0 | 1 | 1 | 0 | 45 | 1 | 46 | 81 |
| % App. Total | 0 | 0 | 0 | | 5.9 | 94.1 | 0 | | 0 | 0 | 100 | | 0 | 97.8 | 2.2 | | |
| PHF | .000 | .000 | .000 | .000 | .500 | 1.00 | .000 | .944 | .000 | .000 | .250 | .250 | .000 | .563 | .250 | .575 | .698 |

Intersection Turning Movement Count

File Name : SR70&LonesomeIsland
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 2

| | LONESOME ISLAND ROAD Southbound | | | | SR 70 Westbound | | | | JC DURRANCE ROAD DRIVEWAYS Northbound | | | | SR 70 Eastbound | | | | |
|------------|------------------------------------|------|-------|------------|--------------------|------|-------|------------|---|------|-------|------------|--------------------|------|-------|------------|------------|
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 07:00 AM | | | | 07:15 AM | | | | 07:00 AM | | | | 07:45 AM | | | |
|--------------|----------|------|------|------|----------|-----------|------|-----------|----------|------|------|----------|----------|-----------|----------|-----------|
| +0 mins. | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 15 | 1 | 0 | 0 | 1 | 0 | 12 | 0 | 12 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 8 | 1 | 9 |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 |
| +45 mins. | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 20 |
| Total Volume | 0 | 0 | 0 | 0 | 1 | 43 | 0 | 44 | 1 | 0 | 0 | 1 | 0 | 45 | 1 | 46 |
| % App. Total | 0 | 0 | 0 | | 2.3 | 97.7 | 0 | | 100 | 0 | 0 | | 0 | 97.8 | 2.2 | |
| PHF | .000 | .000 | .000 | .000 | .250 | .717 | .000 | .733 | .250 | .000 | .000 | .250 | .000 | .563 | .250 | .575 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 04:00 PM

| | | | | | | | | | | | | | | | | | |
|--------------|------|------|------|------|------|-----------|------|-----------|------|------|------|------|------|-----------|------|-----------|-----------|
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 13 | 24 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 14 | 21 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 11 | 21 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 14 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 34 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 46 | 0 | 46 | 80 |
| % App. Total | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .773 | .000 | .773 | .000 | .000 | .000 | .000 | .000 | .821 | .000 | .821 | .833 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 04:00 PM | | | | 04:00 PM | | | | 04:00 PM | | | | 04:00 PM | | | |
|--------------|----------|------|------|------|----------|-----------|------|-----------|----------|------|------|------|----------|-----------|------|-----------|
| +0 mins. | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 13 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 14 |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 11 |
| +45 mins. | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 34 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 46 | 0 | 46 |
| % App. Total | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | |
| PHF | .000 | .000 | .000 | .000 | .000 | .773 | .000 | .773 | .000 | .000 | .000 | .000 | .000 | .821 | .000 | .821 |

Intersection Turning Movement Count

City/County: Brighton/Highlands
 Weather: Clear
 Comments:

File Name : SR70&CR721S
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 1

Groups Printed- Passenger Vehicles - Heavy Vehicles - UTurns

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|---------------------------------|---------------------|----------|----------|------------|-----------------|------------|----------|------------|-------------------------|----------|------------|------------|-----------------|------------|-----------|------------|-------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 20 | 27 | 0 | 47 | 2 | 0 | 5 | 7 | 0 | 25 | 11 | 36 | 90 |
| 07:15 AM | 0 | 0 | 0 | 0 | 25 | 43 | 0 | 68 | 2 | 0 | 9 | 11 | 0 | 35 | 8 | 43 | 122 |
| 07:30 AM | 0 | 1 | 0 | 1 | 33 | 28 | 1 | 62 | 1 | 0 | 5 | 6 | 0 | 32 | 9 | 41 | 110 |
| 07:45 AM | 0 | 0 | 0 | 0 | 31 | 35 | 0 | 66 | 5 | 0 | 11 | 16 | 0 | 31 | 7 | 38 | 120 |
| Total | 0 | 1 | 0 | 1 | 109 | 133 | 1 | 243 | 10 | 0 | 30 | 40 | 0 | 123 | 35 | 158 | 442 |
| 08:00 AM | 0 | 0 | 0 | 0 | 12 | 42 | 1 | 55 | 4 | 0 | 10 | 14 | 0 | 35 | 6 | 41 | 110 |
| 08:15 AM | 0 | 1 | 0 | 1 | 13 | 34 | 0 | 47 | 7 | 0 | 9 | 16 | 0 | 34 | 6 | 40 | 104 |
| 08:30 AM | 0 | 0 | 0 | 0 | 13 | 42 | 1 | 56 | 5 | 0 | 11 | 16 | 0 | 27 | 6 | 33 | 105 |
| 08:45 AM | 0 | 1 | 0 | 1 | 9 | 38 | 0 | 47 | 2 | 0 | 5 | 7 | 0 | 37 | 5 | 42 | 97 |
| Total | 0 | 2 | 0 | 2 | 47 | 156 | 2 | 205 | 18 | 0 | 35 | 53 | 0 | 133 | 23 | 156 | 416 |
| *** BREAK *** | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 0 | 0 | 0 | 9 | 35 | 0 | 44 | 8 | 2 | 20 | 30 | 0 | 35 | 2 | 37 | 111 |
| 04:15 PM | 0 | 1 | 0 | 1 | 15 | 48 | 0 | 63 | 12 | 1 | 28 | 41 | 1 | 34 | 5 | 40 | 145 |
| 04:30 PM | 0 | 3 | 0 | 3 | 11 | 32 | 0 | 43 | 11 | 0 | 20 | 31 | 0 | 62 | 4 | 66 | 143 |
| 04:45 PM | 1 | 0 | 0 | 1 | 16 | 43 | 0 | 59 | 13 | 0 | 25 | 38 | 0 | 61 | 6 | 67 | 165 |
| Total | 1 | 4 | 0 | 5 | 51 | 158 | 0 | 209 | 44 | 3 | 93 | 140 | 1 | 192 | 17 | 210 | 564 |
| 05:00 PM | 0 | 0 | 0 | 0 | 6 | 39 | 0 | 45 | 8 | 0 | 53 | 61 | 0 | 42 | 7 | 49 | 155 |
| 05:15 PM | 0 | 0 | 0 | 0 | 5 | 41 | 0 | 46 | 17 | 0 | 37 | 54 | 0 | 29 | 3 | 32 | 132 |
| 05:30 PM | 0 | 0 | 0 | 0 | 12 | 57 | 0 | 69 | 8 | 0 | 18 | 26 | 0 | 43 | 5 | 48 | 143 |
| 05:45 PM | 0 | 0 | 0 | 0 | 10 | 29 | 0 | 39 | 7 | 0 | 19 | 26 | 1 | 47 | 3 | 51 | 116 |
| Total | 0 | 0 | 0 | 0 | 33 | 166 | 0 | 199 | 40 | 0 | 127 | 167 | 1 | 161 | 18 | 180 | 546 |
| Grand Total | 1 | 7 | 0 | 8 | 240 | 613 | 3 | 856 | 112 | 3 | 285 | 400 | 2 | 609 | 93 | 704 | 1968 |
| Apprch % | 12.5 | 87.5 | 0 | | 28 | 71.6 | 0.4 | | 28 | 0.8 | 71.2 | | 0.3 | 86.5 | 13.2 | | |
| Total % | 0.1 | 0.4 | 0 | 0.4 | 12.2 | 31.1 | 0.2 | 43.5 | 5.7 | 0.2 | 14.5 | 20.3 | 0.1 | 30.9 | 4.7 | 35.8 | |
| Passenger Vehicles % | 1 | 6 | 0 | 7 | 230 | 473 | 2 | 705 | 110 | 3 | 276 | 389 | 1 | 468 | 91 | 560 | 1661 |
| Passenger Vehicles % | 100 | 85.7 | 0 | 87.5 | 95.8 | 77.2 | 66.7 | 82.4 | 98.2 | 100 | 96.8 | 97.2 | 50 | 76.8 | 97.8 | 79.5 | 84.4 |
| Heavy Vehicles % Heavy Vehicles | 0 | 1 | 0 | 1 | 10 | 140 | 1 | 151 | 2 | 0 | 9 | 11 | 0 | 141 | 2 | 143 | 306 |
| UTurns % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| UTurns % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 0 | 0.1 | 0.1 |

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--|---------------------|----------|----------|------------|-----------------|------------|----------|------------|-------------------------|----------|-----------|------------|-----------------|------------|-----------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:15 AM | | | | | | | | | | | | | | | | | |
| 07:15 AM | 0 | 0 | 0 | 0 | 25 | 43 | 0 | 68 | 2 | 0 | 9 | 11 | 0 | 35 | 8 | 43 | 122 |
| 07:30 AM | 0 | 1 | 0 | 1 | 33 | 28 | 1 | 62 | 1 | 0 | 5 | 6 | 0 | 32 | 9 | 41 | 110 |
| 07:45 AM | 0 | 0 | 0 | 0 | 31 | 35 | 0 | 66 | 5 | 0 | 11 | 16 | 0 | 31 | 7 | 38 | 120 |
| 08:00 AM | 0 | 0 | 0 | 0 | 12 | 42 | 1 | 55 | 4 | 0 | 10 | 14 | 0 | 35 | 6 | 41 | 110 |
| Total Volume | 0 | 1 | 0 | 1 | 101 | 148 | 2 | 251 | 12 | 0 | 35 | 47 | 0 | 133 | 30 | 163 | 462 |
| % App. Total | 0 | 100 | 0 | | 40.2 | 59 | 0.8 | | 25.5 | 0 | 74.5 | | 0 | 81.6 | 18.4 | | |
| PHF | .000 | .250 | .000 | .250 | .765 | .860 | .500 | .923 | .600 | .000 | .795 | .734 | .000 | .950 | .833 | .948 | .947 |
| Passenger Vehicles | 0 | 1 | 0 | 1 | 96 | 106 | 2 | 204 | 12 | 0 | 35 | 47 | 0 | 102 | 30 | 132 | 384 |

Intersection Turning Movement Count

| | | | | | | | | | | | | | | | | | |
|----------------------|---|-----|---|-----|------|------|-----|------|-----|---|-----|-----|---|------|-----|------|------|
| % Passenger Vehicles | 0 | 100 | 0 | 100 | 95.0 | 71.6 | 100 | 81.3 | 100 | 0 | 100 | 100 | 0 | 76.7 | 100 | 81.0 | 83.1 |
| Heavy Vehicles | 0 | 0 | 0 | 0 | 5 | 42 | 0 | 47 | 0 | 0 | 0 | 0 | 0 | 31 | 0 | 31 | 78 |
| % Heavy Vehicles | 0 | 0 | 0 | 0 | 5.0 | 28.4 | 0 | 18.7 | 0 | 0 | 0 | 0 | 0 | 23.3 | 0 | 19.0 | 16.9 |
| UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 07:30 AM | | | | 07:15 AM | | | | 07:45 AM | | | | 07:15 AM | | | | |
|----------------------|----------|------|------|------|----------|------|------|------|----------|------|------|------|----------|------|------|------|--|
| +0 mins. | 0 | 1 | 0 | 1 | 25 | 43 | 0 | 68 | 5 | 0 | 11 | 16 | 0 | 35 | 8 | 43 | |
| +15 mins. | 0 | 0 | 0 | 0 | 33 | 28 | 1 | 62 | 4 | 0 | 10 | 14 | 0 | 32 | 9 | 41 | |
| +30 mins. | 0 | 0 | 0 | 0 | 31 | 35 | 0 | 66 | 7 | 0 | 9 | 16 | 0 | 31 | 7 | 38 | |
| +45 mins. | 0 | 1 | 0 | 1 | 12 | 42 | 1 | 55 | 5 | 0 | 11 | 16 | 0 | 35 | 6 | 41 | |
| Total Volume | 0 | 2 | 0 | 2 | 101 | 148 | 2 | 251 | 21 | 0 | 41 | 62 | 0 | 133 | 30 | 163 | |
| % App. Total | 0 | 100 | 0 | | 40.2 | 59 | 0.8 | | 33.9 | 0 | 66.1 | | 0 | 81.6 | 18.4 | | |
| PHF | .000 | .500 | .000 | .500 | .765 | .860 | .500 | .923 | .750 | .000 | .932 | .969 | .000 | .950 | .833 | .948 | |
| Passenger Vehicles | 0 | 2 | 0 | 2 | 96 | 106 | 2 | 204 | 19 | 0 | 38 | 57 | 0 | 102 | 30 | 132 | |
| % Passenger Vehicles | 0 | 100 | 0 | 100 | 95 | 71.6 | 100 | 81.3 | 90.5 | 0 | 92.7 | 91.9 | 0 | 76.7 | 100 | 81 | |
| Heavy Vehicles | 0 | 0 | 0 | 0 | 5 | 42 | 0 | 47 | 2 | 0 | 3 | 5 | 0 | 31 | 0 | 31 | |
| % Heavy Vehicles | 0 | 0 | 0 | 0 | 5 | 28.4 | 0 | 18.7 | 9.5 | 0 | 7.3 | 8.1 | 0 | 23.3 | 0 | 19 | |
| UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 04:15 PM

| | | | | | | | | | | | | | | | | | |
|----------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 04:15 PM | 0 | 1 | 0 | 1 | 15 | 48 | 0 | 63 | 12 | 1 | 28 | 41 | 1 | 34 | 5 | 40 | 145 |
| 04:30 PM | 0 | 3 | 0 | 3 | 11 | 32 | 0 | 43 | 11 | 0 | 20 | 31 | 0 | 62 | 4 | 66 | 143 |
| 04:45 PM | 1 | 0 | 0 | 1 | 16 | 43 | 0 | 59 | 13 | 0 | 25 | 38 | 0 | 61 | 6 | 67 | 165 |
| 05:00 PM | 0 | 0 | 0 | 0 | 6 | 39 | 0 | 45 | 8 | 0 | 53 | 61 | 0 | 42 | 7 | 49 | 155 |
| Total Volume | 1 | 4 | 0 | 5 | 48 | 162 | 0 | 210 | 44 | 1 | 126 | 171 | 1 | 199 | 22 | 222 | 608 |
| % App. Total | 20 | 80 | 0 | | 22.9 | 77.1 | 0 | | 25.7 | 0.6 | 73.7 | | 0.5 | 89.6 | 9.9 | | |
| PHF | .250 | .333 | .000 | .417 | .750 | .844 | .000 | .833 | .846 | .250 | .594 | .701 | .250 | .802 | .786 | .828 | .921 |
| Passenger Vehicles | 1 | 4 | 0 | 5 | 47 | 132 | 0 | 179 | 44 | 1 | 123 | 168 | 1 | 156 | 21 | 178 | 530 |
| % Passenger Vehicles | 100 | 100 | 0 | 100 | 97.9 | 81.5 | 0 | 85.2 | 100 | 100 | 97.6 | 98.2 | 100 | 78.4 | 95.5 | 80.2 | 87.2 |
| Heavy Vehicles | 0 | 0 | 0 | 0 | 1 | 30 | 0 | 31 | 0 | 0 | 3 | 3 | 0 | 43 | 1 | 44 | 78 |
| % Heavy Vehicles | 0 | 0 | 0 | 0 | 2.1 | 18.5 | 0 | 14.8 | 0 | 0 | 2.4 | 1.8 | 0 | 21.6 | 4.5 | 19.8 | 12.8 |
| UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 04:00 PM | | | | 04:45 PM | | | | 04:30 PM | | | | 04:15 PM | | | | |
|----------------------|----------|------|------|------|----------|------|------|------|----------|------|------|------|----------|------|------|------|--|
| +0 mins. | 0 | 0 | 0 | 0 | 16 | 43 | 0 | 59 | 11 | 0 | 20 | 31 | 1 | 34 | 5 | 40 | |
| +15 mins. | 0 | 1 | 0 | 1 | 6 | 39 | 0 | 45 | 13 | 0 | 25 | 38 | 0 | 62 | 4 | 66 | |
| +30 mins. | 0 | 3 | 0 | 3 | 5 | 41 | 0 | 46 | 8 | 0 | 53 | 61 | 0 | 61 | 6 | 67 | |
| +45 mins. | 1 | 0 | 0 | 1 | 12 | 57 | 0 | 69 | 17 | 0 | 37 | 54 | 0 | 42 | 7 | 49 | |
| Total Volume | 1 | 4 | 0 | 5 | 39 | 180 | 0 | 219 | 49 | 0 | 135 | 184 | 1 | 199 | 22 | 222 | |
| % App. Total | 20 | 80 | 0 | | 17.8 | 82.2 | 0 | | 26.6 | 0 | 73.4 | | 0.5 | 89.6 | 9.9 | | |
| PHF | .250 | .333 | .000 | .417 | .609 | .789 | .000 | .793 | .721 | .000 | .637 | .754 | .250 | .802 | .786 | .828 | |
| Passenger Vehicles | 1 | 4 | 0 | 5 | 39 | 149 | 0 | 188 | 49 | 0 | 132 | 181 | 1 | 156 | 21 | 178 | |
| % Passenger Vehicles | 100 | 100 | 0 | 100 | 100 | 82.8 | 0 | 85.8 | 100 | 0 | 97.8 | 98.4 | 100 | 78.4 | 95.5 | 80.2 | |

Intersection Turning Movement Count

| | | | | | | | | | | | | | | | | |
|------------------|---|---|---|---|---|------|---|------|---|---|-----|-----|---|------|-----|------|
| Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 31 | 0 | 31 | 0 | 0 | 3 | 3 | 0 | 43 | 1 | 44 |
| % Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 17.2 | 0 | 14.2 | 0 | 0 | 2.2 | 1.6 | 0 | 21.6 | 4.5 | 19.8 |
| UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % UTurns | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Intersection Turning Movement Count

City/County: Brighton/Highlands
 Weather: Clear
 Comments:

File Name : SR70&CR721S
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 1

Groups Printed- Passenger Vehicles

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--------------------|---------------------|------|-------|------------|-----------------|------|-------|------------|-------------------------|------|-------|------------|-----------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 20 | 18 | 0 | 38 | 2 | 0 | 5 | 7 | 0 | 19 | 11 | 30 | 75 |
| 07:15 AM | 0 | 0 | 0 | 0 | 24 | 23 | 0 | 47 | 2 | 0 | 9 | 11 | 0 | 30 | 8 | 38 | 96 |
| 07:30 AM | 0 | 1 | 0 | 1 | 33 | 22 | 1 | 56 | 1 | 0 | 5 | 6 | 0 | 25 | 9 | 34 | 97 |
| 07:45 AM | 0 | 0 | 0 | 0 | 30 | 26 | 0 | 56 | 5 | 0 | 11 | 16 | 0 | 22 | 7 | 29 | 101 |
| Total | 0 | 1 | 0 | 1 | 107 | 89 | 1 | 197 | 10 | 0 | 30 | 40 | 0 | 96 | 35 | 131 | 369 |
| 08:00 AM | 0 | 0 | 0 | 0 | 9 | 35 | 1 | 45 | 4 | 0 | 10 | 14 | 0 | 25 | 6 | 31 | 90 |
| 08:15 AM | 0 | 1 | 0 | 1 | 12 | 24 | 0 | 36 | 6 | 0 | 8 | 14 | 0 | 28 | 5 | 33 | 84 |
| 08:30 AM | 0 | 0 | 0 | 0 | 12 | 36 | 0 | 48 | 4 | 0 | 9 | 13 | 0 | 17 | 6 | 23 | 84 |
| 08:45 AM | 0 | 0 | 0 | 0 | 9 | 30 | 0 | 39 | 2 | 0 | 4 | 6 | 0 | 22 | 5 | 27 | 72 |
| Total | 0 | 1 | 0 | 1 | 42 | 125 | 1 | 168 | 16 | 0 | 31 | 47 | 0 | 92 | 22 | 114 | 330 |
| *** BREAK *** | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 0 | 0 | 0 | 8 | 25 | 0 | 33 | 8 | 2 | 20 | 30 | 0 | 23 | 2 | 25 | 88 |
| 04:15 PM | 0 | 1 | 0 | 1 | 14 | 39 | 0 | 53 | 12 | 1 | 28 | 41 | 1 | 25 | 5 | 31 | 126 |
| 04:30 PM | 0 | 3 | 0 | 3 | 11 | 24 | 0 | 35 | 11 | 0 | 19 | 30 | 0 | 47 | 3 | 50 | 118 |
| 04:45 PM | 1 | 0 | 0 | 1 | 16 | 34 | 0 | 50 | 13 | 0 | 23 | 36 | 0 | 50 | 6 | 56 | 143 |
| Total | 1 | 4 | 0 | 5 | 49 | 122 | 0 | 171 | 44 | 3 | 90 | 137 | 1 | 145 | 16 | 162 | 475 |
| 05:00 PM | 0 | 0 | 0 | 0 | 6 | 35 | 0 | 41 | 8 | 0 | 53 | 61 | 0 | 34 | 7 | 41 | 143 |
| 05:15 PM | 0 | 0 | 0 | 0 | 5 | 33 | 0 | 38 | 17 | 0 | 37 | 54 | 0 | 27 | 3 | 30 | 122 |
| 05:30 PM | 0 | 0 | 0 | 0 | 12 | 47 | 0 | 59 | 8 | 0 | 16 | 24 | 0 | 38 | 5 | 43 | 126 |
| 05:45 PM | 0 | 0 | 0 | 0 | 9 | 22 | 0 | 31 | 7 | 0 | 19 | 26 | 0 | 36 | 3 | 39 | 96 |
| Total | 0 | 0 | 0 | 0 | 32 | 137 | 0 | 169 | 40 | 0 | 125 | 165 | 0 | 135 | 18 | 153 | 487 |
| Grand Total | 1 | 6 | 0 | 7 | 230 | 473 | 2 | 705 | 110 | 3 | 276 | 389 | 1 | 468 | 91 | 560 | 1661 |
| Apprch % | 14.3 | 85.7 | 0 | | 32.6 | 67.1 | 0.3 | | 28.3 | 0.8 | 71 | | 0.2 | 83.6 | 16.2 | | |
| Total % | 0.1 | 0.4 | 0 | 0.4 | 13.8 | 28.5 | 0.1 | 42.4 | 6.6 | 0.2 | 16.6 | 23.4 | 0.1 | 28.2 | 5.5 | 33.7 | |

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--|---------------------|------|-------|------------|-----------------|------|-------|------------|-------------------------|------|-------|------------|-----------------|-----------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:15 AM | | | | | | | | | | | | | | | | | |
| 07:15 AM | 0 | 0 | 0 | 0 | 24 | 23 | 0 | 47 | 2 | 0 | 9 | 11 | 0 | 30 | 8 | 38 | 96 |
| 07:30 AM | 0 | 1 | 0 | 1 | 33 | 22 | 1 | 56 | 1 | 0 | 5 | 6 | 0 | 25 | 9 | 34 | 97 |
| 07:45 AM | 0 | 0 | 0 | 0 | 30 | 26 | 0 | 56 | 5 | 0 | 11 | 16 | 0 | 22 | 7 | 29 | 101 |
| 08:00 AM | 0 | 0 | 0 | 0 | 9 | 35 | 1 | 45 | 4 | 0 | 10 | 14 | 0 | 25 | 6 | 31 | 90 |
| Total Volume | 0 | 1 | 0 | 1 | 96 | 106 | 2 | 204 | 12 | 0 | 35 | 47 | 0 | 102 | 30 | 132 | 384 |
| % App. Total | 0 | 100 | 0 | | 47.1 | 52 | 1 | | 25.5 | 0 | 74.5 | | 0 | 77.3 | 22.7 | | |
| PHF | .000 | .250 | .000 | .250 | .727 | .757 | .500 | .911 | .600 | .000 | .795 | .734 | .000 | .850 | .833 | .868 | .950 |

Intersection Turning Movement Count

File Name : SR70&CR721S
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 2

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|------------|---------------------|------|-------|------------|-----------------|------|-------|------------|-------------------------|------|-------|------------|-----------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 07:30 AM | | | | 07:15 AM | | | | 07:45 AM | | | | 07:15 AM | | | |
|--------------|----------|------|------|------|----------|------|------|------|----------|------|------|------|----------|------|------|------|
| +0 mins. | 0 | 1 | 0 | 1 | 24 | 23 | 0 | 47 | 5 | 0 | 11 | 16 | 0 | 30 | 8 | 38 |
| +15 mins. | 0 | 0 | 0 | 0 | 33 | 22 | 1 | 56 | 4 | 0 | 10 | 14 | 0 | 25 | 9 | 34 |
| +30 mins. | 0 | 0 | 0 | 0 | 30 | 26 | 0 | 56 | 6 | 0 | 8 | 14 | 0 | 22 | 7 | 29 |
| +45 mins. | 0 | 1 | 0 | 1 | 9 | 35 | 1 | 45 | 4 | 0 | 9 | 13 | 0 | 25 | 6 | 31 |
| Total Volume | 0 | 2 | 0 | 2 | 96 | 106 | 2 | 204 | 19 | 0 | 38 | 57 | 0 | 102 | 30 | 132 |
| % App. Total | 0 | 100 | 0 | | 47.1 | 52 | 1 | | 33.3 | 0 | 66.7 | | 0 | 77.3 | 22.7 | |
| PHF | .000 | .500 | .000 | .500 | .727 | .757 | .500 | .911 | .792 | .000 | .864 | .891 | .000 | .850 | .833 | .868 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 04:45 PM

| | | | | | | | | | | | | | | | | | |
|--------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 04:45 PM | 1 | 0 | 0 | 1 | 16 | 34 | 0 | 50 | 13 | 0 | 23 | 36 | 0 | 50 | 6 | 56 | 143 |
| 05:00 PM | 0 | 0 | 0 | 0 | 6 | 35 | 0 | 41 | 8 | 0 | 53 | 61 | 0 | 34 | 7 | 41 | 143 |
| 05:15 PM | 0 | 0 | 0 | 0 | 5 | 33 | 0 | 38 | 17 | 0 | 37 | 54 | 0 | 27 | 3 | 30 | 122 |
| 05:30 PM | 0 | 0 | 0 | 0 | 12 | 47 | 0 | 59 | 8 | 0 | 16 | 24 | 0 | 38 | 5 | 43 | 126 |
| Total Volume | 1 | 0 | 0 | 1 | 39 | 149 | 0 | 188 | 46 | 0 | 129 | 175 | 0 | 149 | 21 | 170 | 534 |
| % App. Total | 100 | 0 | 0 | | 20.7 | 79.3 | 0 | | 26.3 | 0 | 73.7 | | 0 | 87.6 | 12.4 | | |
| PHF | .250 | .000 | .000 | .250 | .609 | .793 | .000 | .797 | .676 | .000 | .608 | .717 | .000 | .745 | .750 | .759 | .934 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 04:00 PM | | | | 04:45 PM | | | | 04:30 PM | | | | 04:15 PM | | | |
|--------------|----------|------|------|------|----------|------|------|------|----------|------|------|------|----------|------|------|------|
| +0 mins. | 0 | 0 | 0 | 0 | 16 | 34 | 0 | 50 | 11 | 0 | 19 | 30 | 1 | 25 | 5 | 31 |
| +15 mins. | 0 | 1 | 0 | 1 | 6 | 35 | 0 | 41 | 13 | 0 | 23 | 36 | 0 | 47 | 3 | 50 |
| +30 mins. | 0 | 3 | 0 | 3 | 5 | 33 | 0 | 38 | 8 | 0 | 53 | 61 | 0 | 50 | 6 | 56 |
| +45 mins. | 1 | 0 | 0 | 1 | 12 | 47 | 0 | 59 | 17 | 0 | 37 | 54 | 0 | 34 | 7 | 41 |
| Total Volume | 1 | 4 | 0 | 5 | 39 | 149 | 0 | 188 | 49 | 0 | 132 | 181 | 1 | 156 | 21 | 178 |
| % App. Total | 20 | 80 | 0 | | 20.7 | 79.3 | 0 | | 27.1 | 0 | 72.9 | | 0.6 | 87.6 | 11.8 | |
| PHF | .250 | .333 | .000 | .417 | .609 | .793 | .000 | .797 | .721 | .000 | .623 | .742 | .250 | .780 | .750 | .795 |

Intersection Turning Movement Count

City/County: Brighton/Highlands
 Weather: Clear
 Comments:

File Name : SR70&CR721S
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 1

Groups Printed- Heavy Vehicles

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|----------------------|---------------------|----------|----------|------------|-----------------|------------|----------|------------|-------------------------|----------|----------|------------|-----------------|------------|----------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 15 |
| 07:15 AM | 0 | 0 | 0 | 0 | 1 | 20 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 26 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 13 |
| 07:45 AM | 0 | 0 | 0 | 0 | 1 | 9 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 | 19 |
| Total | 0 | 0 | 0 | 0 | 2 | 44 | 0 | 46 | 0 | 0 | 0 | 0 | 0 | 27 | 0 | 27 | 73 |
| 08:00 AM | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 10 | 20 |
| 08:15 AM | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 11 | 1 | 0 | 1 | 2 | 0 | 6 | 1 | 7 | 20 |
| 08:30 AM | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 8 | 1 | 0 | 2 | 3 | 0 | 10 | 0 | 10 | 21 |
| 08:45 AM | 0 | 1 | 0 | 1 | 0 | 8 | 0 | 8 | 0 | 0 | 1 | 1 | 0 | 15 | 0 | 15 | 25 |
| Total | 0 | 1 | 0 | 1 | 5 | 31 | 1 | 37 | 2 | 0 | 4 | 6 | 0 | 41 | 1 | 42 | 86 |
| *** BREAK *** | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 12 | 23 |
| 04:15 PM | 0 | 0 | 0 | 0 | 1 | 9 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 | 19 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 1 | 1 | 0 | 15 | 1 | 16 | 25 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 2 | 2 | 0 | 11 | 0 | 11 | 22 |
| Total | 0 | 0 | 0 | 0 | 2 | 36 | 0 | 38 | 0 | 0 | 3 | 3 | 0 | 47 | 1 | 48 | 89 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 12 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 10 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 10 | 0 | 0 | 2 | 2 | 0 | 5 | 0 | 5 | 17 |
| 05:45 PM | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 11 | 19 |
| Total | 0 | 0 | 0 | 0 | 1 | 29 | 0 | 30 | 0 | 0 | 2 | 2 | 0 | 26 | 0 | 26 | 58 |
| Grand Total | 0 | 1 | 0 | 1 | 10 | 140 | 1 | 151 | 2 | 0 | 9 | 11 | 0 | 141 | 2 | 143 | 306 |
| Apprch % | 0 | 100 | 0 | | 6.6 | 92.7 | 0.7 | | 18.2 | 0 | 81.8 | | 0 | 98.6 | 1.4 | | |
| Total % | 0 | 0.3 | 0 | 0.3 | 3.3 | 45.8 | 0.3 | 49.3 | 0.7 | 0 | 2.9 | 3.6 | 0 | 46.1 | 0.7 | 46.7 | |

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--|---------------------|----------|----------|------------|-----------------|-----------|----------|------------|-------------------------|----------|----------|------------|-----------------|-----------|----------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 10 | 20 |
| 08:15 AM | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 11 | 1 | 0 | 1 | 2 | 0 | 6 | 1 | 7 | 20 |
| 08:30 AM | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 8 | 1 | 0 | 2 | 3 | 0 | 10 | 0 | 10 | 21 |
| 08:45 AM | 0 | 1 | 0 | 1 | 0 | 8 | 0 | 8 | 0 | 0 | 1 | 1 | 0 | 15 | 0 | 15 | 25 |
| Total | 0 | 1 | 0 | 1 | 5 | 31 | 1 | 37 | 2 | 0 | 4 | 6 | 0 | 41 | 1 | 42 | 86 |
| Total Volume | 0 | 1 | 0 | 1 | 5 | 31 | 1 | 37 | 2 | 0 | 4 | 6 | 0 | 41 | 1 | 42 | 86 |
| % App. Total | 0 | 100 | 0 | | 13.5 | 83.8 | 2.7 | | 33.3 | 0 | 66.7 | | 0 | 97.6 | 2.4 | | |
| PHF | .000 | .250 | .000 | .250 | .417 | .775 | .250 | .841 | .500 | .000 | .500 | .500 | .000 | .683 | .250 | .700 | .860 |

Intersection Turning Movement Count

File Name : SR70&CR721S
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 2

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|------------|---------------------|------|-------|------------|-----------------|------|-------|------------|-------------------------|------|-------|------------|-----------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 08:00 AM | | | | 07:15 AM | | | | 08:00 AM | | | | 08:00 AM | | | |
|--------------|----------|------|------|------|----------|-----------|------|-----------|----------|------|------|------|----------|------|------|------|
| +0 mins. | 0 | 0 | 0 | 0 | 1 | 20 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 10 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 1 | 0 | 1 | 2 | 0 | 6 | 1 | 7 |
| +30 mins. | 0 | 0 | 0 | 0 | 1 | 9 | 0 | 10 | 1 | 0 | 2 | 3 | 0 | 10 | 0 | 10 |
| +45 mins. | 0 | 1 | 0 | 1 | 3 | 7 | 0 | 10 | 0 | 0 | 1 | 1 | 0 | 15 | 0 | 15 |
| Total Volume | 0 | 1 | 0 | 1 | 5 | 42 | 0 | 47 | 2 | 0 | 4 | 6 | 0 | 41 | 1 | 42 |
| % App. Total | 0 | 100 | 0 | | 10.6 | 89.4 | 0 | | 33.3 | 0 | 66.7 | | 0 | 97.6 | 2.4 | |
| PHF | .000 | .250 | .000 | .250 | .417 | .525 | .000 | .560 | .500 | .000 | .500 | .500 | .000 | .683 | .250 | .700 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 04:00 PM

| | | | | | | | | | | | | | | | | | |
|--------------|------|------|------|------|------|-----------|------|-----------|------|------|------|------|------|------|------|------|-----------|
| 04:00 PM | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 12 | 23 |
| 04:15 PM | 0 | 0 | 0 | 0 | 1 | 9 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 | 19 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 1 | 1 | 0 | 15 | 1 | 16 | 25 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 2 | 2 | 0 | 11 | 0 | 11 | 22 |
| Total Volume | 0 | 0 | 0 | 0 | 2 | 36 | 0 | 38 | 0 | 0 | 3 | 3 | 0 | 47 | 1 | 48 | 89 |
| % App. Total | 0 | 0 | 0 | | 5.3 | 94.7 | 0 | | 0 | 0 | 100 | | 0 | 97.9 | 2.1 | | |
| PHF | .000 | .000 | .000 | .000 | .500 | .900 | .000 | .864 | .000 | .000 | .375 | .375 | .000 | .783 | .250 | .750 | .890 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 04:00 PM | | | | 04:00 PM | | | | 04:45 PM | | | | 04:00 PM | | | |
|--------------|----------|------|------|------|----------|-----------|------|-----------|----------|------|------|------|----------|------|------|------|
| +0 mins. | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 11 | 0 | 0 | 2 | 2 | 0 | 12 | 0 | 12 |
| +15 mins. | 0 | 0 | 0 | 0 | 1 | 9 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 15 | 1 | 16 |
| +45 mins. | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 2 | 2 | 0 | 11 | 0 | 11 |
| Total Volume | 0 | 0 | 0 | 0 | 2 | 36 | 0 | 38 | 0 | 0 | 4 | 4 | 0 | 47 | 1 | 48 |
| % App. Total | 0 | 0 | 0 | | 5.3 | 94.7 | 0 | | 0 | 0 | 100 | | 0 | 97.9 | 2.1 | |
| PHF | .000 | .000 | .000 | .000 | .500 | .900 | .000 | .864 | .000 | .000 | .500 | .500 | .000 | .783 | .250 | .750 |

Intersection Turning Movement Count

City/County: Brighton/Highlands
 Weather: Clear
 Comments:

File Name : SR70&CR721S
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 1

Groups Printed- UTurns

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|---------------|---------------------|------|-------|------------|-----------------|------|-------|------------|-------------------------|------|-------|------------|-----------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| *** BREAK *** | | | | | | | | | | | | | | | | | |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| Apprch % | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 100 | 0 | 0 | | |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | |

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|--|---------------------|------|-------|------------|-----------------|------|-------|------------|-------------------------|------|-------|------------|-----------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:00 AM | | | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % App. Total | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1
 Peak Hour for Each Approach Begins at:

| | 07:00 AM | | | | 07:00 AM | | | | 07:00 AM | | | | 07:00 AM | | | |
|--------------|----------|------|------|------|----------|------|------|------|----------|------|------|------|----------|------|------|------|
| +0 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +45 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % App. Total | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 05:00 PM

| | | | | | | | | | | | | | | | | | |
|--------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| % App. Total | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 100 | 0 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .000 | .250 | .250 |

Intersection Turning Movement Count

File Name : SR70&CR721S
 Site Code : 1802507
 Start Date : 11/15/2022
 Page No : 2

| Start Time | DRIVEWAY Southbound | | | | SR 70 Westbound | | | | CR 721 SOUTH Northbound | | | | SR 70 Eastbound | | | | Int. Total |
|------------|---------------------|------|-------|------------|-----------------|------|-------|------------|-------------------------|------|-------|------------|-----------------|------|-------|------------|------------|
| | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | |

Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Each Approach Begins at:

| | 04:00 PM | | | | 04:00 PM | | | | 04:00 PM | | | | 05:00 PM | | | |
|--------------|----------|------|------|------|----------|------|------|------|----------|------|------|------|----------|------|------|------|
| +0 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +45 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| % App. Total | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 100 | 0 | 0 | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .000 | .250 |

APPENDIX D: Existing Synchro and HCS LOS Computer Outputs

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.1 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 1 | 167 | 5 | 2 | 140 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 1 | 167 | 5 | 2 | 140 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 |
| Heavy Vehicles, % | 0 | 27 | 25 | 50 | 18 | 0 | 0 | 0 | 100 | 0 | 0 | 0 |
| Mvmt Flow | 1 | 192 | 6 | 2 | 161 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|-----|-----|--------|-----|-----|
| Conflicting Flow All | 161 | 0 | 0 | 198 | 0 | 0 | 362 | 362 | 195 | 362 | 365 | 161 |
| Stage 1 | - | - | - | - | - | - | 197 | 197 | - | 165 | 165 | - |
| Stage 2 | - | - | - | - | - | - | 165 | 165 | - | 197 | 200 | - |
| Critical Hdwy | 4.1 | - | - | 4.6 | - | - | 7.1 | 6.5 | 7.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.2 | - | - | 2.65 | - | - | 3.5 | 4 | 4.2 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1430 | - | - | 1134 | - | - | 598 | 569 | 649 | 598 | 566 | 889 |
| Stage 1 | - | - | - | - | - | - | 809 | 742 | - | 842 | 766 | - |
| Stage 2 | - | - | - | - | - | - | 842 | 766 | - | 809 | 739 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1430 | - | - | 1134 | - | - | 597 | 567 | 649 | 597 | 564 | 889 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 597 | 567 | - | 597 | 564 | - |
| Stage 1 | - | - | - | - | - | - | 808 | 741 | - | 841 | 764 | - |
| Stage 2 | - | - | - | - | - | - | 840 | 764 | - | 808 | 738 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|----------------------|----|--|--|-----|--|--|------|--|--|----|--|--|
| HCM Control Delay, s | 0 | | | 0.1 | | | 11.1 | | | 0 | | |
| HCM LOS | | | | | | | B | | | A | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|-----------------------|-------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 597 | 1430 | - | - | 1134 | - | - | - |
| HCM Lane V/C Ratio | 0.004 | 0.001 | - | - | 0.002 | - | - | - |
| HCM Control Delay (s) | 11.1 | 7.5 | 0 | - | 8.2 | 0 | - | 0 |
| HCM Lane LOS | B | A | A | - | A | A | - | A |
| HCM 95th %tile Q(veh) | 0 | 0 | - | - | 0 | - | - | - |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 0 | 211 | 2 | 0 | 206 | 0 | 7 | 1 | 1 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 211 | 2 | 0 | 206 | 0 | 7 | 1 | 1 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 |
| Heavy Vehicles, % | 0 | 18 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 232 | 2 | 0 | 226 | 0 | 8 | 1 | 1 | 0 | 0 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|-----|-----|--------|-----|-----|
| Conflicting Flow All | 226 | 0 | 0 | 234 | 0 | 0 | 459 | 459 | 233 | 460 | 460 | 226 |
| Stage 1 | - | - | - | - | - | - | 233 | 233 | - | 226 | 226 | - |
| Stage 2 | - | - | - | - | - | - | 226 | 226 | - | 234 | 234 | - |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1354 | - | - | 1345 | - | - | 516 | 502 | 811 | 515 | 501 | 818 |
| Stage 1 | - | - | - | - | - | - | 775 | 716 | - | 781 | 721 | - |
| Stage 2 | - | - | - | - | - | - | 781 | 721 | - | 774 | 715 | - |
| Platoon blocked, % | | - | - | | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1354 | - | - | 1345 | - | - | 516 | 502 | 811 | 513 | 501 | 818 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 516 | 502 | - | 513 | 501 | - |
| Stage 1 | - | - | - | - | - | - | 775 | 716 | - | 781 | 721 | - |
| Stage 2 | - | - | - | - | - | - | 781 | 721 | - | 772 | 715 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|----------------------|----|--|--|----|--|--|------|--|--|----|--|--|
| HCM Control Delay, s | 0 | | | 0 | | | 11.8 | | | 0 | | |
| HCM LOS | | | | | | | B | | | A | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|-----------------------|-------|------|-----|-----|------|-----|-----|-------|
| Capacity (veh/h) | 536 | 1354 | - | - | 1345 | - | - | - |
| HCM Lane V/C Ratio | 0.018 | - | - | - | - | - | - | - |
| HCM Control Delay (s) | 11.8 | 0 | - | - | 0 | - | - | 0 |
| HCM Lane LOS | B | A | - | - | A | - | - | A |
| HCM 95th %tile Q(veh) | 0.1 | 0 | - | - | 0 | - | - | - |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 2.9 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 0 | 123 | 35 | 109 | 133 | 1 | 10 | 0 | 30 | 0 | 1 | 0 |
| Future Vol, veh/h | 0 | 123 | 35 | 109 | 133 | 1 | 10 | 0 | 30 | 0 | 1 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 0 | 23 | 0 | 5 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 129 | 37 | 115 | 140 | 1 | 11 | 0 | 32 | 0 | 1 | 0 |

| Major/Minor | Major1 | | Major2 | | Minor1 | | Minor2 | | | | | |
|----------------------|--------|---|--------|-------|--------|---|--------|-----|-----|-----|-----|-----|
| Conflicting Flow All | 141 | 0 | 0 | 166 | 0 | 0 | 519 | 519 | 148 | 535 | 537 | 141 |
| Stage 1 | - | - | - | - | - | - | 148 | 148 | - | 371 | 371 | - |
| Stage 2 | - | - | - | - | - | - | 371 | 371 | - | 164 | 166 | - |
| Critical Hdwy | 4.1 | - | - | 4.15 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.2 | - | - | 2.245 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1455 | - | - | 1394 | - | - | 471 | 464 | 904 | 459 | 453 | 912 |
| Stage 1 | - | - | - | - | - | - | 859 | 779 | - | 653 | 623 | - |
| Stage 2 | - | - | - | - | - | - | 653 | 623 | - | 843 | 765 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1455 | - | - | 1394 | - | - | 438 | 422 | 904 | 413 | 412 | 912 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 438 | 422 | - | 413 | 412 | - |
| Stage 1 | - | - | - | - | - | - | 859 | 779 | - | 653 | 567 | - |
| Stage 2 | - | - | - | - | - | - | 593 | 567 | - | 814 | 765 | - |

| Approach | EB | WB | NB | SB |
|----------------------|----|-----|------|------|
| HCM Control Delay, s | 0 | 3.5 | 10.4 | 13.8 |
| HCM LOS | | | B | B |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|-----------------------|-------|------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 714 | 1455 | - | - | 1394 | - | - | 412 |
| HCM Lane V/C Ratio | 0.059 | - | - | - | 0.082 | - | - | 0.003 |
| HCM Control Delay (s) | 10.4 | 0 | - | - | 7.8 | 0 | - | 13.8 |
| HCM Lane LOS | B | A | - | - | A | A | - | B |
| HCM 95th %tile Q(veh) | 0.2 | 0 | - | - | 0.3 | - | - | 0 |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 4.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 1 | 199 | 22 | 48 | 162 | 0 | 44 | 1 | 126 | 1 | 4 | 0 |
| Future Vol, veh/h | 1 | 199 | 22 | 48 | 162 | 0 | 44 | 1 | 126 | 1 | 4 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 22 | 5 | 2 | 18 | 0 | 0 | 0 | 2 | 0 | 0 | 0 |
| Mvmt Flow | 1 | 216 | 24 | 52 | 176 | 0 | 48 | 1 | 137 | 1 | 4 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|-----|-------|--------|-----|-----|
| Conflicting Flow All | 176 | 0 | 0 | 240 | 0 | 0 | 512 | 510 | 228 | 579 | 522 | 176 |
| Stage 1 | - | - | - | - | - | - | 230 | 230 | - | 280 | 280 | - |
| Stage 2 | - | - | - | - | - | - | 282 | 280 | - | 299 | 242 | - |
| Critical Hdwy | 4.1 | - | - | 4.12 | - | - | 7.1 | 6.5 | 6.22 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.2 | - | - | 2.218 | - | - | 3.5 | 4 | 3.318 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1412 | - | - | 1327 | - | - | 476 | 469 | 811 | 429 | 462 | 872 |
| Stage 1 | - | - | - | - | - | - | 777 | 718 | - | 731 | 683 | - |
| Stage 2 | - | - | - | - | - | - | 729 | 683 | - | 714 | 709 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1412 | - | - | 1327 | - | - | 456 | 448 | 811 | 344 | 442 | 872 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 456 | 448 | - | 344 | 442 | - |
| Stage 1 | - | - | - | - | - | - | 776 | 717 | - | 730 | 654 | - |
| Stage 2 | - | - | - | - | - | - | 693 | 654 | - | 592 | 708 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|----------------------|----|--|--|-----|--|--|------|--|--|------|--|--|
| HCM Control Delay, s | 0 | | | 1.8 | | | 12.4 | | | 13.7 | | |
| HCM LOS | | | | | | | B | | | B | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|-----------------------|-------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 673 | 1412 | - | - | 1327 | - | - | 418 |
| HCM Lane V/C Ratio | 0.276 | 0.001 | - | - | 0.039 | - | - | 0.013 |
| HCM Control Delay (s) | 12.4 | 7.6 | 0 | - | 7.8 | 0 | - | 13.7 |
| HCM Lane LOS | B | A | A | - | A | A | - | B |
| HCM 95th %tile Q(veh) | 1.1 | 0 | - | - | 0.1 | - | - | 0 |

HCS Two-Lane Highway Report

Project Information

| | | | |
|---------------------|---|---------------|----------------|
| Analyst | Fathy Abdalla | Date | 9/27/2023 |
| Agency | KCA | Analysis Year | 2022 |
| Jurisdiction | Highlands County | Time Analyzed | AM |
| Project Description | SR 70 Widening from Lonesome Island Rd to CR 721 (No Build) | Units | U.S. Customary |

Segment 1

Vehicle Inputs

| | | | |
|--------------|--------------|-----------------------|-------|
| Segment Type | Passing Zone | Length, ft | 40600 |
| Measured FFS | Measured | Free-Flow Speed, mi/h | 60.0 |

Demand and Capacity

| | | | |
|-------------------------------------|------|----------------------------------|-------|
| Directional Demand Flow Rate, veh/h | 278 | Opposing Demand Flow Rate, veh/h | 181 |
| Peak Hour Factor | 0.95 | Total Trucks, % | 14.70 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.16 |

Intermediate Results

| | | | |
|-----------------------------------|----------|----------------------------------|---------|
| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 60.0 |
| Speed Slope Coefficient (m) | 4.40580 | Speed Power Coefficient (p) | 0.54476 |
| PF Slope Coefficient (m) | -1.21258 | PF Power Coefficient (p) | 0.78531 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.7 |
| %Improvement to Percent Followers | 0.0 | %Improvement to Speed | 0.0 |

Subsegment Data

| # | Segment Type | Length, ft | Radius, ft | Superelevation, % | Average Speed, mi/h |
|---|--------------|------------|------------|-------------------|---------------------|
| 1 | Tangent | 40600 | - | - | 58.3 |

Vehicle Results

| | | | |
|------------------------------|------|--|------|
| Average Speed, mi/h | 58.3 | Percent Followers, % | 35.8 |
| Segment Travel Time, minutes | 7.92 | Follower Density (FD), followers/mi/ln | 1.7 |
| Vehicle LOS | A | | |

Facility Results

| T | VMT veh-mi/AP | VHD veh-h/p | Follower Density, followers/ mi/ln | LOS |
|---|------------------|----------------|---------------------------------------|-----|
| 1 | 508 | 0.25 | 1.7 | A |

HCS Two-Lane Highway Report

Project Information

| | | | |
|---------------------|---|---------------|----------------|
| Analyst | Fathy Abdalla | Date | 9/27/2023 |
| Agency | KCA | Analysis Year | 2022 |
| Jurisdiction | Highlands County | Time Analyzed | PM |
| Project Description | SR 70 Widening from Lonesome Island Rd to CR 721 (No Build) | Units | U.S. Customary |

Segment 1

Vehicle Inputs

| | | | |
|--------------|--------------|-----------------------|-------|
| Segment Type | Passing Zone | Length, ft | 40600 |
| Measured FFS | Measured | Free-Flow Speed, mi/h | 60.0 |

Demand and Capacity

| | | | |
|-------------------------------------|------|----------------------------------|-------|
| Directional Demand Flow Rate, veh/h | 254 | Opposing Demand Flow Rate, veh/h | 240 |
| Peak Hour Factor | 0.95 | Total Trucks, % | 14.70 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.15 |

Intermediate Results

| | | | |
|-----------------------------------|----------|----------------------------------|---------|
| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 60.0 |
| Speed Slope Coefficient (m) | 4.42691 | Speed Power Coefficient (p) | 0.52874 |
| PF Slope Coefficient (m) | -1.22637 | PF Power Coefficient (p) | 0.78082 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.5 |
| %Improvement to Percent Followers | 0.0 | %Improvement to Speed | 0.0 |

Subsegment Data

| # | Segment Type | Length, ft | Radius, ft | Superelevation, % | Average Speed, mi/h |
|---|--------------|------------|------------|-------------------|---------------------|
| 1 | Tangent | 40600 | - | - | 58.4 |

Vehicle Results

| | | | |
|------------------------------|------|--|------|
| Average Speed, mi/h | 58.4 | Percent Followers, % | 34.3 |
| Segment Travel Time, minutes | 7.91 | Follower Density (FD), followers/mi/ln | 1.5 |
| Vehicle LOS | A | | |

Facility Results

| T | VMT veh-mi/AP | VHD veh-h/p | Follower Density, followers/ mi/ln | LOS |
|---|------------------|----------------|---------------------------------------|-----|
| 1 | 463 | 0.22 | 1.5 | A |

APPENDIX E: Crash Data and FDOT Statewide Crash Facts

FDOT State Safety Office GIS

| Calendar Y | FDOT Crash Number | Reporting Agency | Case Number | Crash Date | Day | On Roadway Name | Int Roadway Name | Nearest Inventory MP | Travel Direction | Vehicle 1 | Highest Injury in Crash | Lighting | Weather | Road Surface | Crash Harmful Event | Manner of Collision | Vehicle Movement | Driver Action Vehicle 1 |
|------------|-------------------|------------------|-------------|------------|-----------|-----------------|-------------------|----------------------|------------------|-----------|--------------------------------|---------------------|---------------------|--------------|-----------------------------------|----------------------------------|--------------------------|--------------------------------|
| 2020 | 882524830 | FHPF20OFF010503 | | 27-Feb-20 | FRIDAY | SR 70 | CR 721 | 29.178 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 01 FRONT TO REAR | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2018 | 871269200 | FHPF18OFF004358 | | 18-Jan-18 | FRIDAY | SR 70 | GREENBRIER LN | 23.352 | E EAST | | 5 FATAL(WITHIN 30 DAYS) INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 27 GUARDRAIL FACE | 02 FRONT TO FRONT | 01 STRAIGHT AHEAD | FAILED TO KEEP IN PROPER LANE |
| 2018 | 821284980 | HCSO18CAD046338 | | 12-Jul-18 | FRIDAY | SR 70 | CR 721 | 29.235 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 03 RAIN | 02 WET | 18 OTHER NON-FIXED OBJECT | 01 FRONT TO REAR | 01 STRAIGHT AHEAD | FOLLOWED TOO CLOSELY |
| 2018 | 872315400 | FHPF18OFF046600 | | 13-Jul-18 | SATURDAY | SR 70 | JC DURRANCE RD | 22.125 | E EAST | | 2 POSSIBLE INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 13 ANIMAL | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2018 | 872040720 | FHPF18OFF051242 | | 3-Aug-18 | SATURDAY | CR-721 | SR-70 | 0.956 | S SOUTH | | 5 FATAL(WITHIN 30 DAYS) INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 06 FELL/JUMPED FROM MOTOR VEHICLE | 77 OTHER (SEE NARRATIVE) | 15 NEGOTIATING A CURVE | RAN OFF ROADWAY |
| 2018 | 871558060 | FHPF18OFF013577 | | 25-Feb-18 | MONDAY | SR 70 | CR 721 | 29.238 | S SOUTH | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 04 FOG, SMOG, SMOKE | 01 DRY | 01 OVERTURN/ROLLOVER | 77 OTHER (SEE NARRATIVE) | 03 TURNING LEFT | RAN STOP SIGN |
| 2018 | 871884620 | FHPF18OFF056222 | | 25-Aug-18 | SUNDAY | SR 70 | D C BAR RANCH RD | 23.279 | E EAST | | 3 NO-INCAPACITATING INJURY | 02 DUSK | 01 CLEAR | 01 DRY | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | FAILED TO KEEP IN PROPER LANE |
| 2018 | 880245340 | FHPF18OFF079328 | | 7-Dec-18 | SATURDAY | SR 70 | GREENBRIER LN | 26.294 | W WEST | | 4 INCAPACITATING INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 01 FRONT TO REAR | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2018 | 872511760 | FHPF18OFF058900 | | 6-Sep-18 | FRIDAY | SR 70 | CR 721 | 29.116 | W WEST | | 3 NO-INCAPACITATING INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 01 FRONT TO REAR | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2018 | 871269160 | FHPF18OFF003419 | | 14-Jan-18 | MONDAY | SR 70 | CR 721 | 29.216 | N NORTH | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 03 ANGLE | 05 TURNING RIGHT | FAILED TO YIELD RIGHT-OF-WAY |
| 2018 | 872050900 | FHPF18OFF041874 | | 22-Jun-18 | SATURDAY | SR 70 | CR 721 | 29.241 | S SOUTH | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | RAN OFF ROADWAY |
| 2018 | 871524010 | FHPF18OFF028342 | | 25-Apr-18 | THURSDAY | SR 70 | GREENBRIER LN | 23.028 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 01 OVERTURN/ROLLOVER | 05 SIDESWIPE, OPPOSITE DIRECTION | 01 STRAIGHT AHEAD | NOT CODED |
| 2018 | 871555960 | FHPF18OFF030933 | | 5-May-18 | SUNDAY | SR 70 | CR 721 | 29.241 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 25 DITCH | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2018 | 871269360 | FHPF18OFF010889 | | 15-Feb-18 | FRIDAY | SR 70 | CR 721 | 29.116 | E EAST | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 13 ANIMAL | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2019 | 821276110 | HCSO19CAD050084 | | 3-Aug-19 | SUNDAY | SR 70 | D C BAR RANCH RD | 24.029 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 03 RAIN | 02 WET | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 88 UNKNOWN | NO CONTRIBUTING ACTION |
| 2019 | 880872240 | FHPF19OFF008689 | | 14-Feb-19 | FRIDAY | SR 70 | CR 721 | 28.716 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 18 OTHER NON-FIXED OBJECT | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2019 | 880433250 | FHPF19OFF028363 | | 30-May-19 | FRIDAY | SR 70 | 4D PARTNERSHIP RD | 22.879 | S SOUTH | | 5 FATAL(WITHIN 30 DAYS) INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 03 ANGLE | 13 STOPPED IN TRAFFIC | OTHER CONTRIBUTING ACTION |
| 2020 | 890949150 | HCSO20CAD051810 | | 6-Sep-20 | MONDAY | SR 70 E | JC DURRANCE RD | 21.606 | W WEST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 13 ANIMAL | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2018 | 872050940 | FHPF18OFF042984 | | 27-Jun-18 | THURSDAY | SR 70 | CR 721 | 28.216 | W WEST | | 1 NO INJURY | 03 DAWN | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 00 NOT CODED | NOT CODED |
| 2018 | 871991140 | FHPF18OFF035813 | | 26-May-18 | SUNDAY | SR 70 | CR 721 | 29.207 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 02 CLOUDY | 02 WET | 14 MOTOR VEHICLE IN TRANSPORT | 01 FRONT TO REAR | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2018 | 871523580 | FHPF18OFF007270 | | 31-Jan-18 | THURSDAY | SR 70 | D C BAR RANCH RD | 24.029 | W WEST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 03 ANGLE | 06 CHANGING LANES | OPERATED MV IN CARLESS OR NEGL |
| 2020 | 882101700 | FHPF20OFF012810 | | 10-Mar-20 | WEDNESDAY | SR 70 | D C BAR RANCH RD | 26.279 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 09 OTHER NON-COLLISION | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2018 | 871524000 | FHPF18OFF027511 | | 21-Apr-18 | SUNDAY | SR 70 | SOUTHWIND RD | 21.874 | E EAST | | 2 POSSIBLE INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | FAILED TO KEEP IN PROPER LANE |
| 2020 | 882411270 | FHPF20OFF02124 | | 26-May-20 | WEDNESDAY | SR 70 | 4D PARTNERSHIP RD | 24.179 | W WEST | | 2 POSSIBLE INJURY | 01 DAYLIGHT | 03 RAIN | 02 WET | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 01 STRAIGHT AHEAD | OTHER CONTRIBUTING ACTION |
| 2019 | 881710790 | FHPF19OFF039631 | | 3-Aug-19 | SUNDAY | SR 70 | CR 721 | 29.257 | E EAST | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 13 ANIMAL | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2019 | 819849980 | FHPF19OFF023728 | | 5-May-19 | MONDAY | SR 70 | CR 721 | 28.238 | E EAST | | 4 INCAPACITATING INJURY | 01 DAYLIGHT | 02 CLOUDY | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 01 FRONT TO REAR | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2019 | 880872230 | FHPF19OFF008629 | | 14-Feb-19 | FRIDAY | SR 70 | US 27 | 23.99 | W WEST | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 11 OVERTAKING/PASSING | IMPROPER PASSING |
| 2019 | 858704990 | HCSO19CAD002064 | | 8-Jan-19 | WEDNESDAY | SR 70 | GREENBRIER LN | 24.278 | W WEST | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 13 ANIMAL | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2019 | 880186940 | FHPF19OFF035618 | | 11-Jul-19 | FRIDAY | SR 70 | CR 721 | 29.138 | W WEST | | 3 NO-INCAPACITATING INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 11 OVERTAKING/PASSING | NO CONTRIBUTING ACTION |
| 2019 | 882562960 | FHPF19OFF062817 | | 15-Dec-19 | MONDAY | SR 70 | CR 721 | 29.216 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 03 ANGLE | 11 OVERTAKING/PASSING | IMPROPER PASSING |
| 2019 | 880888940 | FHPF19OFF042644 | | 20-Aug-19 | WEDNESDAY | SR 70 | CR 721 | 29.235 | W WEST | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 13 ANIMAL | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2019 | 881482260 | FHPF19OFF043621 | | 25-Aug-19 | MONDAY | SR 70 | CR 721 | 28.216 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 11 OVERTAKING/PASSING | WRONG SIDE OF WRONG WAY |
| 2019 | 881710740 | FHPF19OFF037241 | | 20-Jul-19 | SUNDAY | SR 70 | GREENBRIER LN | 24.278 | W WEST | | 3 NO-INCAPACITATING INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 03 ANGLE | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2020 | 883411960 | FHPF20OFF034809 | | 16-Aug-20 | MONDAY | SR 70 | GREENBRIER LN | 23.978 | E EAST | | 5 FATAL(WITHIN 30 DAYS) INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 77 OTHER (SEE NARRATIVE) | FAILED TO KEEP IN PROPER LANE |
| 2020 | 883516270 | FHPF20OFF026252 | | 21-Jun-20 | MONDAY | SR 70 | CR 721 | 27.696 | W WEST | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 02 CLOUDY | 02 WET | 25 DITCH | 77 OTHER (SEE NARRATIVE) | 15 NEGOTIATING A CURVE | NO CONTRIBUTING ACTION |
| 2019 | 880245660 | FHPF19OFF006196 | | 1-Feb-19 | SATURDAY | SR 70 | CR 721 | 28.916 | E EAST | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 04 FOG, SMOG, SMOKE | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 01 FRONT TO REAR | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2020 | 882988290 | FHPF20OFF018748 | | 2-May-20 | SUNDAY | SR 70 | D C BAR RANCH RD | 25.264 | O OFF-ROAD | | 2 POSSIBLE INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 03 ANGLE | 03 TURNING LEFT | FAILED TO YIELD RIGHT-OF-WAY |
| 2020 | 898623340 | HCSO20CAD028264 | | 13-May-20 | THURSDAY | SR 70 | GREENBRIER LN | 22.459 | W WEST | | 1 NO INJURY | 01 DAYLIGHT | 02 CLOUDY | 01 DRY | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2019 | 858709560 | HCSO19CAD067257 | | 9-Oct-19 | THURSDAY | SR 70 | D C BAR RANCH RD | 24.279 | W WEST | | 3 NO-INCAPACITATING INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 01 STRAIGHT AHEAD | OTHER CONTRIBUTING ACTION |
| 2020 | 821263850 | HCSO20CAD067258 | | 18-Nov-20 | THURSDAY | SR 70 E | CR 29 | 22.245 | W WEST | | 1 NO INJURY | 03 DAWN | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 01 FRONT TO REAR | 01 STRAIGHT AHEAD | FOLLOWED TOO CLOSELY |
| 2020 | 821305630 | HCSO20CAD003372 | | 15-Jan-20 | THURSDAY | SR 70 | D C BAR RANCH RD | 23.995 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NOT CODED |
| 2020 | 882411360 | FHPF20OFF033873 | | 10-Aug-20 | TUESDAY | SR 70 | CR 721 | 28.716 | E EAST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2020 | 883768100 | FHPF20OFF044637 | | 15-Oct-20 | FRIDAY | SR 70 | CR 721 | 28.397 | E EAST | | 5 FATAL(WITHIN 30 DAYS) INJURY | 02 DUSK | 01 CLEAR | 01 DRY | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2020 | 883959480 | FHPF20OFF048500 | | 8-Nov-20 | MONDAY | SR 70 | GREENBRIER LN | 23.126 | E EAST | | 3 NO-INCAPACITATING INJURY | 05 DARK-NOT LIGHTED | 03 RAIN | 02 WET | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 01 STRAIGHT AHEAD | NOT CODED |
| 2020 | 883978700 | FHPF20OFF044281 | | 13-Oct-20 | WEDNESDAY | SR 70 | CR 721 | 28.966 | W WEST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 01 STRAIGHT AHEAD | FAILED TO KEEP IN PROPER LANE |
| 2021 | 885785830 | FHPF21OFF052640 | | 27-Oct-21 | THURSDAY | SR 70 | CR 721 | 28.801 | W WEST | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2021 | 244651210 | HCSO21CAD040761 | | 23-Jun-21 | THURSDAY | SR 70 | J C DURRANCE RD | 21.653 | W WEST | | 1 NO INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | OTHER CONTRIBUTING ACTION |
| 2021 | 884708800 | FHPF21OFF016809 | | 8-Apr-21 | FRIDAY | SR 70 | CR 721 | 29.207 | W WEST | | 4 INCAPACITATING INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 01 FRONT TO REAR | 01 STRAIGHT AHEAD | OPERATED MV IN CARLESS OR NEGL |
| 2021 | 858703790 | HCSO21CAD029709 | | 5-May-21 | THURSDAY | SR 70 | CR 721 | 29.212 | E EAST | | 1 NO INJURY | 03 DAWN | 04 FOG, SMOG, SMOKE | 01 DRY | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2021 | 885268740 | FHPF21OFF033109 | | 8-Jul-21 | FRIDAY | SR 70 | CR 721 | 27.846 | E EAST | | 1 NO INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 13 ANIMAL | 77 OTHER (SEE NARRATIVE) | 01 STRAIGHT AHEAD | NO CONTRIBUTING ACTION |
| 2019 | 880257780 | FHPF19OFF002776 | | 12-Jan-19 | SUNDAY | SR 70 | CR 721 | 27.238 | E EAST | | 5 FATAL(WITHIN 30 DAYS) INJURY | 01 DAYLIGHT | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 02 FRONT TO FRONT | 01 STRAIGHT AHEAD | IMPROPER PASSING |
| 2019 | 880872710 | FHPF19OFF025301 | | 14-May-19 | WEDNESDAY | SR 70 | GREENBRIER LN | 23.894 | E EAST | | 4 INCAPACITATING INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 05 SIDESWIPE, OPPOSITE DIRECTION | 01 STRAIGHT AHEAD | FAILED TO KEEP IN PROPER LANE |
| 2022 | 249379490 | FHP22ON0310826 | | 18-Jun-22 | SUNDAY | SR 70 | CR 721 | 28.657 | S SOUTH | | 5 FATAL(WITHIN 30 DAYS) INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 03 ANGLE | 10 MAKING U-TURN | IMPROPER TURN |
| 2022 | 248961800 | FHP22ON0181945 | | 10-Apr-22 | MONDAY | SR 70 | CR 721 | 27.736 | W WEST | | 2 POSSIBLE INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 27 GUARDRAIL FACE | 77 OTHER (SEE NARRATIVE) | 15 NEGOTIATING A CURVE | NO CONTRIBUTING ACTION |
| 2022 | 249226900 | FHP22ON0223429 | | 3-May-22 | WEDNESDAY | SR 70 | CR 721 | 27.716 | E EAST | | 4 INCAPACITATING INJURY | 05 DARK-NOT LIGHTED | 01 CLEAR | 01 DRY | 14 MOTOR VEHICLE IN TRANSPORT | 02 FRONT TO FRONT | 15 NEGOTIATING A CURVE | FAILED TO KEEP IN PROPER LANE |

SignalFour Analytics

| REPORT_NUMBER | CRASH_YEAR | CRASH_DATE_AND_TIME | INVESTIGATING_AGENCY_REPORT_NUMBER | ON_STREET_ROAD_HIGHWAY | LIGHT_CONDITION | WEATHER_CONDITION | ROAD_SURFACE_CONDITION | FIRST_HARMFUL_EVENT | S4_CRASH_TYPE | S4_CRASH_SEVERITY | S4_DAY_OR_NIGHT |
|---------------|------------|---------------------|------------------------------------|------------------------|--------------------|-------------------|------------------------|-----------------------------------|--------------------------|-------------------|-----------------|
| 88437567 | 2021 | 2/27/2021 | FHPF21OFF009454 | SR-70 W | Dark - Not Lighted | Clear | Dry | Motor Vehicle in Transport | Single Vehicle | Injury | DAY |
| 24987484 | 2022 | 10/10/2022 | FHP22ON0521573 | SR-70 | Dark - Not Lighted | Cloudy | Dry | Other Non-Fixed Object | Single Vehicle | No Injury | NIGHT |
| 89862519 | 2021 | 6/23/2021 | HCSO21CAD040499 | SR 70 X SW CR721 | Dark - Not Lighted | Clear | Dry | Motor Vehicle in Transport | Opposing Sideswipe | No Injury | NIGHT |
| 88578582 | 2021 | 10/29/2021 | FHPF21OFF052649 | SR-70 | Dark - Not Lighted | Clear | Dry | Other Non-Fixed Object | Single Vehicle | No Injury | NIGHT |
| 24989666 | 2022 | 8/10/2022 | FHP22ON0405295 | STATE ROAD 70 | Daylight | Clear | Dry | Thrown or Falling Object | Other | No Injury | DAY |
| 88016200 | 2019 | 5/12/2019 | FHPF19OFF024813 | CR-721 | Dark - Not Lighted | Rain | Wet | Other Non-Collision | Single Vehicle | No Injury | NIGHT |
| 83790370 | 2021 | 6/23/2021 | FHPF21OFF030232 | SR-70 | Dark - Not Lighted | Clear | Dry | Motor Vehicle in Transport | Left Leaving | No Injury | NIGHT |
| 24959384 | 2022 | 8/31/2022 | FHP22ON0443610 | SR-70 | Daylight | Clear | Dry | Guardrail Face | Off Road | Injury | DAY |
| 88456329 | 2021 | 3/18/2021 | FHPF21OFF012835 | SR 70 | Daylight | Clear | Dry | Motor Vehicle in Transport | Other | No Injury | DAY |
| 25049365 | 2022 | 12/16/2022 | FHP22ON0648770 | STATE ROAD 70 | Daylight | Clear | Dry | Cargo/Equipment Loss or Shift | Other | Injury | DAY |
| 24962757 | 2022 | 10/10/2022 | FHP22ON0521537 | SR-70 | Dark - Not Lighted | Clear | Dry | Motor Vehicle in Transport | Opposing Sideswipe | Serious Injury | NIGHT |
| 88148219 | 2019 | 8/7/2019 | FHPF19OFF040129 | SR 70 | Daylight | Cloudy | Dry | Struck by Falling, Shifting Cargo | Same Direction Sideswipe | No Injury | DAY |
| 88397927 | 2021 | 2/8/2021 | FHPF21OFF006007 | SR 70 | Daylight | Cloudy | Dry | Animal | Animal | No Injury | DAY |
| 88545657 | 2021 | 7/26/2021 | FHPF21OFF036258 | SR 70 | Daylight | Cloudy | Dry | Motor Vehicle in Transport | Same Direction Sideswipe | No Injury | DAY |
| 89582881 | 2021 | 12/3/2021 | FHP21ON0018731 | STATE ROAD 70 | Daylight | Clear | Dry | Motor Vehicle in Transport | Rear End | No Injury | DAY |
| 88353354 | 2020 | 10/22/2020 | FHPF20OFF045509 | STATE ROAD 70 | Daylight | Rain | Wet | Guardrail Face | Off Road | No Injury | DAY |
| 24959395 | 2022 | 9/24/2022 | FHP22ON0489559 | SR-70 | Daylight | Clear | Dry | Other Non-Fixed Object | Other | No Injury | DAY |
| 24465943 | 2021 | 12/7/2021 | HCSO21CAD076875 | SR 70 | Daylight | Clear | Dry | Motor Vehicle in Transport | Head On | No Injury | DAY |
| 84644943 | 2021 | 3/26/2021 | HCSO21CAD019543 | SR 70 | Dark - Not Lighted | Clear | Dry | Animal | Animal | No Injury | NIGHT |
| 87891325 | 2021 | 3/25/2021 | HCSO21CAD019511 | SR 70 | Dark - Not Lighted | Clear | Dry | Animal | Animal | Injury | NIGHT |
| 24896192 | 2022 | 4/26/2022 | FHP22ON0209412 | SR-70 | Daylight | Clear | Dry | Other Non-Collision | Single Vehicle | No Injury | DAY |
| 88444567 | 2021 | 2/12/2021 | FHPF21OFF006874 | STATE ROAD 70 | Daylight | Clear | Dry | Motor Vehicle in Transport | Same Direction Sideswipe | No Injury | DAY |
| 88438595 | 2021 | 4/23/2021 | FHPF21OFF019268 | STATE ROAD 70 | Dark - Not Lighted | Clear | Dry | Motor Vehicle in Transport | Unknown | Injury | NIGHT |
| 87207048 | 2018 | 9/1/2018 | FHPF18OFF057458 | 25750 SR-70 | Dark - Not Lighted | Clear | Dry | Ditch | Off Road | No Injury | NIGHT |
| 87178415 | 2018 | 2/20/2018 | FHPF18OFF011986 | STATE ROAD 70 | Daylight | Clear | Dry | Motor Vehicle in Transport | Rear End | No Injury | DAY |
| 25029987 | 2022 | 11/6/2022 | FHP22ON0573911 | SR-70 | Daylight | Clear | Dry | Motor Vehicle in Transport | Left Leaving | Fatality | DAY |
| 25439531 | 2022 | 10/27/2022 | HCSO22OFF152776 | STATE ROAD 70 E | Daylight | Clear | Dry | Motor Vehicle in Transport | Rear End | No Injury | DAY |
| 89862733 | 2021 | 2/23/2021 14:45 | HCSO21CAD012344 | SR 70 E MM 95 | Dusk | Clear | Dry | Motor Vehicle in Transport | Opposing Sideswipe | No Injury | DAY |
| 85870233 | 2022 | 2/3/2022 17:55 | HCSO22CAD007116 | SR 70 E MM 95 | Dusk | Clear | Dry | Animal | Animal | No Injury | DAY |



Traffic Crash Facts

Annual Report 2020

Providing Highway Safety and Security through Excellence in Service, Education, and Enforcement

Environmental Factors & Injury Levels

Note: The environmental factor titled "Road Contributing Circumstance" can be listed on the crash report with more than one value per crash event. Therefore injury totals may differ from the true count of fatalities and injuries found in the summary on pages 8 & 9.

| | | Fatal | Incapacitating | Non-Incapacitating | Possible | No Injuries |
|-------------------------------|-----------------------------|--------------|----------------|--------------------|----------------|----------------|
| Weather Conditions | Blowing Sand, Soil, Dirt | 0 | 3 | 0 | 3 | 12 |
| | Clear | 2,524 | 12,025 | 47,419 | 100,650 | 439,938 |
| | Cloudy | 514 | 2,308 | 9,221 | 19,382 | 74,233 |
| | Fog, Smog, Smoke | 31 | 67 | 186 | 315 | 1,273 |
| | Not Specified | 0 | 0 | 1 | 3 | 92 |
| | Other, Explain in Narrative | 13 | 12 | 51 | 152 | 1,119 |
| | Rain | 250 | 1,197 | 5,851 | 13,547 | 56,889 |
| | Severe Crosswinds | 0 | 1 | 7 | 24 | 68 |
| | Sleet/Hail/Freezing Rain | 0 | 1 | 2 | 4 | 25 |
| | Unknown | 0 | 0 | 0 | 0 | 0 |
| | Total | 3,332 | 15,614 | 62,738 | 134,080 | 573,649 |
| Road Surface Condition | Dry | 2,875 | 13,515 | 53,165 | 112,672 | 485,085 |
| | Ice/Frost | 0 | 0 | 0 | 7 | 10 |
| | Mud, Dirt, Gravel | 6 | 62 | 153 | 143 | 751 |
| | Not Specified | 0 | 0 | 1 | 3 | 92 |
| | Oil | 0 | 4 | 9 | 17 | 25 |
| | Other, Explain in Narrative | 6 | 21 | 40 | 46 | 248 |
| | Sand | 0 | 20 | 28 | 39 | 208 |
| | Unknown | 9 | 10 | 41 | 154 | 1,295 |
| | Water (standing/moving) | 2 | 2 | 18 | 24 | 260 |
| | Wet | 434 | 1,980 | 9,283 | 20,975 | 85,675 |
| | Total | 3,332 | 15,614 | 62,738 | 134,080 | 573,649 |

14.99%

Environmental Factors & Injury Levels

Note: The environmental factor titled "Road Contributing Circumstance" can be listed on the crash report with more than one value per crash event. Therefore injury totals may differ from the true count of fatalities and injuries found in the summary on pages 8 & 9.

| | | Fatal | Incapacitating | Non-Incapacitating | Possible | No Injuries |
|--------------------------------|---|--------------|----------------|--------------------|----------------|----------------|
| Lighting Condition | Dark-Lighted | 996 | 3,341 | 13,041 | 27,101 | 112,157 |
| | Dark-Not Lighted | 809 | 2,150 | 5,373 | 7,868 | 31,426 |
| | Dark-Unknown Lighting | 19 | 23 | 97 | 213 | 1,290 |
| | Dawn | 62 | 303 | 1,188 | 2,298 | 9,624 |
| | Daylight | 1,309 | 9,206 | 40,721 | 91,158 | 398,016 |
| | Dusk | 127 | 569 | 2,271 | 5,249 | 19,119 |
| | Not Specified | 0 | 0 | 1 | 3 | 91 |
| | Other, Explain in Narrative | 4 | 11 | 23 | 44 | 290 |
| | Unknown | 6 | 11 | 23 | 146 | 1,636 |
| | Total | 3,332 | 15,614 | 62,738 | 134,080 | 573,649 |
| Road Contributing Circumstance | Debris | 4 | 17 | 70 | 109 | 1,120 |
| | None | 3,152 | 14,853 | 59,313 | 127,002 | 543,539 |
| | Non-Highway Work | 0 | 1 | 2 | 16 | 90 |
| | Obstruction in Roadway | 4 | 29 | 178 | 316 | 1,458 |
| | Other, Explain in Narrative | 11 | 80 | 398 | 785 | 3,653 |
| | Road Surface Condition (wet, icy, snow, slush, etc.) | 113 | 491 | 2,491 | 5,296 | 20,435 |
| | Ruts, Holes, Bumps | 5 | 38 | 85 | 85 | 325 |
| | Shoulders (none, low, soft, high) | 5 | 9 | 30 | 39 | 180 |
| | Traffic Control Device Inoperative, Missing or Obscured | 0 | 18 | 80 | 154 | 577 |
| | Unknown | 40 | 73 | 216 | 587 | 3,126 |
| | Work Zone (construction/maintenance/utility) | 77 | 303 | 1,083 | 2,442 | 10,583 |
| | Worn, Travel-Polished Surface | 0 | 7 | 15 | 27 | 100 |
| | Total | 3,411 | 15,919 | 63,961 | 136,858 | 585,186 |

25.88%

Environmental Factors & Injury Levels

***Note:** The environmental factor titled "Road Contributing Circumstance" can be listed on the crash report with more than one value per crash event. Therefore injury totals may differ from the true count of fatalities and injuries found in the summary on pages 8 & 9.*

| | | Fatal | Incapacitating | Non-Incapacitating | Possible | No Injuries |
|----------------------------|-------------------------------|--------------|----------------|--------------------|----------------|----------------|
| Roadway Type | County | 597 | 2,943 | 12,004 | 25,138 | 95,525 |
| | Forest Road | 0 | 11 | 29 | 17 | 103 |
| | Interstate | 360 | 1,576 | 5,781 | 12,319 | 60,450 |
| | Local | 789 | 4,356 | 19,228 | 42,663 | 182,489 |
| | Not Specified | 0 | 0 | 10 | 3 | 105 |
| | Other, Explain in Narrative | 6 | 87 | 263 | 509 | 2,875 |
| | Parking Lot | 26 | 385 | 1,935 | 4,523 | 40,985 |
| | Private Roadway | 13 | 119 | 454 | 667 | 4,261 |
| | State | 904 | 3,689 | 14,839 | 31,893 | 122,468 |
| | Turnpike/Toll | 50 | 264 | 981 | 1,673 | 11,553 |
| | U.S. | 587 | 2,184 | 7,214 | 14,675 | 52,835 |
| | Unknown | 0 | 0 | 0 | 0 | 0 |
| | Total | 3,332 | 15,614 | 62,738 | 134,080 | 573,649 |
| First Harmful Event | Animal | 7 | 31 | 168 | 361 | 2,463 |
| | Bridge Overhead Structure | 0 | 5 | 13 | 18 | 109 |
| | Bridge Pier or Support | 1 | 6 | 10 | 17 | 62 |
| | Bridge Rail | 2 | 10 | 28 | 54 | 166 |
| | Cable Barrier | 1 | 2 | 16 | 47 | 338 |
| | Cargo/Equipment Loss or Shift | 0 | 8 | 40 | 38 | 645 |
| | Concrete Traffic Barrier | 30 | 165 | 748 | 1,282 | 5,302 |
| | Cross Centerline | 0 | 0 | 0 | 0 | 0 |
| | Cross Median | 0 | 0 | 0 | 0 | 4 |
| | Culvert | 19 | 58 | 122 | 110 | 331 |

Environmental Factors & Injury Levels

Note: The environmental factor titled "Road Contributing Circumstance" can be listed on the crash report with more than one value per crash event. Therefore injury totals may differ from the true count of fatalities and injuries found in the summary on pages 8 & 9.

| | | Fatal | Incapacitating | Non-Incapacitating | Possible | No Injuries |
|-----------------------|---|-------|----------------|--------------------|----------|-------------|
| First Harmful Event | Curb | 119 | 339 | 788 | 912 | 3,945 |
| | Ditch | 18 | 153 | 427 | 618 | 1,898 |
| | Downhill Runaway | 0 | 0 | 0 | 0 | 0 |
| | Embankment | 20 | 32 | 85 | 96 | 267 |
| | Equipment Failure (blown tire, brake failure, etc.) | 0 | 0 | 0 | 0 | 0 |
| | Fell/Jumped From Motor Vehicle | 23 | 101 | 257 | 98 | 279 |
| | Fence | 29 | 133 | 294 | 530 | 2,723 |
| | Fire/Explosion | 0 | 1 | 8 | 6 | 153 |
| | Guardrail End | 8 | 26 | 101 | 134 | 508 |
| | Guardrail Face | 53 | 210 | 668 | 1,131 | 4,366 |
| | Immersion | 2 | 1 | 5 | 19 | 86 |
| | Impact Attenuator/Crash Cushion | 4 | 31 | 89 | 140 | 441 |
| | Jackknife | 0 | 7 | 26 | 67 | 337 |
| | Mailbox | 12 | 57 | 135 | 274 | 1,760 |
| | Motor Vehicle in Transport | 1,522 | 9,962 | 46,993 | 114,441 | 476,700 |
| | Not Specified | 0 | 0 | 1 | 3 | 99 |
| | Other Fixed Object (wall, building, tunnel, etc.) | 48 | 187 | 731 | 1,094 | 6,090 |
| | Other Non-Collision | 96 | 264 | 760 | 934 | 3,565 |
| | Other Non-Fixed Object | 15 | 84 | 371 | 511 | 4,562 |
| | Other Post, Pole, or Support | 22 | 63 | 285 | 483 | 2,825 |
| Other Traffic Barrier | 5 | 21 | 71 | 124 | 606 | |
| Overturn/Rollover | 165 | 760 | 1,710 | 1,628 | 3,765 | |
| Parked Motor Vehicle | 29 | 196 | 739 | 1,699 | 24,465 | |

Environmental Factors & Injury Levels

Note: The environmental factor titled "Road Contributing Circumstance" can be listed on the crash report with more than one value per crash event. Therefore injury totals may differ from the true count of fatalities and injuries found in the summary on pages 8 & 9.

| | | Fatal | Incapacitating | Non-Incapacitating | Possible | No Injuries |
|----------------------------|--|---------------|----------------|--------------------|----------------|-------------|
| First Harmful Event | Pedalcycle | 140 | 578 | 1,791 | 1,536 | 4,681 |
| | Pedestrian | 663 | 1,134 | 2,678 | 2,330 | 7,650 |
| | Railway Vehicle (train, engine) | 7 | 5 | 9 | 22 | 153 |
| | Ran into Water/ Canal | 10 | 10 | 65 | 85 | 515 |
| | Ran Off Roadway, Left | 0 | 1 | 1 | 0 | 0 |
| | Ran Off Roadway, Right | 0 | 0 | 1 | 1 | 4 |
| | Struck By Falling, Shifting Cargo or Anything Set in Motion by Motor Vehicle | 1 | 9 | 29 | 50 | 1,480 |
| | Separation of Units | 0 | 0 | 0 | 0 | 0 |
| | Thrown or Falling Object | 0 | 2 | 10 | 32 | 350 |
| | Traffic Sign Support | 23 | 99 | 217 | 337 | 1,829 |
| | Traffic Signal Support | 5 | 16 | 40 | 38 | 222 |
| | Tree (standing) | 186 | 598 | 1,455 | 1,734 | 4,419 |
| | Unknown | 0 | 0 | 0 | 0 | 0 |
| | Utility Pole/Light Support | 37 | 229 | 724 | 1,006 | 3,179 |
| | Work Zone/Maintenance Equipment | 10 | 20 | 29 | 40 | 307 |
| Total | 3,332 | 15,614 | 62,738 | 134,080 | 573,649 | |

APPENDIX F: Signal Warrant Analysis Report

Signal Warrant Analysis

Florida Department of Transportation

District One

SR 70 from Lonesome Island Road to CR 721

Limits of Project: From Lonesome Island Road to the Southern Leg of CR 721

Highlands County, Florida

Financial Management Number: 449851-1

ETDM Number: 14490

Date: July 2024

PROFESSIONAL ENGINEER CERTIFICATE

I hereby certify that I am a registered professional engineer in the State of Florida practicing with Kisinger Campo & Associates, and that I have supervised the preparation of, and approved the analysis, findings, opinions, conclusions, and technical advice reported in:

REPORT: Signal Warrant Analysis
PROJECT: SR 70 from Lonesome Island Road to CR 721
LOCATION: Highlands County
FPID NO.: 449851-1
CLIENT: FDOT District One

The following duly authorized engineering business performed the engineering work represented by this report:

Kisinger Campo & Associates, Corp.
201 N. Franklin St., Suite 400
Tampa, FL 33602
Telephone: (813) 871-5331

I, M. Fathy Abdalla, Florida P.E. Number 63914, have prepared this Signal Warrant Analysis for SR 70 at CR 721. This Signal Warrant Analysis contains detailed engineering information that fulfills the purpose and need for this project.

I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of transportation engineering as applied through design standards and criteria set forth by the federal, state, and local regulatory agencies as well as professional judgement and experience.

Name: M. Fathy Abdalla, P.E.

Signature: _____

M. Fathy Abdalla 2024.07.03
13:02:43-04'00'

P.E. Number: 63914

Date: _____

This report has been digitally signed and sealed by M. Fathy Abdalla, P.E. on the date indicated here. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

Executive Summary

The purpose of this study is to evaluate the feasibility of installing a traffic signal at the intersection of the SR 70 and CR 721 in Highlands County, Florida in the Opening Year of 2032 with proposed widening along SR 70 from a two to four lane road. The methodology used in this study is consistent with the FHWA Manual on Uniform Traffic Control Devices (MUTCD) and the FDOT Manual on Uniform Traffic Studies (MUTS).

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Project Description

The purpose of this project is to provide safety and capacity improvements along SR 70. Improvements are recommended based on historic crash data of the corridor, existing evacuation clearance times, and population growth in the project area. SR 70 serves as a major east-west corridor and evacuation route in Highlands County and across the state of Florida. The intersection currently operates under flashing signal control. Figure 1 shows an aerial photograph of the existing conditions, Figure 2 shows the existing typical section, and Figure 3 shows the existing lane configurations.

Figure 1 Existing Intersection Conditions



Figure 2 SR 70 – Existing Typical Section

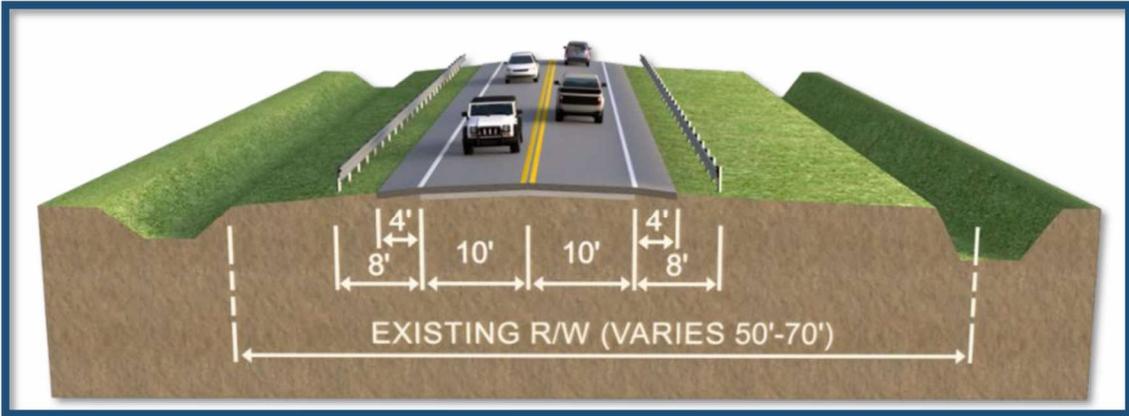
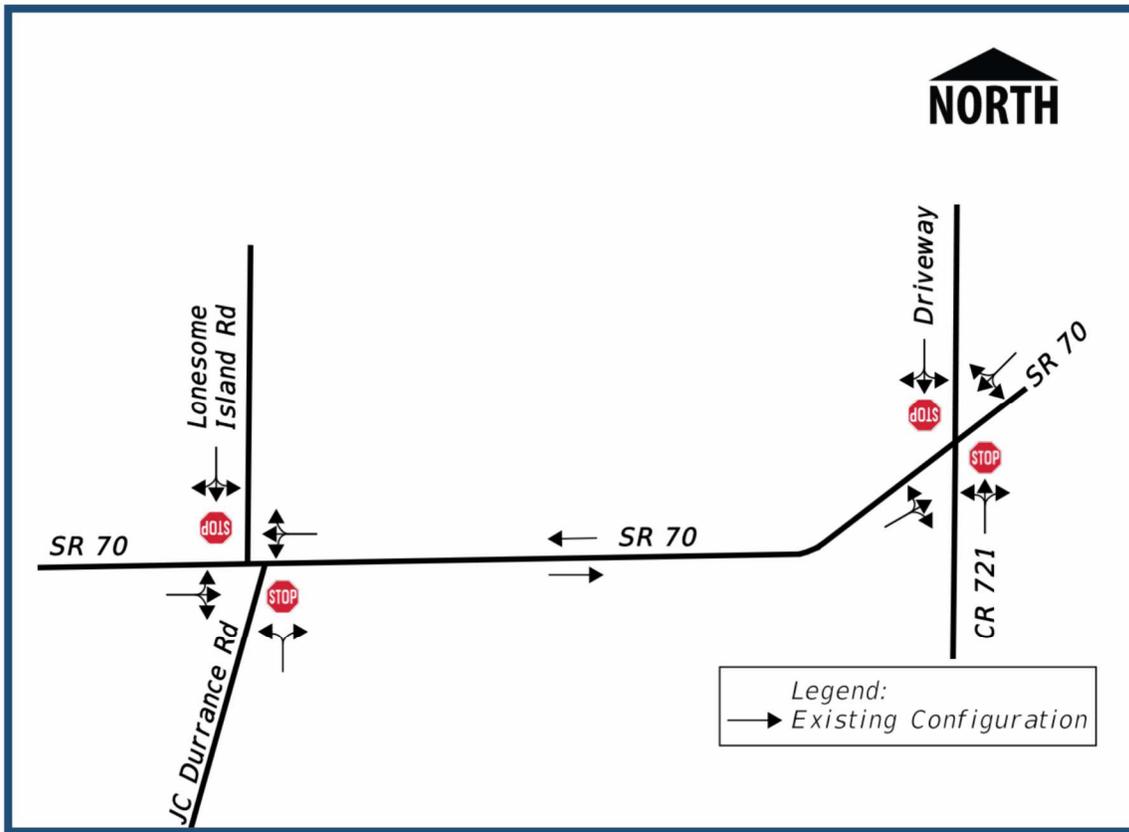


Figure 3 SR 70 – Existing Lane Configurations



Proposed Lane Configuration

The on-going FDOT District One design project along SR 70 (FPID 449851-1) is proposing improvements to the intersection of SR 70 at CR 721. This project is proposing to widen SR 70 from two to four lanes within the intersection of CR 721. The proposed typical section shows widening SR 70 to a four-lane divided rural roadway with a 40-foot median and is depicted in Figure 4. There will be two 12-ft travel lanes in each direction, with outside shoulders that are approximately 10-ft wide (5-ft paved) throughout the corridor. A 12-ft shared use path is proposed along the south side of the road. The proposed ROW varies along the corridor but is a minimum of an additional 60 feet. Figure 5 shows the proposed lane configuration.

Figure 4 SR 70 - Proposed Typical Section

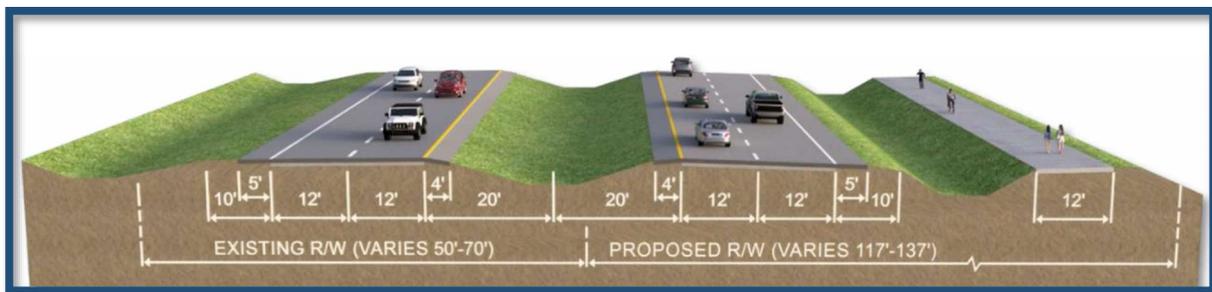
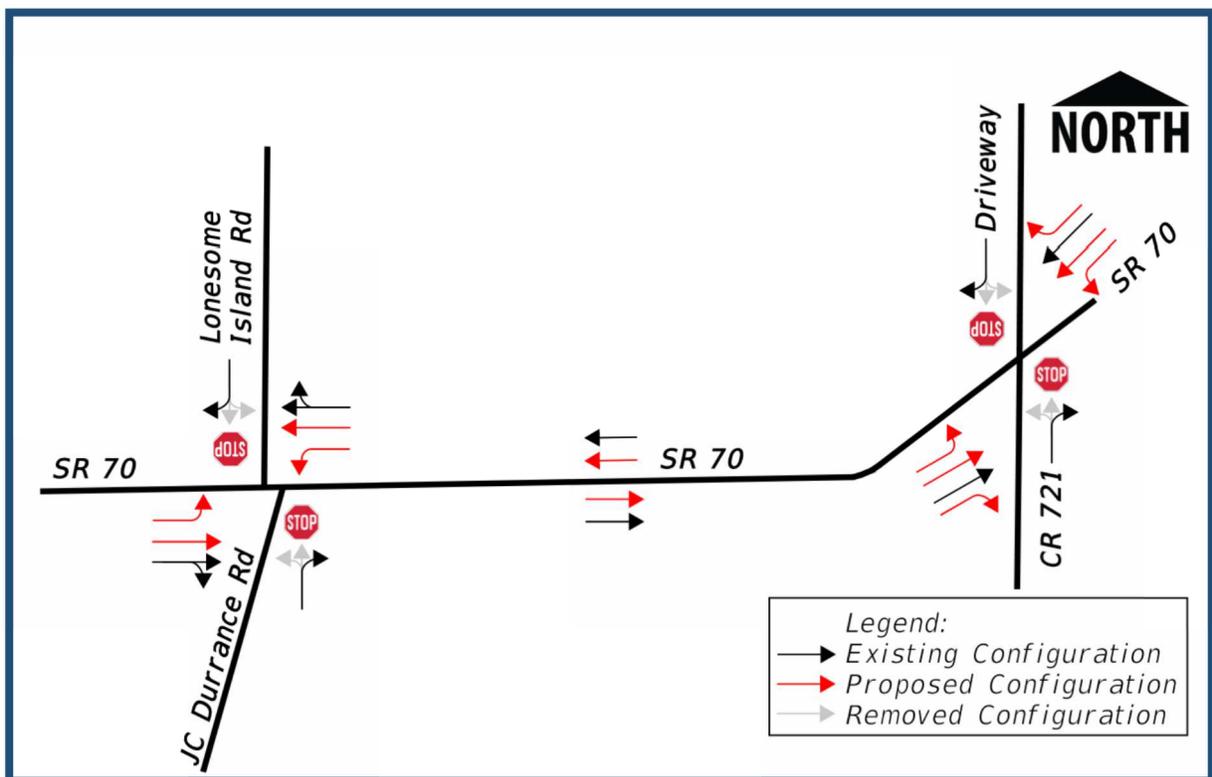


Figure 5 Build Scenario Proposed Lane Geometry



Traffic Data

Twenty-four hour bi-directional volume counts were conducted for all approaches on November 2nd, 2022. The traffic counts were used in conjunction with established growth rates for the intersection location to project traffic during the Opening Year 2032. Right turn traffic on the Minor Street approach was excluded in the traffic projection. Table 1 shows the 2032 Opening Year 8-hour traffic volumes that were developed for the study intersection based on the counts from November 2nd, 2022. For the purposes of this study SR 70 was considered the Major Street and CR 721 was considered the Minor Street.

Table 1 Opening Year 2032 8-Hour Volumes

| Time | 2022 Counts | | | | Growth Rate | 2032 Projection | |
|----------|---------------|---------------------|-------------------|----------------------|-------------|-----------------|-----------|
| | SR 70 EB & WB | CR 721 NB Left Turn | CR 721 NB Through | CR 721 NB Right Turn | | SR 70 EB & WB | CR 721 NB |
| 8:00 AM | 456 | 14 | 0 | 41 | 4% | 675 | 21 |
| 12:00 PM | 373 | 15 | 0 | 43 | | 552 | 23 |
| 1:00 PM | 458 | 18 | 0 | 52 | | 678 | 27 |
| 2:00 PM | 472 | 23 | 1 | 67 | | 699 | 35 |
| 3:00 PM | 631 | 27 | 1 | 78 | | 934 | 41 |
| 4:00 PM | 468 | 30 | 1 | 85 | | 693 | 45 |
| 5:00 PM | 398 | 31 | 1 | 89 | | 589 | 47 |
| 6:00 PM | 304 | 17 | 0 | 49 | | 450 | 26 |

Evaluation of Signal Warranting Conditions

Warrant 1: Eight-Hour Vehicular Volumes

The minimum Vehicular Volume, Condition A, is intended for application where a large volume of intersecting traffic is the principal reason to consider installing a traffic control signal. The Interruption of Continuous Traffic, Condition B, is intended for application where the traffic volume on a major street is so heavy that traffic on a minor intersecting street suffers excessive delay or conflict in entering or crossing the major street. Warrant 1 is met if the requirements for Condition A or Condition B are fulfilled for any eight hours of an average day or if a combination of warrants, 80% of Condition A and 80% of Condition B, is fulfilled for any eight hours of an average day. Figures 6 and 7 show that the 8-hour volumes did not meet any of the requirements for Condition A or B, therefore Warrant 1 is not satisfied.

Conclusion: Warrant 1 has not been met

Figure 6 Table 4C-1 for Warrant 1, Condition A

| Number of Lanes for moving traffic on each approach | | Vehicles per hour on major-street (total of both approaches) | | | Vehicles per hour on minor-street (one direction only) | | |
|---|-----------|--|------------------|------------------|--|------------------|------------------|
| Major | Minor | 100% ^a | 80% ^b | 70% ^c | 100% ^a | 80% ^b | 70% ^c |
| 1 | 1 | 500 | 400 | 350 | 150 | 120 | 105 |
| 2 or more | 1 | 600 | 480 | 420 | 150 | 120 | 105 |
| 2 or more | 2 or more | 600 | 480 | 420 | 200 | 160 | 140 |
| 1 | 2 or more | 500 | 400 | 350 | 200 | 160 | 140 |

^a Basic Minimum hourly volume
^b Used for combination of Conditions A and B after adequate trial of other remedial measures
^c May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

Figure 7 Table 4C-1 for Warrant 1, Condition B

| Number of Lanes for moving traffic on each approach | | Vehicles per hour on major-street (total of both approaches) | | | Vehicles per hour on minor-street (one direction only) | | |
|---|-----------|--|------------------|------------------|--|------------------|------------------|
| Major | Minor | 100% ^a | 80% ^b | 70% ^c | 100% ^a | 80% ^b | 70% ^c |
| 1 | 1 | 750 | 600 | 525 | 75 | 60 | 53 |
| 2 or more | 1 | 900 | 720 | 630 | 75 | 60 | 53 |
| 2 or more | 2 or more | 900 | 720 | 630 | 100 | 80 | 70 |
| 1 | 2 or more | 750 | 600 | 525 | 100 | 80 | 70 |

^a Basic Minimum hourly volume
^b Used for combination of Conditions A and B after adequate trial of other remedial measures
^c May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

Warrant 2: Four-Hour Vehicular Volumes

The Four-Hour Vehicular Volume signal warrant conditions are applied where the volume of intersecting traffic is the principal reason to consider installing a traffic control signal. This warrant has not been met due to low traffic volumes on CR 721.

Conclusion: Warrant 2 has not been met

Warrant 3: Peak Hour Vehicular Volumes

The Peak Hour signal warrant is intended for use at a location where traffic conditions are such that for a minimum of one hour of an average day, the minor street traffic suffers undue delay when entering or crossing the major street. This warrant is intended for use at manufacturing plants, industrial complexes, or high-occupancy vehicle facilities attracting or discharging large numbers of vehicles over a short time. The warrant is not applicable to this intersection per MUTCD Section 4C.04 note 3.

Conclusion: Warrant 3 is Not Applicable

Warrant 4: Pedestrian Volume

This warrant is intended where the major street traffic causes pedestrians to experience excessive delays in crossing the major street. Either the average volume of vehicles per hour (vph) over any 4-hour period or the peak one-hour of an average day can be used to determine if this warrant is met. This warrant is not applicable because there were no observed pedestrians during the study period and pedestrian volumes are not projected to increase at this intersection.

Conclusion: Warrant 4 is Not Applicable

Warrant 5: School Crossing

The School Crossing signal warrant is intended for application where the fact that schoolchildren cross the major street is the principal reason to consider installing a traffic control signal. This warrant does not apply to this intersection since schoolchildren are not anticipated to use this intersection as a school crossing with the proposed conditions.

Conclusion: Warrant 5 is Not Applicable

Warrant 6: Coordinated Signal System

The Coordinated Signal System warrant is intended for applications where installing traffic control signals at intersections, where they would not otherwise be needed, can be justified in order to maintain proper platooning of vehicles. This warrant does not apply because the intersection does not necessitate progressive movement in a coordinated signal system.

Conclusion: Warrant 6 is Not Applicable

Warrant 7: Crash Experience

This warrant is intended where the severity and frequency of crashes are the principal reason for the installation of a signal. This warrant requires five or more crashes of types susceptible to correction by a traffic signal to have occurred within a 12-month period. The intersection of SR 70 and CR 721 has been the site of 19 reported crashes between 2018 and 2022. Among these crashes, rear-ends were the most frequent, accounting for 21% of the total. Rear end crashes often result from road users operating their vehicles carelessly or negligently. There were two fatal crashes reported in the study period. The first fatal crash was reported in 2018 as a “fell/jumped from motor vehicle” crash on CR 721 near the intersection under daylight and dry conditions, the initial cause was reported as running off roadway. This crash cannot be attributed to the roadway characteristics with the available information. The second fatal crash was reported in 2019 as a head on crash on SR 70 near CR 721 under daylight and dry conditions, the initial cause was reported as improper passing. This warrant is not applicable because crashes are not projected for the proposed conditions and therefore cannot be evaluated.

Conclusion: Warrant 7 is Not Applicable

Warrant 8: Roadway Network

This warrant is intended where the installation of a signal would encourage concentrated and organized flow on the roadway network.

Conclusion: Warrant 8 is Not Applicable

Warrant 9: Intersection Near Grade Crossing

There is no grade crossing expected to be within the vicinity of the study.

Conclusion: Warrant 9 is Not Applicable

SWA Summary

This study investigated the warrants for a traffic signal at the intersection of SR 70 and CR 721 based on Opening Year 2032 proposed conditions. The MUTCD requires at least one warrant to be met to consider a new traffic signal. The SWA shows that no warrants were met for the intersection. Table 2 provides a summary of the SWA.

Table 2 SWA Summary

| | Warrant | Not Applicable | Met | Not Met |
|---|------------------------------------|----------------|-----|---------|
| 1 | Eight-Hour Volume | | | X |
| 2 | Four-Hour Volume | | | X |
| 3 | Peak Hour | X | | |
| 4 | Pedestrian Volume | X | | |
| 5 | School Crossing | X | | |
| 6 | Coordinated Signal System | X | | |
| 7 | Crash Experience | X | | |
| 8 | Roadway Network | X | | |
| 9 | Intersection Near a Grade Crossing | X | | |

Recommendation

This study does not recommend the inclusion of signalized alternatives in an Intersection Control Evaluation (ICE) analysis. This intersection does not warrant a signal based on the projected traffic volumes and proposed conditions.

Attachments

Traffic Counts

Crash History

Signal Warrant Analysis Forms

Traffic Counts

CLASS COUNT REPORT

Location: CR 721 (south leg) south of SR 70
 Direction: Northbound
 Start Date: 11/2/2022
 Stop Date: 11/2/2022

City/County: Brighton/Highlands
 Start Time: 00:00
 Stop Time: 24:00

GPS: 27.217675
 -81.094633

| END TIME | VEHICLE CLASS | | | | | | | | | | | | | | Total | |
|---------------------|---------------|-----------|-----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|
| | Cycle | Car | 2A-4T | Bus | 2A-SU | 3A-SU | 4A-SU | 4A-ST | 5A-ST | 6A-ST | 5A-MT | 6A-MT | 7A-MT | None | | Unclass |
| 15 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 30 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 45 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 100 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Hourly Total | 0 | 16 | 4 | 0 | 20 |
| 115 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 130 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 145 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 200 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| Hourly Total | 0 | 5 | 2 | 1 | 0 | 8 |
| 215 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 230 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 245 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 300 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| Hourly Total | 0 | 9 | 6 | 0 | 15 |
| 315 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 330 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 345 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 400 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Hourly Total | 0 | 2 | 3 | 0 | 1 | 0 | 6 |
| 415 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 430 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 445 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 500 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Hourly Total | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 515 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 530 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 |
| 545 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 600 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| Hourly Total | 0 | 3 | 6 | 0 | 2 | 11 |
| 615 | 0 | 3 | 4 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 630 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 645 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 |
| 700 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| Hourly Total | 0 | 7 | 12 | 1 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 25 |
| 715 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 730 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 745 | 0 | 3 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 800 | 0 | 4 | 4 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| Hourly Total | 0 | 16 | 16 | 0 | 3 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 39 |
| 815 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 830 | 0 | 3 | 4 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 10 |

| | | | | | | | | | | | | | | | | |
|---------------------|----------|-----------|-----------|----------|-----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------|
| 845 | 0 | 11 | 8 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 22 |
| 900 | 0 | 5 | 6 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| Hourly Total | 0 | 26 | 21 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 55 |
| 915 | 0 | 2 | 4 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 930 | 0 | 4 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 945 | 1 | 2 | 8 | 0 | 2 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| 1000 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| Hourly Total | 1 | 10 | 21 | 0 | 5 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 40 |
| 1015 | 0 | 4 | 3 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 1030 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 1045 | 0 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 1100 | 0 | 3 | 3 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| Hourly Total | 0 | 16 | 12 | 0 | 3 | 4 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 39 |
| 1115 | 0 | 5 | 7 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 15 |
| 1130 | 0 | 3 | 7 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 1145 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 1200 | 0 | 3 | 1 | 0 | 1 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 9 |
| Hourly Total | 0 | 14 | 19 | 0 | 3 | 2 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 44 |
| 1215 | 0 | 12 | 6 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| 1230 | 0 | 5 | 6 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| 1245 | 0 | 6 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 1300 | 0 | 7 | 4 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| Hourly Total | 0 | 30 | 21 | 0 | 4 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 59 |
| 1315 | 1 | 1 | 7 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 1330 | 0 | 8 | 9 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 20 |
| 1345 | 0 | 9 | 6 | 0 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 |
| 1400 | 1 | 10 | 7 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| Hourly Total | 2 | 28 | 29 | 0 | 6 | 2 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 70 |
| 1415 | 0 | 12 | 12 | 0 | 1 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 28 |
| 1430 | 0 | 9 | 10 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 |
| 1445 | 1 | 11 | 7 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 24 |
| 1500 | 0 | 8 | 7 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 18 |
| Hourly Total | 1 | 40 | 36 | 0 | 6 | 2 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 91 |
| 1515 | 0 | 10 | 7 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| 1530 | 0 | 16 | 10 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 |
| 1545 | 0 | 19 | 8 | 0 | 5 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 36 |
| 1600 | 0 | 9 | 10 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 |
| Hourly Total | 0 | 54 | 35 | 0 | 11 | 2 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 106 |
| 1615 | 0 | 17 | 12 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 31 |
| 1630 | 0 | 25 | 10 | 0 | 2 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 41 |
| 1645 | 0 | 14 | 12 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 |
| 1700 | 0 | 4 | 7 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| Hourly Total | 0 | 60 | 41 | 0 | 11 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 116 |
| 1715 | 0 | 21 | 15 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 |
| 1730 | 0 | 18 | 15 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 |
| 1745 | 0 | 15 | 10 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 |
| 1800 | 0 | 12 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| Hourly Total | 0 | 66 | 47 | 0 | 8 | 0 | 121 |
| 1815 | 0 | 9 | 5 | 0 | 2 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 |
| 1830 | 0 | 6 | 11 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18 |
| 1845 | 0 | 5 | 7 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |

| | | | | | | | | | | | | | | | | |
|---------------------|-------------|--------------|--------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|---------------|
| 1900 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| Hourly Total | 0 | 29 | 25 | 1 | 3 | 2 | 0 | 6 | 0 | 66 |
| 1915 | 0 | 11 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| 1930 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 12 |
| 1945 | 0 | 8 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 2000 | 0 | 6 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| Hourly Total | 0 | 34 | 12 | 0 | 5 | 0 | 1 | 52 |
| 2015 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 2030 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 2045 | 0 | 8 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 2100 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Hourly Total | 0 | 18 | 9 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 28 |
| 2115 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 2130 | 0 | 6 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 2145 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 10 |
| 2200 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| Hourly Total | 0 | 23 | 8 | 0 | 1 | 32 |
| 2215 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 2230 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 2245 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 2300 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Hourly Total | 0 | 10 | 11 | 0 | 21 |
| 2315 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 2330 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 2345 | 0 | 6 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 2400 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Hourly Total | 0 | 14 | 3 | 0 | 1 | 0 | 18 |
| DAILY TOTAL | 4 | 532 | 399 | 3 | 74 | 17 | 0 | 27 | 17 | 0 | 0 | 0 | 0 | 0 | 11 | 1084 |
| Percentages | 0.4% | 49.1% | 36.8% | 0.3% | 6.8% | 1.6% | 0.0% | 2.5% | 1.6% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.0% | 100.0% |

CLASS COUNT REPORT

Location: SR 70 west of CR 721 (south leg)
 Direction: Eastbound
 Start Date: 11/2/2022
 Stop Date: 11/2/2022

City/County: Brighton/Highlands
 Start Time: 00:00
 Stop Time: 24:00

GPS: 27.223264
 -81.098127

| END TIME | VEHICLE CLASS | | | | | | | | | | | | | | Total | |
|---------------------|---------------|-----------|-----------|----------|-----------|----------|----------|----------|-----------|----------|----------|----------|----------|----------|-----------|------------|
| | Cycle | Car | 2A-4T | Bus | 2A-SU | 3A-SU | 4A-SU | 4A-ST | 5A-ST | 6A-ST | 5A-MT | 6A-MT | 7A-MT | None | | Unclass |
| 15 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 30 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 45 | 0 | 1 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 100 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Hourly Total | 0 | 4 | 5 | 0 | 1 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| 115 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 130 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 145 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 200 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| Hourly Total | 0 | 4 | 3 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 215 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 230 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 3 |
| 245 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 3 |
| 300 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Hourly Total | 1 | 1 | 2 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 9 |
| 315 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 330 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 345 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 400 | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Hourly Total | 0 | 3 | 4 | 0 | 3 | 0 | 0 | 1 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 21 |
| 415 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 430 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 445 | 0 | 3 | 3 | 0 | 1 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 500 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Hourly Total | 0 | 9 | 7 | 0 | 3 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 29 |
| 515 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 530 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 545 | 0 | 5 | 6 | 0 | 3 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| 600 | 0 | 9 | 10 | 1 | 4 | 1 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 32 |
| Hourly Total | 0 | 24 | 19 | 1 | 7 | 1 | 0 | 4 | 18 | 1 | 0 | 0 | 0 | 0 | 0 | 75 |
| 615 | 0 | 13 | 7 | 0 | 5 | 1 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 33 |
| 630 | 0 | 13 | 13 | 1 | 4 | 2 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 39 |
| 645 | 0 | 10 | 15 | 0 | 4 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 37 |
| 700 | 0 | 13 | 13 | 0 | 3 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 35 |
| Hourly Total | 0 | 49 | 48 | 1 | 16 | 3 | 0 | 5 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 144 |
| 715 | 0 | 6 | 11 | 0 | 4 | 2 | 0 | 2 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 34 |
| 730 | 0 | 9 | 17 | 0 | 1 | 2 | 0 | 1 | 7 | 1 | 0 | 0 | 0 | 0 | 8 | 46 |
| 745 | 2 | 15 | 9 | 1 | 8 | 3 | 1 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 6 | 51 |
| 800 | 1 | 6 | 12 | 0 | 4 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 27 |
| Hourly Total | 3 | 36 | 49 | 1 | 17 | 8 | 1 | 6 | 22 | 1 | 0 | 0 | 0 | 0 | 14 | 158 |
| 815 | 1 | 9 | 13 | 0 | 6 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 1 | F-16 35 |
| 830 | 0 | 13 | 17 | 0 | 2 | 0 | 0 | 5 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 43 |

| | | | | | | | | | | | | | | | | |
|---------------------|----------|------------|-----------|----------|-----------|----------|----------|-----------|-----------|----------|----------|----------|----------|----------|----------|------------|
| 845 | 0 | 14 | 10 | 1 | 4 | 2 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 38 |
| 900 | 1 | 16 | 16 | 0 | 6 | 1 | 1 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 47 |
| Hourly Total | 2 | 52 | 56 | 1 | 18 | 3 | 1 | 10 | 19 | 0 | 0 | 0 | 0 | 0 | 1 | 163 |
| 915 | 2 | 16 | 16 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 |
| 930 | 1 | 12 | 13 | 0 | 6 | 2 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 38 |
| 945 | 0 | 9 | 6 | 0 | 3 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 1 | 25 |
| 1000 | 0 | 17 | 10 | 1 | 6 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 44 |
| Hourly Total | 3 | 54 | 45 | 1 | 18 | 3 | 0 | 7 | 13 | 0 | 0 | 0 | 0 | 0 | 1 | 145 |
| 1015 | 0 | 15 | 7 | 0 | 4 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 32 |
| 1030 | 0 | 13 | 19 | 0 | 1 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 41 |
| 1045 | 0 | 20 | 7 | 0 | 5 | 0 | 0 | 4 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 40 |
| 1100 | 0 | 18 | 12 | 0 | 3 | 1 | 0 | 8 | 13 | 1 | 0 | 0 | 0 | 0 | 1 | 57 |
| Hourly Total | 0 | 66 | 45 | 0 | 13 | 1 | 0 | 18 | 23 | 2 | 0 | 0 | 0 | 0 | 2 | 170 |
| 1115 | 0 | 23 | 12 | 0 | 4 | 0 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 4 | 52 |
| 1130 | 0 | 15 | 12 | 0 | 1 | 0 | 0 | 1 | 11 | 0 | 0 | 0 | 0 | 0 | 1 | 41 |
| 1145 | 2 | 14 | 10 | 0 | 3 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 39 |
| 1200 | 1 | 18 | 7 | 0 | 2 | 1 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 33 |
| Hourly Total | 3 | 70 | 41 | 0 | 10 | 5 | 0 | 4 | 23 | 2 | 0 | 0 | 0 | 0 | 7 | 165 |
| 1215 | 0 | 11 | 7 | 1 | 1 | 0 | 0 | 6 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 35 |
| 1230 | 0 | 15 | 7 | 0 | 1 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 0 | 1 | 32 |
| 1245 | 0 | 9 | 7 | 1 | 8 | 0 | 1 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 1 | 35 |
| 1300 | 0 | 12 | 7 | 0 | 6 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 31 |
| Hourly Total | 0 | 47 | 28 | 2 | 16 | 0 | 1 | 13 | 24 | 0 | 0 | 0 | 0 | 0 | 2 | 133 |
| 1315 | 0 | 14 | 9 | 0 | 2 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 30 |
| 1330 | 0 | 28 | 16 | 1 | 3 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 53 |
| 1345 | 0 | 22 | 10 | 0 | 1 | 1 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 44 |
| 1400 | 0 | 18 | 8 | 0 | 2 | 0 | 0 | 7 | 6 | 0 | 0 | 0 | 0 | 0 | 1 | 42 |
| Hourly Total | 0 | 82 | 43 | 1 | 8 | 1 | 0 | 13 | 20 | 0 | 0 | 0 | 0 | 0 | 1 | 169 |
| 1415 | 0 | 32 | 11 | 0 | 6 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 0 | 1 | 60 |
| 1430 | 0 | 16 | 10 | 0 | 2 | 1 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 35 |
| 1445 | 0 | 29 | 25 | 0 | 6 | 0 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 67 |
| 1500 | 0 | 38 | 17 | 2 | 2 | 2 | 0 | 1 | 9 | 0 | 0 | 0 | 0 | 0 | 2 | 73 |
| Hourly Total | 0 | 115 | 63 | 2 | 16 | 3 | 0 | 8 | 24 | 0 | 0 | 0 | 0 | 0 | 4 | 235 |
| 1515 | 2 | 51 | 25 | 0 | 2 | 3 | 0 | 1 | 9 | 0 | 0 | 0 | 0 | 0 | 1 | 94 |
| 1530 | 0 | 27 | 18 | 1 | 5 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 55 |
| 1545 | 0 | 53 | 24 | 1 | 5 | 1 | 1 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 92 |
| 1600 | 0 | 39 | 17 | 0 | 7 | 0 | 0 | 8 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 78 |
| Hourly Total | 2 | 170 | 84 | 2 | 19 | 4 | 1 | 14 | 22 | 0 | 0 | 0 | 0 | 0 | 1 | 319 |
| 1615 | 0 | 28 | 17 | 2 | 10 | 0 | 0 | 3 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 66 |
| 1630 | 0 | 29 | 29 | 1 | 5 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 71 |
| 1645 | 0 | 14 | 16 | 0 | 4 | 0 | 1 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 4 | 48 |
| 1700 | 0 | 16 | 15 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 35 |
| Hourly Total | 0 | 87 | 77 | 3 | 20 | 0 | 1 | 7 | 20 | 1 | 0 | 0 | 0 | 0 | 4 | 220 |
| 1715 | 0 | 10 | 17 | 0 | 8 | 0 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 1 | 45 |
| 1730 | 0 | 18 | 18 | 0 | 4 | 3 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 45 |
| 1745 | 0 | 16 | 17 | 0 | 3 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 40 |
| 1800 | 0 | 15 | 15 | 0 | 2 | 0 | 0 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 40 |
| Hourly Total | 0 | 59 | 67 | 0 | 17 | 4 | 0 | 9 | 12 | 0 | 0 | 0 | 0 | 0 | 2 | 170 |
| 1815 | 2 | 12 | 7 | 0 | 6 | 4 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 34 |
| 1830 | 1 | 9 | 11 | 0 | 7 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 30 |
| 1845 | 1 | 15 | 10 | 0 | 6 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 |

| | | | | | | | | | | | | | | | | |
|---------------------|-------------|--------------|--------------|-------------|-------------|-------------|-------------|-------------|--------------|-------------|-------------|-------------|-------------|-------------|-------------|---------------|
| 1900 | 0 | 8 | 9 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| Hourly Total | 4 | 44 | 37 | 0 | 20 | 7 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 119 |
| 1915 | 0 | 9 | 10 | 0 | 4 | 3 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 32 |
| 1930 | 0 | 11 | 7 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 26 |
| 1945 | 0 | 11 | 7 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 22 |
| 2000 | 0 | 13 | 5 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 23 |
| Hourly Total | 0 | 44 | 29 | 2 | 6 | 3 | 0 | 5 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 103 |
| 2015 | 0 | 17 | 6 | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 |
| 2030 | 0 | 8 | 12 | 0 | 2 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| 2045 | 0 | 5 | 6 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14 |
| 2100 | 0 | 7 | 2 | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| Hourly Total | 0 | 37 | 26 | 0 | 11 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 81 |
| 2115 | 0 | 3 | 6 | 0 | 3 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| 2130 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 2145 | 0 | 4 | 4 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 13 |
| 2200 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| Hourly Total | 0 | 14 | 14 | 0 | 4 | 0 | 0 | 4 | 8 | 0 | 0 | 1 | 0 | 0 | 0 | 45 |
| 2215 | 0 | 2 | 6 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 2230 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 2245 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 2300 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Hourly Total | 0 | 13 | 12 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 29 |
| 2315 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 2330 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 2345 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 2400 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Hourly Total | 0 | 9 | 0 | 0 | 1 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| DAILY TOTAL | 18 | 1093 | 804 | 17 | 247 | 46 | 5 | 137 | 325 | 7 | 0 | 3 | 0 | 0 | 41 | 2743 |
| Percentages | 0.7% | 39.8% | 29.3% | 0.6% | 9.0% | 1.7% | 0.2% | 5.0% | 11.8% | 0.3% | 0.0% | 0.1% | 0.0% | 0.0% | 1.5% | 100.0% |

Volume Count Report

Start Date: November 2, 2022
 Stop Date: November 3, 2022
 City: Brighton
 Location: SR 70 east of CR 721 (south leg)

Start Time: 0:00
 Stop Time: 0:00
 County: Highlands

GPS: 27.228944
 -81.089467

Eastbound Volume

Wednesday, November 2, 2022

| End Time | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 | 08 | 09 | 10 | 11 |
|-----------------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|------------|------------|------------|------------|
| 15 | 7 | 2 | 3 | 6 | 7 | 11 | 54 | 55 | 47 | 44 | 40 | 71 |
| 30 | 13 | 6 | 9 | 13 | 6 | 15 | 40 | 41 | 60 | 46 | 55 | 62 |
| 45 | 12 | 3 | 10 | 6 | 15 | 39 | 52 | 67 | 62 | 50 | 56 | 44 |
| 00 | 2 | 6 | 8 | 11 | 11 | 41 | 40 | 36 | 54 | 56 | 91 | 43 |
| Hr Total | 34 | 17 | 30 | 36 | 39 | 106 | 186 | 199 | 223 | 196 | 242 | 220 |

| End Time | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
|-----------------|------------|------------|------------|------------|------------|------------|------------|------------|-----------|-----------|-----------|-----------|
| 15 | 68 | 41 | 93 | 60 | 84 | 82 | 71 | 44 | 25 | 16 | 20 | 8 |
| 30 | 47 | 67 | 61 | 57 | 91 | 68 | 51 | 41 | 24 | 16 | 9 | 8 |
| 45 | 45 | 68 | 86 | 76 | 75 | 56 | 50 | 34 | 16 | 27 | 6 | 8 |
| 00 | 49 | 57 | 58 | 80 | 92 | 58 | 44 | 24 | 21 | 15 | 9 | 6 |
| Hr Total | 209 | 233 | 298 | 273 | 342 | 264 | 216 | 143 | 86 | 74 | 44 | 30 |

24 Hour Total: 3,740
 AM Peak Hour begins: 10:30
 PM Peak Hour begins: 16:00
 AM Peak Volume: 280
 PM Peak Volume: 342
 AM Peak Hour Factor: 0.77
 PM Peak Hour Factor: 0.93

Westbound Volume

Wednesday, November 2, 2022

| End Time | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 | 08 | 09 | 10 | 11 |
|-----------------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|------------|------------|------------|------------|
| 15 | 13 | 1 | 3 | 2 | 4 | 20 | 48 | 57 | 68 | 65 | 67 | 63 |
| 30 | 6 | 4 | 4 | 7 | 9 | 36 | 66 | 68 | 97 | 55 | 68 | 77 |
| 45 | 8 | 10 | 0 | 6 | 18 | 42 | 67 | 88 | 71 | 62 | 49 | 74 |
| 00 | 1 | 0 | 12 | 8 | 12 | 40 | 70 | 74 | 57 | 60 | 58 | 56 |
| Hr Total | 28 | 15 | 19 | 23 | 43 | 138 | 251 | 287 | 293 | 242 | 242 | 270 |

| End Time | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
|-----------------|------------|------------|------------|------------|------------|------------|------------|------------|-----------|-----------|-----------|-----------|
| 15 | 69 | 68 | 67 | 88 | 70 | 48 | 60 | 22 | 26 | 19 | 9 | 11 |
| 30 | 43 | 68 | 54 | 81 | 71 | 64 | 40 | 33 | 23 | 20 | 13 | 5 |
| 45 | 60 | 75 | 68 | 63 | 64 | 72 | 52 | 28 | 27 | 20 | 9 | 3 |
| 00 | 68 | 78 | 48 | 80 | 43 | 44 | 33 | 34 | 17 | 14 | 7 | 7 |
| Hr Total | 240 | 289 | 237 | 312 | 248 | 228 | 185 | 117 | 93 | 73 | 38 | 26 |

24 Hour Total: 3,937
 AM Peak Hour begins: 7:30
 PM Peak Hour begins: 15:00
 AM Peak Volume: 327
 PM Peak Volume: 312
 AM Peak Hour Factor: 0.84
 PM Peak Hour Factor: 0.89

Total Volume

Wednesday, November 2, 2022

| End Time | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 | 08 | 09 | 10 | 11 |
|-----------------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|------------|------------|------------|------------|
| 15 | 20 | 3 | 6 | 8 | 11 | 31 | 102 | 112 | 115 | 109 | 107 | 134 |
| 30 | 19 | 10 | 13 | 20 | 15 | 51 | 106 | 109 | 157 | 101 | 123 | 139 |
| 45 | 20 | 13 | 10 | 12 | 33 | 81 | 119 | 155 | 133 | 112 | 105 | 118 |
| 00 | 3 | 6 | 20 | 19 | 23 | 81 | 110 | 110 | 111 | 116 | 149 | 99 |
| Hr Total | 62 | 32 | 49 | 59 | 82 | 244 | 437 | 486 | 516 | 438 | 484 | 490 |

| End Time | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
|-----------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|-----------|-----------|
| 15 | 137 | 109 | 160 | 148 | 154 | 130 | 131 | 66 | 51 | 35 | 29 | 19 |
| 30 | 90 | 135 | 115 | 138 | 162 | 132 | 91 | 74 | 47 | 36 | 22 | 13 |
| 45 | 105 | 143 | 154 | 139 | 139 | 128 | 102 | 62 | 43 | 47 | 15 | 11 |
| 00 | 117 | 135 | 106 | 160 | 135 | 102 | 77 | 58 | 38 | 29 | 16 | 13 |
| Hr Total | 449 | 522 | 535 | 585 | 590 | 492 | 401 | 260 | 179 | 147 | 82 | 56 |

24 Hour Total: 7,677
 AM Peak Hour begins: 10:45
 PM Peak Hour begins: 15:30
 AM Peak Volume: 540
 PM Peak Volume: 615
 AM Peak Hour Factor: 0.91
 PM Peak Hour Factor: 0.95

Signal Warrant Analysis Forms

TRAFFIC SIGNAL WARRANT SUMMARY

Introduction

- The Signal Warrant Analysis Spreadsheets are a tool for assisting traffic engineers when evaluating the need for a traffic signal installation
 - The filled spreadsheets can be used as part of the supporting documents for the signal warrant evaluation
- Note: This templates are a useful resource, but it remains necessary to apply engineering judgment and to consider specific environmental, traffic, geometric, and operational conditions

Instructions

Fill in "Orange" areas only

Automated cells based on in Input Data in "orange" cells

General Information

Fill in below the general information including:

District, County (drop-down menu)

City, Engineer, Date

Major and Minor Street with corresponding number of lanes and speed limits

Enter Eight Hour Volumes

Any 8 hours of an average day. Major-street and minor-street volumes shall be for the same 8 hours; however, the 8 hours satisfied in Condition A shall **not** be required to be the same 8 hours satisfied in Condition B **for 80% columns only**. On the minor street, the higher volume shall not be required to be on the same approach during each of the 8 hours.

Enter Four Hour Volumes

Any 4 hours of an average day. Vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor-street approach (one direction only, not required to be on the same approach during each of the 4 hours)

Enter Pedestrian Volumes (4-h)

Pedestrians per hour crossing the major street (total of all crossings)

Enter Peak Hour Volumes

Vehicular: Any four consecutive 15-minute periods of an average day

Pedestrian: Any four consecutive 15-minute periods of an average day representing the vehicles per hour on the major street (total of both approaches) and the corresponding pedestrians per hour crossing the major street (total of all crossings)

Input Data

City: **Brighton**
 County: **09 – Highlands**
 District: **One**

Engineer: **KCA**
 Date: **OPENING YEAR 2032**

Major Street: **SR 70** Major Street # Lanes: **2** Major Approach Speed: **60**
 Minor Street: **CR 721** Minor Street # Lanes: **1** Minor Approach Speed: **45**

| Eight Hour Volumes (Condition A) | | | For Warrant 7 |
|----------------------------------|--|--------------------------------------|----------------------------------|
| Hours | Major Street (total of both approaches) | Minor Street (one direction only) | Ped Crossings on Major Street |
| 8:00 AM | 675 | 21 | |
| 12:00 PM | 552 | 23 | |
| 1:00 PM | 678 | 27 | |
| 2:00 PM | 699 | 35 | |
| 3:00 PM | 934 | 41 | |
| 4:00 PM | 693 | 45 | |
| 5:00 PM | 589 | 47 | |
| 6:00 PM | 450 | 26 | |

| Eight Hour Volumes (Condition B) | | |
|----------------------------------|--|--------------------------------------|
| Hours | Major Street (total of both approaches) | Minor Street (one direction only) |
| 8:00 AM | 675 | 21 |
| 12:00 PM | 552 | 23 |
| 1:00 PM | 678 | 27 |
| 2:00 PM | 699 | 35 |
| 3:00 PM | 934 | 41 |
| 4:00 PM | 693 | 45 |
| 5:00 PM | 589 | 47 |
| 6:00 PM | 450 | 26 |

| Highest Four Hour Vehicular Volumes | | |
|-------------------------------------|--|--------------------------------------|
| Hours | Major Street (total of both approaches) | Minor Street (one direction only) |
| 2:00 PM | 699 | 35 |
| 3:00 PM | 934 | 41 |
| 4:00 PM | 693 | 45 |
| 5:00 PM | 589 | 47 |

| Highest Four Hour Pedestrian Volumes | | |
|--------------------------------------|--|--|
| Hours | Major Street (total of both approaches) | Pedestrian Crossings on Major Street |
| | | |
| | | |
| | | |
| | | |

| Vehicular Peak Hour Volumes | | | |
|-----------------------------|--|--------------------------------------|--------------------------|
| Peak Hour | Major Street (total of both approaches) | Minor Street (one direction only) | Total Entering Volume |
| 5:00 PM | 589 | 47 | 636 |

| Pedestrian Peak Hour Volumes | | |
|------------------------------|--|---|
| Peak Hour | Major Street (total of both approaches) | Pedestrian Crossing Volumes on Major Street |
| | | |
| | | |
| | | |

TRAFFIC SIGNAL WARRANT SUMMARY

City: Brighton
County: 09 – Highlands
District: One

Engineer: KCA
Date: OPENING YEAR 2032

Major Street: SR 70 Lanes: 2 Major Approach Speed: 60
Minor Street: CR 721 Lanes: 1 Minor Approach Speed: 45

MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf>

Volume Level Criteria

1. Is the posted speed or 85th-percentile of major street > 40 mph? Yes No
2. Is the intersection in a built-up area of an isolated community with a population < 10,000? Yes No
- "70%" volume level **may** be used if Question 1 **or** 2 above is answered "Yes" MAY 70% 100%

WARRANT 1 - EIGHT-HOUR VEHICULAR VOLUME

Warrant 1 is satisfied if Condition A **or** Condition B is "100%" satisfied for eight hours. Yes No

Warrant 1 is also satisfied if both Condition A **and** Condition B are "80%" satisfied (should only be applied after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems). Yes No

Warrant 1 is satisfied if Condition A **or** Condition B is "70%" satisfied for eight hours. Yes No

Condition A - Minimum Vehicular Volume

Condition A is intended for application at locations where a large volume of intersecting traffic is the principal reason to consider installing a traffic control signal.

- Applicable: Yes No
100% Satisfied: Yes No
80% Satisfied: Yes No
70% Satisfied: Yes No

| Number of Lanes for moving traffic on each approach | | Vehicles per hour on major-street (total of both approaches) | | | Vehicles per hour on minor-street (one direction only) | | |
|---|-----------|--|------------------|------------------|--|------------------|------------------|
| Major | Minor | 100% ^a | 80% ^b | 70% ^c | 100% ^a | 80% ^b | 70% ^c |
| 1 | 1 | 500 | 400 | 350 | 150 | 120 | 105 |
| 2 or more | 1 | 600 | 480 | 420 | 150 | 120 | 105 |
| 2 or more | 2 or more | 600 | 480 | 420 | 200 | 160 | 140 |
| 1 | 2 or more | 500 | 400 | 350 | 200 | 160 | 140 |

^a Basic Minimum hourly volume

^b Used for combination of Conditions A and B after adequate trial of other remedial measures

^c May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

Record 8 highest hours and the corresponding major-street and minor-street volumes in the Instructions Sheet.

| Street | Eight Highest Hours | | | | | | | |
|--------|---------------------|----------|---------|---------|---------|---------|---------|---------|
| | 8:00 AM | 12:00 PM | 1:00 PM | 2:00 PM | 3:00 PM | 4:00 PM | 5:00 PM | 6:00 PM |
| Major | 675 | 552 | 678 | 699 | 934 | 693 | 589 | 450 |
| Minor | 21 | 23 | 27 | 35 | 41 | 45 | 47 | 26 |

Existing Volumes

State of Florida Department of Transportation
TRAFFIC SIGNAL WARRANT SUMMARY

Condition B - Interruption of Continuous Traffic

Condition B is intended for application where Condition A is not satisfied and the traffic volume on a major street is so heavy that traffic on the minor intersecting street suffers excessive delay or conflict in entering or crossing the major street.

| | | |
|-----------------|---|--|
| Applicable: | <input checked="" type="checkbox"/> Yes | <input type="checkbox"/> No |
| 100% Satisfied: | <input type="checkbox"/> Yes | <input checked="" type="checkbox"/> No |
| 80% Satisfied: | <input type="checkbox"/> Yes | <input checked="" type="checkbox"/> No |
| 70% Satisfied: | <input type="checkbox"/> Yes | <input checked="" type="checkbox"/> No |

| Number of Lanes for moving traffic on each approach | | Vehicles per hour on major-street (total of both approaches) | | | Vehicles per hour on minor-street (one direction only) | | |
|---|-----------|--|------------------|------------------|--|------------------|------------------|
| | | 100% ^a | 80% ^b | 70% ^c | 100% ^a | 80% ^b | 70% ^c |
| Major | Minor | | | | | | |
| 1 | 1 | 750 | 600 | 525 | 75 | 60 | 53 |
| 2 or more | 1 | 900 | 720 | 630 | 75 | 60 | 53 |
| 2 or more | 2 or more | 900 | 720 | 630 | 100 | 80 | 70 |
| 1 | 2 or more | 750 | 600 | 525 | 100 | 80 | 70 |

^a Basic Minimum hourly volume

^b Used for combination of Conditions A and B after adequate trial of other remedial measures

^c May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

Record 8 highest hours and the corresponding major-street and minor-street volumes in the Instructions Sheet.

| Eight Highest Hours | | | | | | | | |
|---------------------|---------|----------|---------|---------|---------|---------|---------|---------|
| Street | 8:00 AM | 12:00 PM | 1:00 PM | 2:00 PM | 3:00 PM | 4:00 PM | 5:00 PM | 6:00 PM |
| Major | 675 | 552 | 678 | 699 | 934 | 693 | 589 | 450 |
| Minor | 21 | 23 | 27 | 35 | 41 | 45 | 47 | 26 |

Existing Volumes

TRAFFIC SIGNAL WARRANT SUMMARY

City: **Brighton**
County: **09 – Highlands**
District: **One**

Engineer: **KCA**
Date: **OPENING YEAR 2032**

Major Street: **SR 70** Lanes: **2** Major Approach Speed: **60**
Minor Street: **CR 721** Lanes: **1** Minor Approach Speed: **45**

MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf>

Volume Level Criteria

- Is the posted speed or 85th-percentile of major street > 40 mph? Yes No
 - Is the intersection in a built-up area of an isolated community with a population < 10,000? Yes No
- "70%" volume level **may** be used if Question 1 **or** 2 above is answered "Yes" MAY 70% 100%

WARRANT 2 - FOUR-HOUR VEHICULAR VOLUME

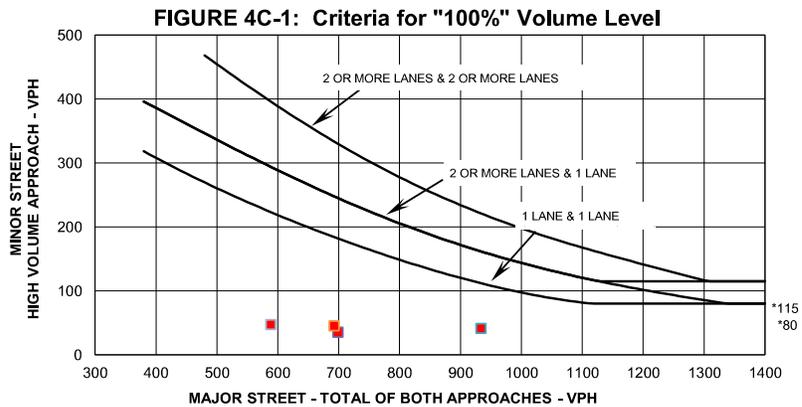
If all four points lie above the applicable line, then the warrant is satisfied.

Applicable: Yes No
Satisfied: Yes No

Plot four volume combinations on the applicable figure below.

100% Volume Level

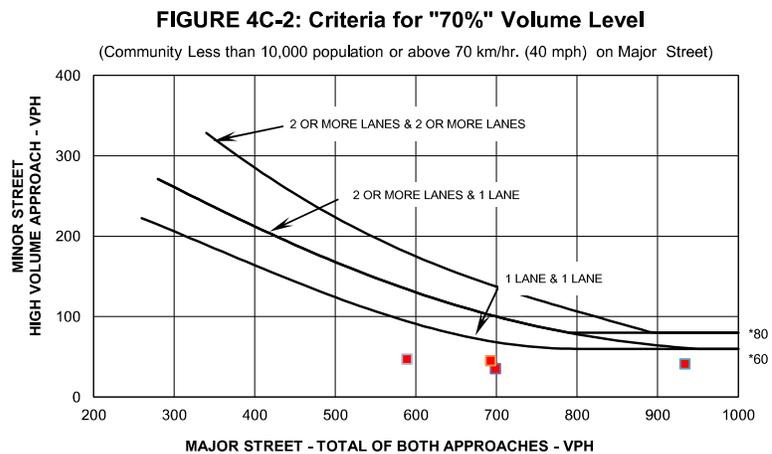
| Four Highest Hours | Volumes | |
|--------------------|--------------|--------------|
| | Major Street | Minor Street |
| 2:00 PM | 699 | 35 |
| 3:00 PM | 934 | 41 |
| 4:00 PM | 693 | 45 |
| 5:00 PM | 589 | 47 |



* Note: 115 ph. applies as the lower threshold volume for a minor street approach with two or more lanes and 80 mph applies as the lower threshold volume threshold for a minor street approach with one lane.

70% Volume Level

| Four Highest Hours | Volumes | |
|--------------------|--------------|--------------|
| | Major Street | Minor Street |
| 2:00 PM | 699 | 35 |
| 3:00 PM | 934 | 41 |
| 4:00 PM | 693 | 45 |
| 5:00 PM | 589 | 47 |



* Note: 80 ph. applies as the lower threshold volume for a minor street approach with two or more lanes and 60 ph. applies as the lower threshold volume threshold for a minor street approach with one lane.

TRAFFIC SIGNAL WARRANT SUMMARY

City: **Brighton**
County: **09 – Highlands**
District: **One**

Engineer: **KCA**
Date: **OPENING YEAR 2032**

Major Street: **SR 70**
Minor Street: **CR 721**

Lanes: **2** Major Approach Speed: **60**
Lanes: **1** Minor Approach Speed: **45**

MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf>

Volume Level Criteria

- Is the posted speed or 85th-percentile of major street > 40 mph? Yes No
 - Is the intersection in a built-up area of an isolated community with a population < 10,000? Yes No
- "70%" volume level **may** be used if Question 1 **or** 2 above is answered "Yes" MAY 70% 100%

WARRANT 3 - PEAK HOUR

If all three criteria are fulfilled **or** the plotted point lies above the appropriate line, then the warrant is satisfied.

Applicable: Yes No
Satisfied: Yes No

Unusual condition justifying use of warrant:

-

Record hour when criteria are fulfilled and the corresponding delay or volume in boxes provided.

| Peak Hour 100% Volume | | |
|-----------------------|------------|------------|
| Time | Major Vol. | Minor Vol. |
| 5:00 PM | 589 | 47 |

| Peak Hour 70% Volume | | |
|----------------------|------------|------------|
| Time | Major Vol. | Minor Vol. |
| 5:00 PM | 589 | 47 |

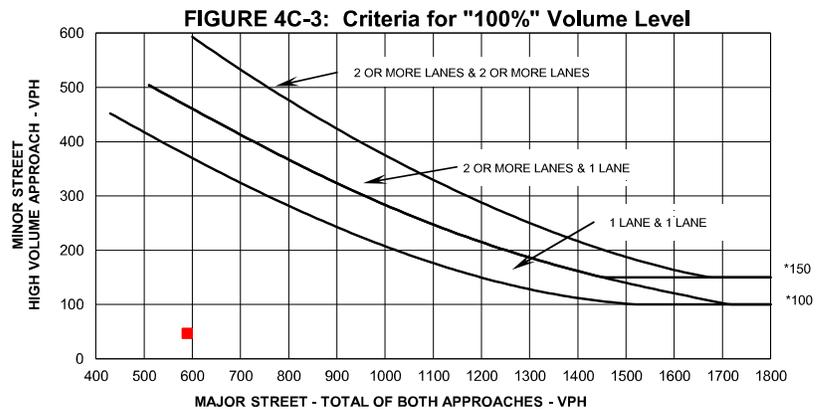
Criteria

| 1. Delay on Minor Approach *(vehicle-hours) | | |
|--|------------------------------|-----------------------------|
| Approach Lanes | 1 | 2 |
| Delay Criteria* | 4.0 | 5.0 |
| Delay* | | |
| Fulfilled?: | <input type="checkbox"/> Yes | <input type="checkbox"/> No |

| 2. Volume on Minor Approach One-Direction *(vehicles per hour) | | |
|---|------------------------------|-----------------------------|
| Approach Lanes | 1 | 2 |
| Volume Criteria* | 100 | 150 |
| Volume* | | |
| Fulfilled?: | <input type="checkbox"/> Yes | <input type="checkbox"/> No |

| 3. Total Intersection Entering Volume *(vehicles per hour) | | |
|---|------------------------------|-----------------------------|
| No. of Approaches | 3 | 4 |
| Volume Criteria* | 650 | 800 |
| Volume* | | |
| Fulfilled?: | <input type="checkbox"/> Yes | <input type="checkbox"/> No |

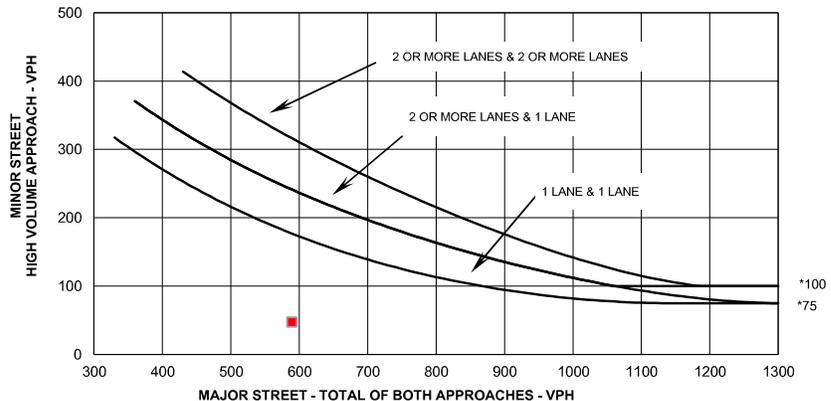
Plot volume combination on the applicable figure below.



* Note: 150 vph applies as the lower threshold volume for a minor street approach with two or more lanes and 100 vph applies as the lower threshold volume threshold for a minor street approach with one lane.

FIGURE 4C-4: Criteria for "70%" Volume Level

(Community Less than 10,000 population or above 70 km/hr. (40 mph) on Major Street)



* Note: 100 ph. applies as the lower threshold volume for a minor street approach with two or more lanes and 75 phi applies as the lower threshold volume threshold for a minor street approach with one lane.

TRAFFIC SIGNAL WARRANT SUMMARY

City: **Brighton**
County: **09 – Highlands**
District: **One**

Engineer: **KCA**
Date: **OPENING YEAR 2032**

Major Street: **SR 70** Lanes: **2** Major Approach Speed: **60**
Minor Street: **CR 721** Lanes: **1** Minor Approach Speed: **45**

MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pc>

Volume Level Criteria

- Is the posted speed or 85th-percentile of major street > 35 mph? Yes No
 - Is the intersection in a built-up area of an isolated community with a population < 10,000? Yes No
- "70%" volume level **may** be used if Question 1 **or** 2 above is answered "Yes" MAY 70% 100%

Option

Pedestrian volume crossing the major street **may** be reduced as much as 50% if the 15th-percentile crossing speed of pedestrians is less than 3.5 ft/sec. A walking speed study was conducted which reported a pedestrian speed less than 3.5 ft/sec for the 15th percentile. Yes No

WARRANT 4 - PEDESTRIAN VOLUME

For each of any 4 hours of an average day, the plotted points lie above the appropriate line, then the warrant is satisfied.
Applicable: Yes No
Satisfied: Yes No

100% Volume Level

| Four Highest Hours | Volumes | |
|--------------------|--------------|------------------|
| | Major Street | Pedestrian Total |
| | | |
| | | |
| | | |
| | | |

Plot four volume combinations on the applicable figure below.

Figure 4C-5. Criteria for "100%" Volume Level

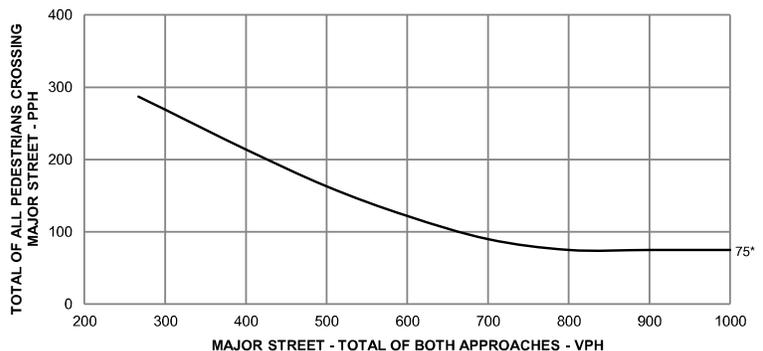


* Note: 107 pph applies as the lower threshold volume for 100% volume level

70% Volume Level

| Four Highest Hours | Volumes | |
|--------------------|--------------|------------------|
| | Major Street | Pedestrian Total |
| | | |
| | | |
| | | |
| | | |

Figure 4C-6 Criteria for "70%" Volume Level



* Note: 75 pph applies as the lower threshold volume for 70% volume level

WARRANT 4 - PEDESTRIAN VOLUME

For 1 hour (any four consecutive 15-minute periods) of an average day, the plotted point falls above the appropriate line, then the warrant is satisfied.

Applicable: Yes No
 Satisfied: Yes No

Plot one volume combination on the applicable figure below.

100% Volume Level

| Peak Hour | Volumes | |
|-----------|--------------|------------------|
| | Major Street | Pedestrian Total |
| | | |

Figure 4C-7. Criteria for "100%" Volume Level - Peak Hour

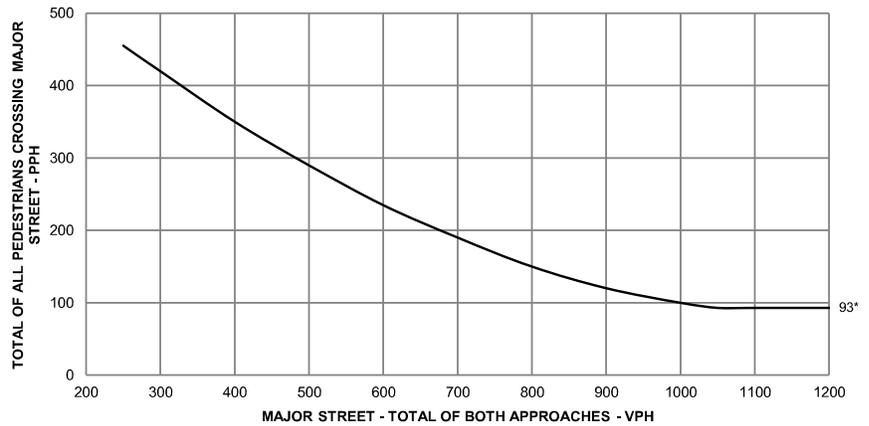


* Note: 133 pph applies as the lower threshold volume

70% Volume Level

| Peak Hour | Volumes | |
|-----------|--------------|------------------|
| | Major Street | Pedestrian Total |
| | | |

Figure 4C-8 Criteria for "70%" Volume Level - Peak Hour



* Note: 93 pph applies as the lower threshold volume

TRAFFIC SIGNAL WARRANT SUMMARY

City: **Brighton**
 County: **09 – Highlands**
 District: **One**

Engineer: **KCA**
 Date: **OPENING YEAR 2032**

Major Street: **SR 70** Lanes: **2** Major Approach Speed: **60**
 Minor Street: **CR 721** Lanes: **1** Minor Approach Speed: **45**

MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf>

WARRANT 5 - SCHOOL CROSSING

Record hours where criteria are fulfilled and the corresponding volume or gap frequency in the boxes provided. The warrant is satisfied if all three of the criteria are fulfilled.

Applicable: Yes No
 Satisfied: Yes No

| Criteria | | | | Fulfilled? | |
|----------|---|-----------|-------|------------|----|
| | | | | Yes | No |
| 1. | There are a minimum of 20 students crossing the major street during the highest crossing hour. | Students: | Hour: | | |
| | | | | | |
| 2. | There are fewer adequate gaps in the major street traffic stream during the period when the children are using the established school crossing than the number of minutes in the same period. | Minutes: | Gaps: | | |
| | | | | | |
| 3. | The nearest traffic signal along the major street is located more than 300 ft. (90 m) away, or the nearest signal is within 300 ft. (90 m) but the proposed traffic signal will not restrict the progressive movement of traffic. | | | | |

TRAFFIC SIGNAL WARRANT SUMMARY

City: **Brighton**
 County: **09 – Highlands**
 District: **One**

Engineer: **KCA**
 Date: **OPENING YEAR 2032**

Major Street: **SR 70** Lanes: **2** Major Approach Speed: **60**
 Minor Street: **CR 721** Lanes: **1** Minor Approach Speed: **45**

MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf>

WARRANT 6 - COORDINATED SIGNAL SYSTEM

Indicate if the criteria are fulfilled in the boxes provided. The warrant is satisfied if either criterion is fulfilled. This warrant should not be applied when the resulting signal spacing would be less than 300 m (1,000 ft.).

Applicable: Yes No
 Satisfied: Yes No

| Criteria | Fulfilled? | |
|--|------------|----|
| | Yes | No |
| 1. On a one-way street or a street that has traffic predominately in one direction, the adjacent signals are so far apart that they do not provide the necessary degree of vehicle platooning. | | |
| 2. On a two-way street, adjacent signals do not provide the necessary degree of platooning, and the proposed and adjacent signals will collectively provide a progressive operation. | | |

TRAFFIC SIGNAL WARRANT SUMMARY

City: **Brighton**
County: **09 – Highlands**
District: **One**

Engineer: **KCA**
Date: **OPENING YEAR 2032**

Major Street: **SR 70**
Minor Street: **CR 721**

Lanes: **2** Major Approach Speed: **60**
Lanes: **1** Minor Approach Speed: **45**

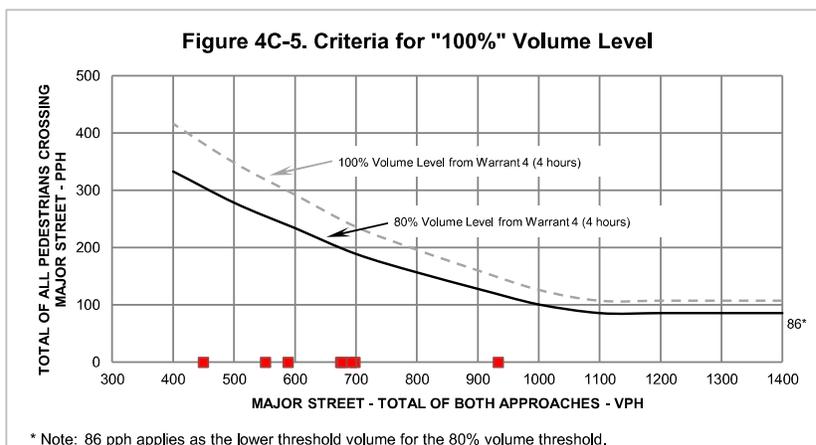
MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf>

WARRANT 7 - CRASH EXPERIENCE

Record hours where criteria are fulfilled, the corresponding volume, and other information in the boxes provided. The warrant is satisfied if **all three** of the criteria are fulfilled.

Applicable: Yes No
Satisfied: Yes No

| Criteria | | | | Fulfilled? | |
|---|-----------------------|--|----------------------------------|-------------|----------------------------|
| | | | | Yes | No |
| 1. Adequate trial of other remedial measure has failed to reduce crash frequency. | Measure tried: | | | | |
| 2. Five or more reported crashes, of types susceptible to correction by signal, have occurred within a 12-month period. | Observed Crash Types: | | Number of crashes per 12 months: | | |
| 3. One of the following volume warrants is met: | | | | Met? | |
| Warrant 1, Condition A (80% satisfied), or | | | | No | |
| Warrant 1, Condition B (80% satisfied), or | | | | No | |
| Warrant 4, Pedestrian Volume satisfied at 80% of volume requirements for any 8 hours of an average day. | | | | Hour | Major Street Volume |
| | | | | 8:00 AM | 675 |
| | | | | 12:00 PM | 552 |
| | | | | 1:00 PM | 678 |
| | | | | 2:00 PM | 699 |
| | | | | 3:00 PM | 934 |
| | | | | 4:00 PM | 693 |
| | | | | 5:00 PM | 589 |
| 6:00 PM | 450 | | | | |
| | | | | | |



TRAFFIC SIGNAL WARRANT SUMMARY

City: **Brighton**
County: **09 – Highlands**
District: **One**

Engineer: **KCA**
Date: **OPENING YEAR 2032**

Major Street: **SR 70**
Minor Street: **CR 721**

Lanes: **2** Major Approach Speed: **60**
Lanes: **1** Minor Approach Speed: **45**

MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf>

WARRANT 8 - ROADWAY NETWORK

Record hours where criteria are fulfilled, and the corresponding volume or other information in the boxes provided. The warrant is satisfied if at least one of the criteria is fulfilled and if all intersecting routes have one or more of the Major Route characteristics listed.

Applicable: Yes No

Satisfied: Yes No

| Criteria | | | | | | Met? | | Fulfilled? | | |
|--|---|--|--|--|------------------|------|----------|------------|----|--|
| | | | | | | Yes | No | Yes | No | |
| 1. Both of the criteria to the right are met. | a. Total entering volume of at least 1,000 veh/hr during a typical weekday peak hour. | | | | Entering Volume: | | | | | |
| | b. Five-year projected volumes that satisfy one or more of Warrants 1, 2, or 3. | | | | Warrant: | 1 | 2 | 3 | | |
| | | | | | Satisfied?: | | | | | |
| 2. Total entering volume at least 1,000 veh/hr for each of any 5 hrs of a non-normal business day (Sat. or Sun.) | | | | | | | ← Hour | | | |
| | | | | | | | ← Volume | | | |

| Characteristics of Major Routes | | | Met? | | Fulfilled? | |
|--|---------------|--|------|----|------------|----|
| | | | Yes | No | Yes | No |
| 1. Part of the street or highway system that serves as the principal roadway network for through traffic flow. | Major Street: | | | | | |
| | Minor Street: | | | | | |
| 2. Rural or suburban highway outside of, entering, or traversing a city. | Major Street: | | | | | |
| | Minor Street: | | | | | |
| 3. Appears as a major route on an official plan. | Major Street: | | | | | |
| | Minor Street: | | | | | |

TRAFFIC SIGNAL WARRANT SUMMARY

City: **Brighton**
County: **09 – Highlands**
District: **One**

Engineer: **KCA**
Date: **OPENING YEAR 2032**

Major Street: **SR 70**
Minor Street: **CR 721**

Lanes: **2** Major Approach Speed: **60**
Lanes: **1** Minor Approach Speed: **45**

MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf>

Approach Lane Criteria

1. How many approach lanes are there at the track crossing?

1 2 or more

If there is 1 lane, use Figure 4C-9 and if there are 2 or more, use Figure 4C-10.

Fig 4C-9 Fig 4C-10

WARRANT 9 - INTERSECTION NEAR A GRADE CROSSING

This signal warrant should be applied only after adequate consideration has been given to other alternatives or after a trial of an alternative has failed to alleviate the safety concerns associated with the grade crossing.

Indicate if both criteria are fulfilled in the boxes provided. The warrant is satisfied if both criteria are met.

Applicable: Yes No

Satisfied: Yes No

| Criteria | Fulfilled? | |
|--|--------------------------|-------------------------------------|
| | Yes | No |
| 1. A grade crossing exists on an approach controlled by a STOP or YIELD sign and the center of the track nearest to the intersection is within 140 feet of the stop line or yield line on the approach; and | <input type="checkbox"/> | <input checked="" type="checkbox"/> |
| 2. During the highest traffic volume hour during which the rail uses the crossing, the plotted point falls above the applicable curve for the existing combination of approach lanes over the track and the distance D (clear storage distance). | <input type="checkbox"/> | <input type="checkbox"/> |

Use the following tables (4C-2, 4C-3, and 4C-4 to appropriately adjust the minor-street approach volume).

Inputs

Occurrences of Rail traffic per day
% of High Occupancy Buses on Approach Lane at Track Crossing
Enter D (feet)
% of Tractor-Trailer Trucks on Approach Lane at Track Crossing

Adjustment Factors from Tables

| | |
|--|-------------|
| | |
| | 1.00 |
| | |
| | 0.50 |

Table 4C-2. Adjustment Factor for Daily Frequency of Rail Traffic

| Rail Traffic per Day | Adjustment Factor |
|----------------------|-------------------|
| 1 | 0.67 |
| 2 | 0.91 |
| 3 to 5 | 1.00 |
| 6 to 8 | 1.18 |
| 9 to 11 | 1.25 |
| 12 or more | 1.33 |

Table 4C-3. Adjustment Factor for Percentage of High-Occupancy Buses

| % of High-Occupancy Buses* on Minor Street Approach | Adjustment Factor |
|---|-------------------|
| 0% | 1.00 |
| 2% | 1.09 |
| 4% | 1.19 |
| 6% or more | 1.32 |

* A high-occupancy bus is defined as a bus occupied by at least 20 people

Table 4C-4. Adjustment Factor for Percentage of Tractor-Trailer Trucks

| % of Tractor-Trailer Trucks on Minor-Street Approach | Adjustment Factor | |
|--|---------------------|----------------------|
| | D less than 70 feet | D of 70 feet or more |
| 0% to 2.5% | 0.50 | 0.50 |
| 2.6% to 7.5% | 0.75 | 0.75 |
| 7.6% to 12.5% | 1.00 | 1.00 |
| 12.6% to 17.5% | 2.30 | 1.15 |
| 17.6% to 22.5% | 2.70 | 1.35 |
| 22.6% to 27.5% | 3.28 | 1.64 |
| More than 27.5% | 4.18 | 2.09 |

Input the major and minor street volumes before adjustment factors are applied

| 1 Approach Lane | | |
|-----------------|--|--|
| | | |

D (ft) Major Vol. Minor Vol.

After adjustment factors are applied

| 1 Approach Lane w/Factors | | |
|---------------------------|--|--|
| | | |

D (ft) Major Vol. Minor Vol.

Input D and the major and minor street volumes before adjustment factors are applied

| 2 or more Approach Lanes | | |
|--------------------------|--|--|
| | | |

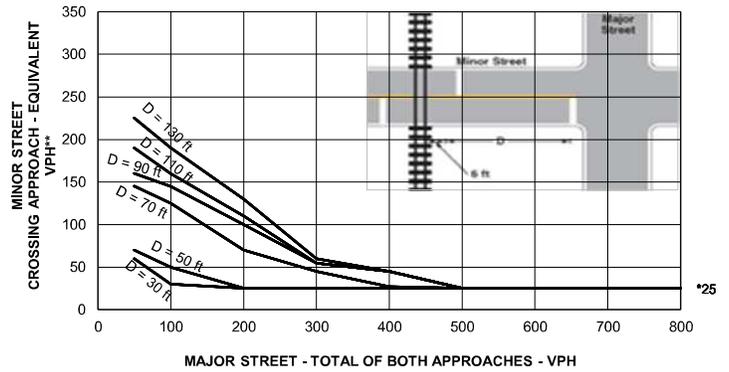
D (ft) Major Vol. Minor Vol.

After adjustment factors are applied

| 2+ Approach Lane w/Factors | | |
|----------------------------|--|--|
| | | |

D (ft) Major Vol. Minor Vol.

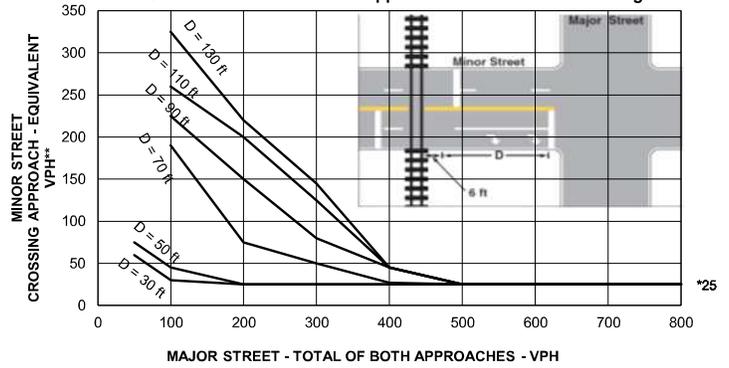
FIGURE 4C-9: Criteria for 1 Approach Lane at the Track Crossing



* Note: 25 vph applies as the lower threshold volume

**Note: VPH after applying the adjustment factors in Tables 4C-2, 4C, and/or 4C-4, if appropriate

FIGURE 4C-10: Criteria for 2+ Approach Lanes at Track Crossing



* Note: 25 vph applies as the lower threshold volume

**Note: VPH after applying the adjustment factors in Tables 4C-2, 4C, and/or 4C-4, if appropriate

TRAFFIC SIGNAL WARRANT SUMMARY

City: **Brighton**
 County: **09 – Highlands**
 District: **One**

Engineer: **KCA**
 Date: **OPENING YEAR 2032**

Major Street: **SR 70**
 Minor Street: **CR 721**

Lanes: **2**
 Lanes: **1**

Major Approach Speed: **60**
 Minor Approach Speed: **45**

MUTCD Electronic Reference to Chapter 4: <http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf>

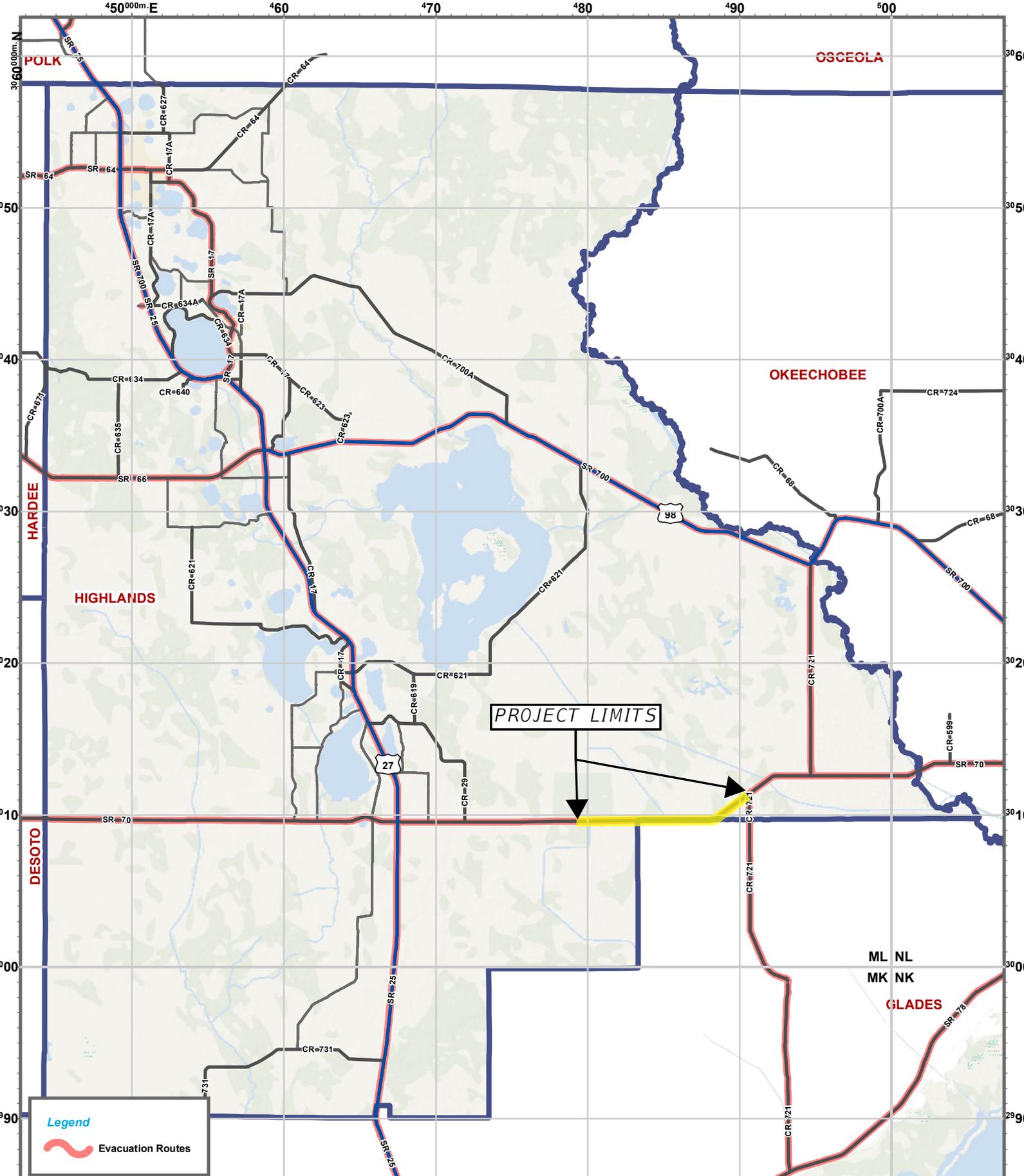
CONCLUSIONS

Remarks: **Based on the planned 4-lane divided typical section of SR 70, the traffic volume projections at CR 721 indicate none of the warrants are expected to be met in opening year 2032.**

WARRANTS SATISFIED:

| | | | |
|-----------|--|------------------------------|---|
| Warrant 1 | <input type="checkbox"/> Not Applicable | <input type="checkbox"/> Met | <input checked="" type="checkbox"/> Not Met |
| Warrant 2 | <input type="checkbox"/> Not Applicable | <input type="checkbox"/> Met | <input checked="" type="checkbox"/> Not Met |
| Warrant 3 | <input checked="" type="checkbox"/> Not Applicable | <input type="checkbox"/> Met | <input type="checkbox"/> Not Met |
| Warrant 4 | <input checked="" type="checkbox"/> Not Applicable | <input type="checkbox"/> Met | <input type="checkbox"/> Not Met |
| Warrant 5 | <input checked="" type="checkbox"/> Not Applicable | <input type="checkbox"/> Met | <input type="checkbox"/> Not Met |
| Warrant 6 | <input checked="" type="checkbox"/> Not Applicable | <input type="checkbox"/> Met | <input type="checkbox"/> Not Met |
| Warrant 7 | <input checked="" type="checkbox"/> Not Applicable | <input type="checkbox"/> Met | <input type="checkbox"/> Not Met |
| Warrant 8 | <input checked="" type="checkbox"/> Not Applicable | <input type="checkbox"/> Met | <input type="checkbox"/> Not Met |
| Warrant 9 | <input checked="" type="checkbox"/> Not Applicable | <input type="checkbox"/> Met | <input type="checkbox"/> Not Met |

APPENDIX G: Existing Highlands County Evacuation Scenario Reports



Disclaimer: Map is intended for reference only
No warranty for accuracy provided

Created By: GIS Section
Requested By: Standard Map Product
Date: 8/18/2021
Time: 1:07:36 PM
Path: S:\Projects\EvacRoute_SurgeZone_Maps\2021_Maps\MXDs\EvacRoutes\UTM17_Portrait.mxd

HIGHLANDS EVACUATION ROUTES





TIME Scenario Report: CFRPC_Base_Scenario_1_Level_A_2020

| | |
|--|---|
| Name: | CFRPC_Base_Scenario_1_Level_A_2020 |
| Description: | |
| Comments: | |
| Date: | 6/12/2021 12:24:39 AM |
| Region: | 2 - Central Florida |
| Behavioral Assumption: | 100% Response |
| Network Period: | 2020 |
| Population Period: | 2020 |
| Model: | Run Full Model |
| University Population: | Fall/Spring Session (100% in residence) |
| Number of Evacuating Counties: | 10 |
| Number of Tourist Counties: | 10 |
| Number of Shelters Open: | 712 |
| Shelter Status: | Primary Open |
| Shelter Capacity: | 312,823 |
| Number of No-Go Counties: | 0 |
| Number of Modified Network Counties: | 0 |
| Number of Modified Small Area Counties: | 0 |
| Regional Clearance Time: | 19.5 |



Evacuation Demographics Summary: Population

| Counties | Site-Built Population | Mobile Home Population | University Population | Tourist Population | Total Evacuating Population |
|--------------|-----------------------|------------------------|-----------------------|--------------------|-----------------------------|
| Charlotte | 81,014 | 12,385 | 0 | 1,226 | 94,625 |
| DeSoto | 3,881 | 8,797 | 0 | 0 | 12,678 |
| Hardee | 2,746 | 5,994 | 0 | 0 | 8,740 |
| Highlands | 13,021 | 16,770 | 0 | 0 | 29,791 |
| Hillsborough | 380,908 | 76,919 | 91 | 7,290 | 465,208 |
| Manatee | 112,739 | 34,973 | 0 | 2,504 | 150,217 |
| Okeechobee | 3,942 | 10,791 | 0 | 0 | 14,733 |
| Pinellas | 327,576 | 58,448 | 314 | 23,754 | 410,092 |
| Polk | 58,391 | 112,822 | 0 | 0 | 171,213 |
| Sarasota | 123,757 | 26,052 | 38 | 5,738 | 155,585 |



Evacuation Demographics Summary: Vehicles

| Counties | Site-Built Evacuating Vehicles | Mobile Home Evacuating Vehicles | University Evacuating Vehicles | Tourist Evacuating Vehicles | Total Evacuating Vehicles |
|--------------|--------------------------------|---------------------------------|--------------------------------|-----------------------------|---------------------------|
| Charlotte | 39,981 | 8,743 | 0 | 613 | 49,337 |
| DeSoto | 1,520 | 4,409 | 0 | 0 | 5,930 |
| Hardee | 909 | 2,667 | 0 | 0 | 3,577 |
| Highlands | 5,292 | 9,351 | 0 | 0 | 14,643 |
| Hillsborough | 174,307 | 51,122 | 91 | 3,645 | 229,165 |
| Manatee | 48,966 | 21,614 | 0 | 1,252 | 71,832 |
| Okeechobee | 1,486 | 5,906 | 0 | 0 | 7,393 |
| Pinellas | 170,768 | 35,935 | 314 | 11,877 | 218,893 |
| Polk | 20,744 | 59,927 | 0 | 0 | 80,672 |
| Sarasota | 60,390 | 17,973 | 38 | 2,869 | 81,270 |



Sheltering Demand

| Counties | Sheltering Demand |
|--------------|-------------------|
| Charlotte | 4,721 |
| DeSoto | 1,711 |
| Hardee | 1,092 |
| Highlands | 4,980 |
| Hillsborough | 22,067 |
| Manatee | 7,744 |
| Okeechobee | 1,724 |
| Pinellas | 19,754 |
| Polk | 17,142 |
| Sarasota | 9,694 |

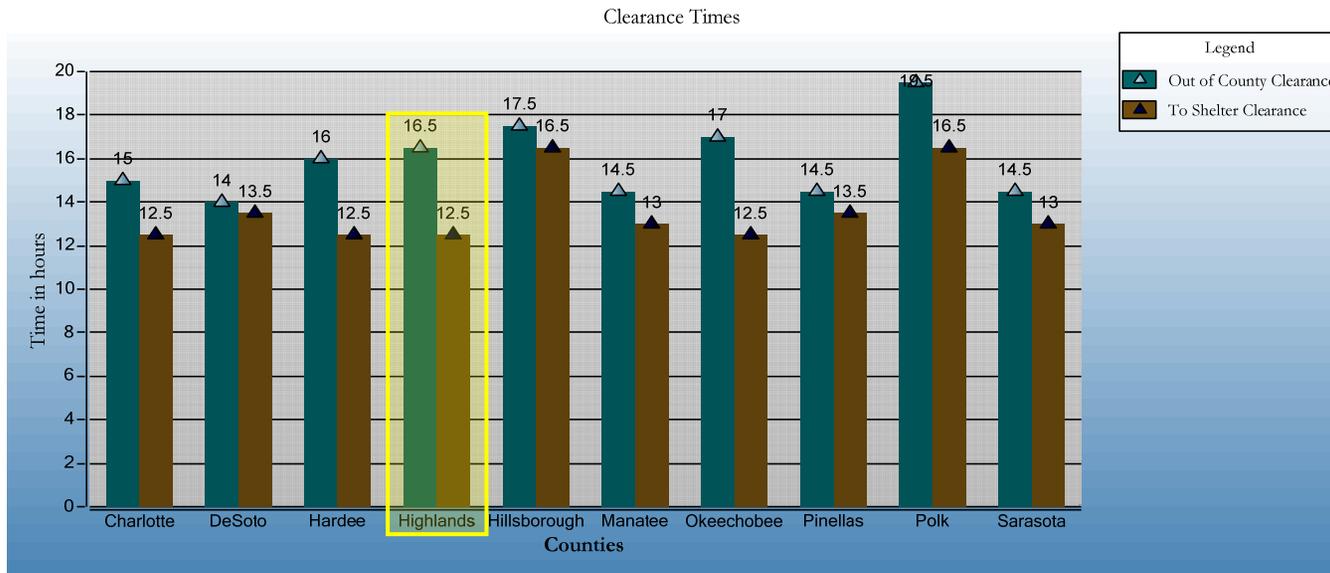


Evacuation Clearance Times (Hours)

| Counties | In County | Out of County | To Shelter |
|--------------|-----------|---------------|------------|
| Charlotte | 15.0 | 15.0 | 12.5 |
| DeSoto | 14.0 | 14.0 | 13.5 |
| Hardee | 16.0 | 16.0 | 12.5 |
| Highlands | 16.5 | 16.5 | 12.5 |
| Hillsborough | 17.5 | 17.5 | 16.5 |
| Manatee | 14.5 | 14.5 | 13.0 |
| Okeechobee | 17.0 | 17.0 | 12.5 |
| Pinellas | 14.5 | 14.5 | 13.5 |
| Polk | 19.5 | 19.5 | 16.5 |
| Sarasota | 14.5 | 14.5 | 13.0 |



Evacuation Clearance Times (Graph)





TIME Scenario Report: CFRPC_Base_Scenario_2_Level_B_2020

| | |
|--|---|
| Name: | CFRPC_Base_Scenario_2_Level_B_2020 |
| Description: | |
| Comments: | |
| Date: | 6/11/2021 11:58:35 PM |
| Region: | 2 - Central Florida |
| Behavioral Assumption: | 100% Response |
| Network Period: | 2020 |
| Population Period: | 2020 |
| Model: | Run Full Model |
| University Population: | Fall/Spring Session (100% in residence) |
| Number of Evacuating Counties: | 10 |
| Number of Tourist Counties: | 10 |
| Number of Shelters Open: | 712 |
| Shelter Status: | Primary Open |
| Shelter Capacity: | 312,823 |
| Number of No-Go Counties: | 0 |
| Number of Modified Network Counties: | 0 |
| Number of Modified Small Area Counties: | 0 |
| Regional Clearance Time: | 22.5 |



Evacuation Demographics Summary: Population

| Counties | Site-Built Population | Mobile Home Population | University Population | Tourist Population | Total Evacuating Population |
|--------------|-----------------------|------------------------|-----------------------|--------------------|-----------------------------|
| Charlotte | 131,851 | 12,385 | 0 | 2,058 | 146,294 |
| DeSoto | 5,093 | 8,797 | 0 | 0 | 13,890 |
| Hardee | 2,746 | 5,994 | 0 | 0 | 8,740 |
| Highlands | 17,362 | 16,770 | 0 | 0 | 34,132 |
| Hillsborough | 454,186 | 76,919 | 99 | 11,197 | 542,402 |
| Manatee | 140,733 | 34,973 | 0 | 2,822 | 178,528 |
| Okeechobee | 4,548 | 10,791 | 0 | 0 | 15,339 |
| Pasco | 139,260 | 81,235 | 0 | 0 | 220,495 |
| Pinellas | 402,842 | 58,448 | 314 | 25,274 | 486,878 |
| Polk | 75,908 | 112,822 | 0 | 0 | 188,731 |



Evacuation Demographics Summary: Vehicles

| Counties | Site-Built Evacuating Vehicles | Mobile Home Evacuating Vehicles | University Evacuating Vehicles | Tourist Evacuating Vehicles | Total Evacuating Vehicles |
|--------------|--------------------------------|---------------------------------|--------------------------------|-----------------------------|---------------------------|
| Charlotte | 62,958 | 8,743 | 0 | 1,029 | 72,730 |
| DeSoto | 1,990 | 4,409 | 0 | 0 | 6,400 |
| Hardee | 909 | 2,667 | 0 | 0 | 3,577 |
| Highlands | 7,056 | 9,351 | 0 | 0 | 16,406 |
| Hillsborough | 207,194 | 51,122 | 99 | 5,598 | 264,013 |
| Manatee | 60,500 | 21,614 | 0 | 1,411 | 83,524 |
| Okeechobee | 1,715 | 5,906 | 0 | 0 | 7,621 |
| Pasco | 67,443 | 45,522 | 0 | 0 | 112,964 |
| Pinellas | 206,301 | 35,935 | 314 | 12,637 | 255,186 |
| Polk | 26,968 | 59,927 | 0 | 0 | 86,895 |



Sheltering Demand

| Counties | Sheltering Demand |
|--------------|-------------------|
| Charlotte | 7,474 |
| DeSoto | 1,907 |
| Hardee | 1,141 |
| Highlands | 5,676 |
| Hillsborough | 26,048 |
| Manatee | 9,341 |
| Okeechobee | 1,896 |
| Pasco | 14,761 |
| Pinellas | 23,336 |
| Polk | 19,401 |

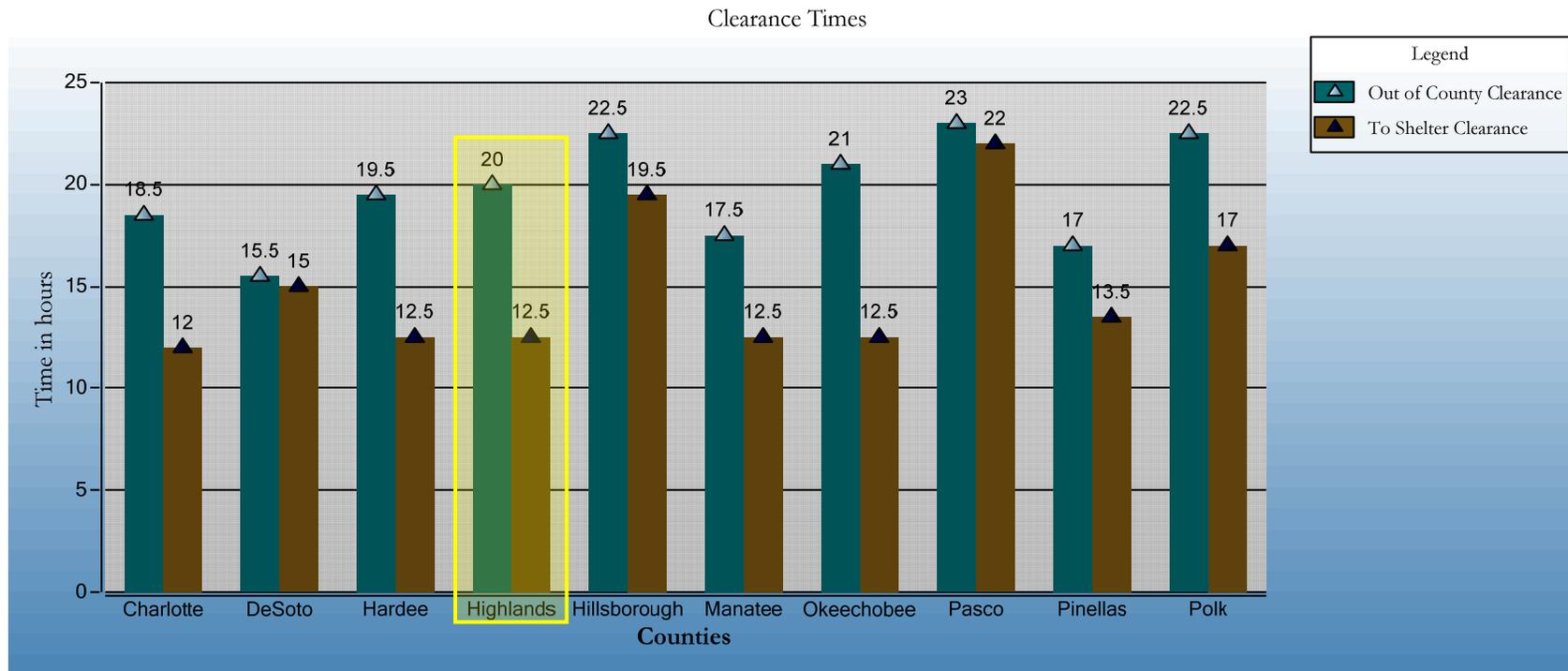


Evacuation Clearance Times (Hours)

| Counties | In County | Out of County | To Shelter |
|--------------|-----------|---------------|------------|
| Charlotte | 18.5 | 18.5 | 12.0 |
| DeSoto | 15.5 | 15.5 | 15.0 |
| Hardee | 19.5 | 19.5 | 12.5 |
| Highlands | 20.0 | 20.0 | 12.5 |
| Hillsborough | 22.5 | 22.5 | 19.5 |
| Manatee | 17.5 | 17.5 | 12.5 |
| Okeechobee | 21.0 | 21.0 | 12.5 |
| Pasco | 23.0 | 23.0 | 22.0 |
| Pinellas | 17.0 | 17.0 | 13.5 |
| Polk | 22.5 | 22.5 | 17.0 |



Evacuation Clearance Times (Graph)





TIME Scenario Report: CFRPC_Base_Scenario_3_Level_C_2020

| | |
|--|---|
| Name: | CFRPC_Base_Scenario_3_Level_C_2020 |
| Description: | |
| Comments: | |
| Date: | 6/11/2021 9:12:40 PM |
| Region: | 2 - Central Florida |
| Behavioral Assumption: | 100% Response |
| Network Period: | 2020 |
| Population Period: | 2020 |
| Model: | Run Full Model |
| University Population: | Fall/Spring Session (100% in residence) |
| Number of Evacuating Counties: | 10 |
| Number of Tourist Counties: | 10 |
| Number of Shelters Open: | 712 |
| Shelter Status: | Primary Open |
| Shelter Capacity: | 312,823 |
| Number of No-Go Counties: | 0 |
| Number of Modified Network Counties: | 0 |
| Number of Modified Small Area Counties: | 0 |
| Regional Clearance Time: | 31.0 |



Evacuation Demographics Summary: Population

| Counties | Site-Built Population | Mobile Home Population | University Population | Tourist Population | Total Evacuating Population |
|--------------|-----------------------|------------------------|-----------------------|--------------------|-----------------------------|
| Charlotte | 157,307 | 12,385 | 0 | 2,234 | 171,927 |
| DeSoto | 7,332 | 8,797 | 0 | 0 | 16,130 |
| Hardee | 4,224 | 5,994 | 0 | 0 | 10,218 |
| Highlands | 21,714 | 16,770 | 0 | 0 | 38,484 |
| Hillsborough | 558,745 | 76,919 | 137 | 22,025 | 657,826 |
| Manatee | 187,159 | 34,973 | 0 | 4,543 | 226,675 |
| Okeechobee | 6,974 | 10,791 | 0 | 0 | 17,765 |
| Pinellas | 506,960 | 58,448 | 314 | 29,819 | 595,540 |
| Polk | 116,782 | 112,822 | 0 | 0 | 229,604 |
| Sarasota | 250,843 | 26,052 | 72 | 9,164 | 286,130 |



Evacuation Demographics Summary: Vehicles

| Counties | Site-Built Evacuating Vehicles | Mobile Home Evacuating Vehicles | University Evacuating Vehicles | Tourist Evacuating Vehicles | Total Evacuating Vehicles |
|--------------|--------------------------------|---------------------------------|--------------------------------|-----------------------------|---------------------------|
| Charlotte | 74,479 | 8,743 | 0 | 1,117 | 84,340 |
| DeSoto | 2,833 | 4,409 | 0 | 0 | 7,242 |
| Hardee | 1,399 | 2,667 | 0 | 0 | 4,066 |
| Highlands | 8,820 | 9,351 | 0 | 0 | 18,170 |
| Hillsborough | 254,056 | 51,122 | 137 | 11,012 | 316,327 |
| Manatee | 78,727 | 21,614 | 0 | 2,271 | 102,612 |
| Okeechobee | 2,630 | 5,906 | 0 | 0 | 8,536 |
| Pinellas | 254,847 | 35,935 | 314 | 14,909 | 306,005 |
| Polk | 41,489 | 59,927 | 0 | 0 | 101,416 |
| Sarasota | 120,792 | 17,973 | 72 | 4,582 | 143,419 |



Sheltering Demand

| Counties | Sheltering Demand |
|--------------|-------------------|
| Charlotte | 9,291 |
| DeSoto | 2,124 |
| Hardee | 1,277 |
| Highlands | 6,099 |
| Hillsborough | 32,745 |
| Manatee | 11,964 |
| Okeechobee | 2,150 |
| Pinellas | 29,387 |
| Polk | 22,087 |
| Sarasota | 17,438 |

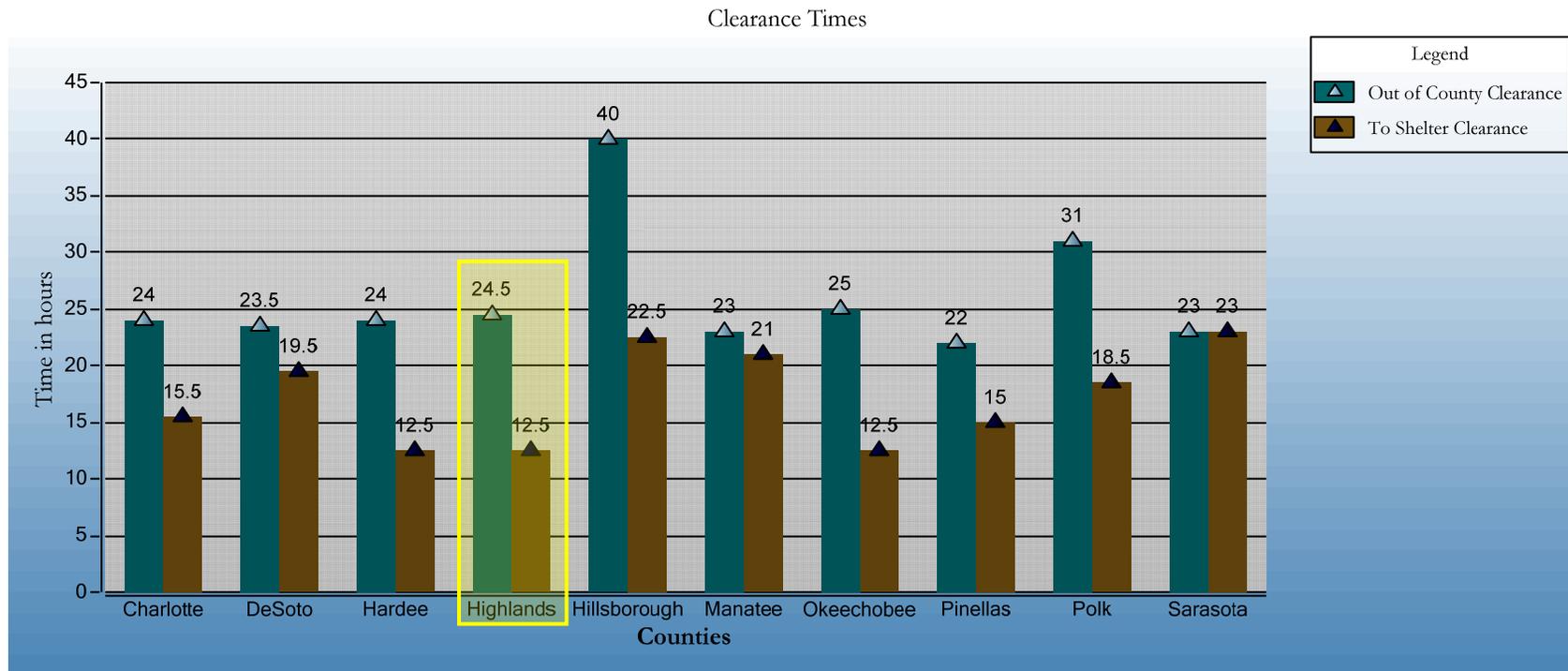


Evacuation Clearance Times (Hours)

| Counties | In County | Out of County | To Shelter |
|--------------|-----------|---------------|------------|
| Charlotte | 24.0 | 24.0 | 15.5 |
| DeSoto | 23.5 | 23.5 | 19.5 |
| Hardee | 24.0 | 24.0 | 12.5 |
| Highlands | 24.5 | 24.5 | 12.5 |
| Hillsborough | 40.0 | 40.0 | 22.5 |
| Manatee | 23.0 | 23.0 | 21.0 |
| Okeechobee | 25.0 | 25.0 | 12.5 |
| Pinellas | 22.0 | 22.0 | 15.0 |
| Polk | 31.0 | 31.0 | 18.5 |
| Sarasota | 23.0 | 23.0 | 23.0 |



Evacuation Clearance Times (Graph)





TIME Scenario Report: CFRPC_Base_Scenario_4_Level_D_2020

| | |
|--|---|
| Name: | CFRPC_Base_Scenario_4_Level_D_2020 |
| Description: | |
| Comments: | |
| Date: | 6/10/2021 8:30:30 PM |
| Region: | 2 - Central Florida |
| Behavioral Assumption: | 100% Response |
| Network Period: | 2020 |
| Population Period: | 2020 |
| Model: | Run Full Model |
| University Population: | Fall/Spring Session (100% in residence) |
| Number of Evacuating Counties: | 10 |
| Number of Tourist Counties: | 10 |
| Number of Shelters Open: | 712 |
| Shelter Status: | Primary Open |
| Shelter Capacity: | 312,823 |
| Number of No-Go Counties: | 0 |
| Number of Modified Network Counties: | 0 |
| Number of Modified Small Area Counties: | 0 |
| Regional Clearance Time: | 40.5 |



Evacuation Demographics Summary: Population

| Counties | Site-Built Population | Mobile Home Population | University Population | Tourist Population | Total Evacuating Population |
|--------------|-----------------------|------------------------|-----------------------|--------------------|-----------------------------|
| Charlotte | 167,585 | 12,385 | 0 | 3,475 | 183,445 |
| DeSoto | 9,795 | 8,797 | 0 | 0 | 18,592 |
| Hardee | 6,336 | 5,994 | 0 | 0 | 12,330 |
| Highlands | 33,036 | 16,770 | 0 | 0 | 49,806 |
| Hillsborough | 721,557 | 76,919 | 193 | 25,927 | 824,597 |
| Manatee | 264,968 | 34,973 | 0 | 6,361 | 306,303 |
| Okeechobee | 10,006 | 10,791 | 0 | 0 | 20,797 |
| Pasco | 247,543 | 81,235 | 0 | 0 | 328,778 |
| Pinellas | 618,473 | 58,448 | 314 | 31,523 | 708,757 |
| Polk | 175,173 | 112,822 | 0 | 0 | 287,995 |



Evacuation Demographics Summary: Vehicles

| Counties | Site-Built Evacuating Vehicles | Mobile Home Evacuating Vehicles | University Evacuating Vehicles | Tourist Evacuating Vehicles | Total Evacuating Vehicles |
|--------------|--------------------------------|---------------------------------|--------------------------------|-----------------------------|---------------------------|
| Charlotte | 79,346 | 8,743 | 0 | 1,738 | 89,827 |
| DeSoto | 4,053 | 4,960 | 0 | 0 | 9,014 |
| Hardee | 2,249 | 2,667 | 0 | 0 | 4,916 |
| Highlands | 14,364 | 10,519 | 0 | 0 | 24,883 |
| Hillsborough | 324,932 | 51,122 | 193 | 12,964 | 389,210 |
| Manatee | 109,190 | 21,614 | 0 | 3,181 | 133,985 |
| Okeechobee | 3,773 | 6,275 | 0 | 0 | 10,049 |
| Pasco | 117,950 | 45,522 | 0 | 0 | 163,472 |
| Pinellas | 306,953 | 35,935 | 314 | 15,761 | 358,963 |
| Polk | 62,233 | 67,418 | 0 | 0 | 129,651 |



Sheltering Demand

| Counties | Sheltering Demand |
|--------------|-------------------|
| Charlotte | 10,280 |
| DeSoto | 2,605 |
| Hardee | 1,554 |
| Highlands | 7,929 |
| Hillsborough | 49,563 |
| Manatee | 17,379 |
| Okeechobee | 2,627 |
| Pasco | 22,881 |
| Pinellas | 37,507 |
| Polk | 28,879 |

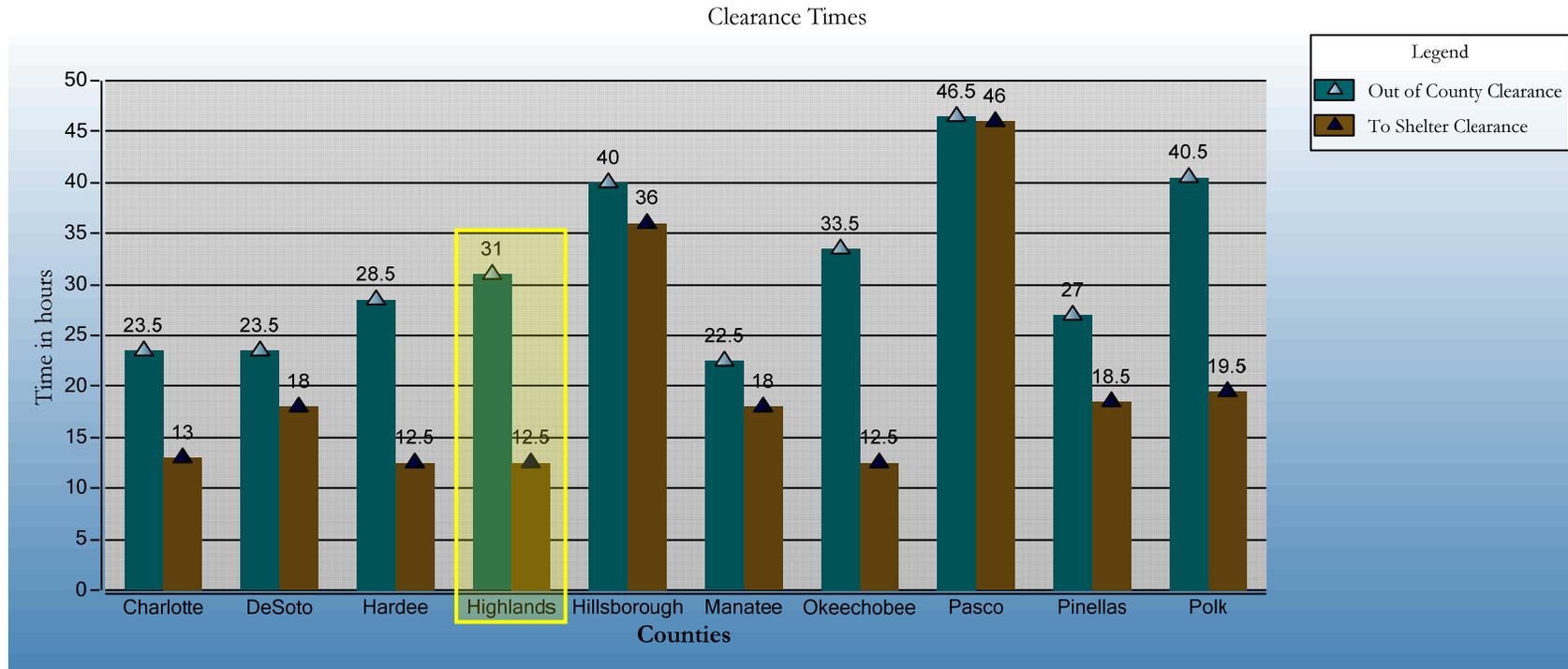


Evacuation Clearance Times (Hours)

| Counties | In County | Out of County | To Shelter |
|--------------|-----------|---------------|------------|
| Charlotte | 23.5 | 23.5 | 13.0 |
| DeSoto | 23.5 | 23.5 | 18.0 |
| Hardee | 28.5 | 28.5 | 12.5 |
| Highlands | 31.0 | 31.0 | 12.5 |
| Hillsborough | 40.0 | 40.0 | 36.0 |
| Manatee | 22.5 | 22.5 | 18.0 |
| Okeechobee | 33.5 | 33.5 | 12.5 |
| Pasco | 46.5 | 46.5 | 46.0 |
| Pinellas | 27.0 | 27.0 | 18.5 |
| Polk | 40.5 | 40.5 | 19.5 |



Evacuation Clearance Times (Graph)





TIME Scenario Report: CFRPC_Base_Scenario_5_Level_E_2020

| | |
|--|---|
| Name: | CFRPC_Base_Scenario_5_Level_E_2020 |
| Description: | |
| Comments: | |
| Date: | 6/10/2021 8:13:41 PM |
| Region: | 2 - Central Florida |
| Behavioral Assumption: | 100% Response |
| Network Period: | 2020 |
| Population Period: | 2020 |
| Model: | Run Full Model |
| University Population: | Fall/Spring Session (100% in residence) |
| Number of Evacuating Counties: | 10 |
| Number of Tourist Counties: | 10 |
| Number of Shelters Open: | 712 |
| Shelter Status: | Primary Open |
| Shelter Capacity: | 312,823 |
| Number of No-Go Counties | 0 |
| Number of Modified Network Counties | 0 |
| Number of Modified Small Area Counties: | 0 |



Evacuation Demographics Summary: Population

| Counties | Site-Built Population | Mobile Home Population | University Population | Tourist Population | Total Evacuating Population |
|--------------|-----------------------|------------------------|-----------------------|--------------------|-----------------------------|
| Charlotte | 167,958 | 12,385 | 0 | 3,475 | 183,818 |
| DeSoto | 12,883 | 8,797 | 0 | 125 | 21,805 |
| Hardee | 6,970 | 5,994 | 0 | 0 | 12,964 |
| Highlands | 38,288 | 16,770 | 0 | 0 | 55,058 |
| Hillsborough | 875,845 | 76,919 | 275 | 30,337 | 983,376 |
| Manatee | 295,771 | 34,973 | 0 | 7,433 | 338,177 |
| Okeechobee | 10,613 | 10,791 | 0 | 0 | 21,404 |
| Pinellas | 679,606 | 58,448 | 314 | 33,073 | 771,441 |
| Polk | 192,690 | 112,822 | 0 | 0 | 305,513 |
| Sarasota | 336,930 | 26,052 | 134 | 10,860 | 373,977 |



Evacuation Demographics Summary: Vehicles

| Counties | Site-Built Evacuating Vehicles | Mobile Home Evacuating Vehicles | University Evacuating Vehicles | Tourist Evacuating Vehicles | Total Evacuating Vehicles |
|--------------|--------------------------------|---------------------------------|--------------------------------|-----------------------------|---------------------------|
| Charlotte | 79,508 | 8,743 | 0 | 1,738 | 89,988 |
| DeSoto | 5,339 | 4,960 | 0 | 63 | 10,363 |
| Hardee | 2,474 | 2,845 | 0 | 0 | 5,318 |
| Highlands | 16,632 | 10,519 | 0 | 0 | 27,151 |
| Hillsborough | 392,015 | 51,122 | 275 | 15,169 | 458,580 |
| Manatee | 122,610 | 21,614 | 0 | 3,716 | 147,941 |
| Okeechobee | 4,288 | 6,275 | 0 | 0 | 10,563 |
| Pinellas | 335,057 | 35,935 | 314 | 16,537 | 387,842 |
| Polk | 73,722 | 67,418 | 0 | 0 | 141,141 |
| Sarasota | 159,850 | 17,973 | 134 | 5,430 | 183,387 |



Sheltering Demand

| Counties | Sheltering Demand |
|--------------|-------------------|
| Charlotte | 10,671 |
| DeSoto | 2,925 |
| Hardee | 1,680 |
| Highlands | 8,477 |
| Hillsborough | 63,451 |
| Manatee | 20,378 |
| Okeechobee | 2,779 |
| Pinellas | 43,760 |
| Polk | 31,217 |
| Sarasota | 25,578 |

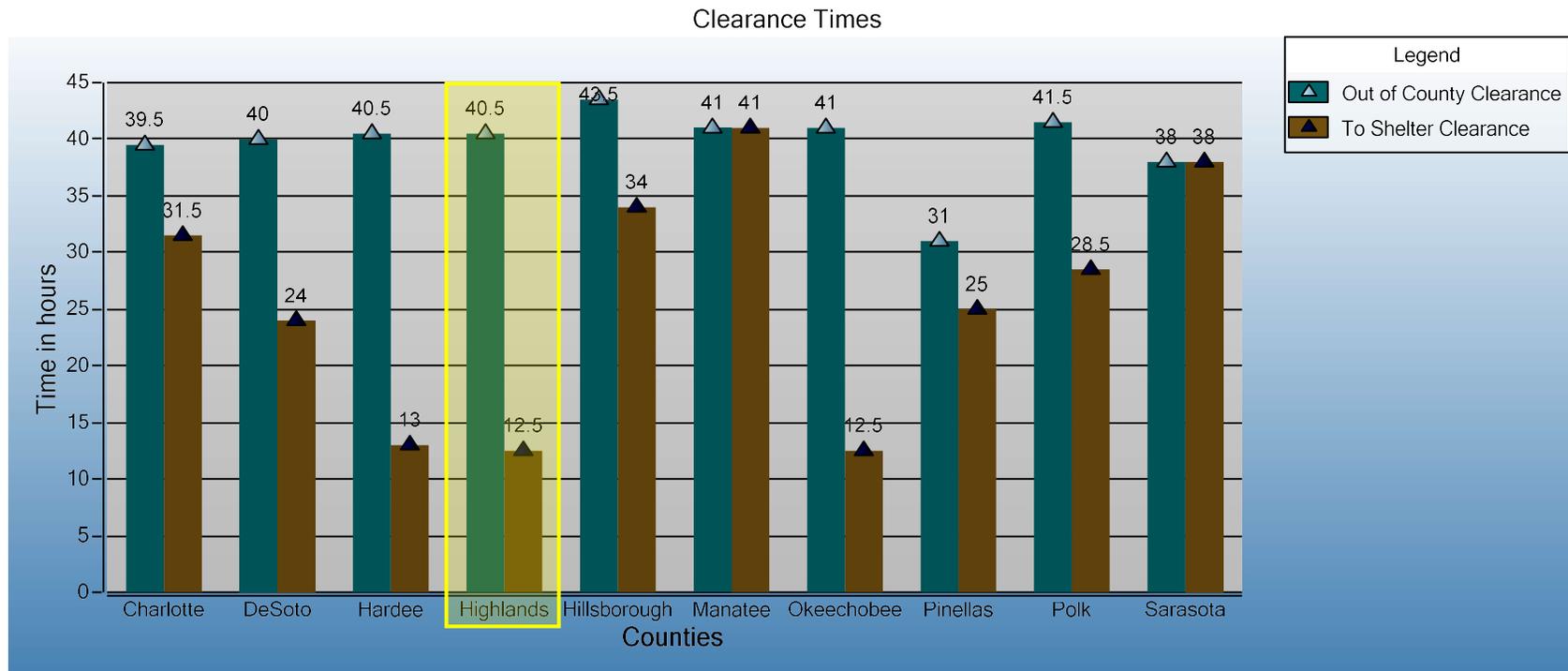


Evacuation Clearance Times (Hours)

| Counties | In County | Out of County | To Shelter |
|--------------|-----------|---------------|------------|
| Charlotte | 39.5 | 39.5 | 31.5 |
| DeSoto | 40.0 | 40.0 | 24.0 |
| Hardee | 40.5 | 40.5 | 13.0 |
| Highlands | 40.5 | 40.5 | 12.5 |
| Hillsborough | 43.5 | 43.5 | 34.0 |
| Manatee | 41.0 | 41.0 | 41.0 |
| Okeechobee | 41.0 | 41.0 | 12.5 |
| Pinellas | 31.0 | 31.0 | 25.0 |
| Polk | 41.5 | 41.5 | 28.5 |
| Sarasota | 38.0 | 38.0 | 38.0 |



Evacuation Clearance Times (Graph)



APPENDIX H: Future Synchro, SIDRA, and HCS LOS Computer Outputs

Synchro, HCS LOS Computer Outputs Design Year 2052 Volumes - No Build

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 3 | 526 | 14 | 6 | 413 | 0 | 9 | 0 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 3 | 526 | 14 | 6 | 413 | 0 | 9 | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 16 | 16 | 16 | 0 | 0 | 100 | 0 | 0 | 0 |
| Mvmt Flow | 3 | 554 | 15 | 6 | 435 | 0 | 9 | 0 | 0 | 0 | 0 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|------|-----|--------|------|-----|
| Conflicting Flow All | 435 | 0 | 0 | 568 | 0 | 0 | 1015 | 1015 | 561 | 1007 | 1022 | 435 |
| Stage 1 | - | - | - | - | - | - | 567 | 567 | - | 447 | 447 | - |
| Stage 2 | - | - | - | - | - | - | 447 | 447 | - | 560 | 575 | - |
| Critical Hdwy | 4.26 | - | - | 4.26 | - | - | 7.1 | 6.5 | 7.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.344 | - | - | 2.344 | - | - | 3.5 | 4 | 4.2 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1054 | - | - | 938 | - | - | 219 | 240 | 380 | 221 | 238 | 626 |
| Stage 1 | - | - | - | - | - | - | 512 | 510 | - | 594 | 577 | - |
| Stage 2 | - | - | - | - | - | - | 594 | 577 | - | 516 | 506 | - |
| Platoon blocked, % | | - | - | - | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1054 | - | - | 938 | - | - | 216 | 237 | 380 | 218 | 235 | 626 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 216 | 237 | - | 218 | 235 | - |
| Stage 1 | - | - | - | - | - | - | 509 | 508 | - | 589 | 571 | - |
| Stage 2 | - | - | - | - | - | - | 589 | 571 | - | 514 | 504 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|------------------------|------|--|--|------|--|--|-------|--|--|----|--|--|
| HCM Control Delay, s/v | 0.05 | | | 0.13 | | | 22.45 | | | 0 | | |
| HCM LOS | | | | | | | C | | | A | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 216 | 10 | - | - | 26 | - | - | - |
| HCM Lane V/C Ratio | 0.044 | 0.003 | - | - | 0.007 | - | - | - |
| HCM Control Delay (s/veh) | 22.4 | 8.4 | 0 | - | 8.9 | 0 | - | 0 |
| HCM Lane LOS | C | A | A | - | A | A | - | A |
| HCM 95th %tile Q(veh) | 0.1 | 0 | - | - | 0 | - | - | - |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.4 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 0 | 489 | 5 | 0 | 419 | 0 | 16 | 2 | 2 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 489 | 5 | 0 | 419 | 0 | 16 | 2 | 2 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 16 | 16 | 16 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 515 | 5 | 0 | 441 | 0 | 17 | 2 | 2 | 0 | 0 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|-----|-----|--------|-----|-----|
| Conflicting Flow All | 441 | 0 | 0 | 520 | 0 | 0 | 958 | 958 | 517 | 957 | 961 | 441 |
| Stage 1 | - | - | - | - | - | - | 517 | 517 | - | 441 | 441 | - |
| Stage 2 | - | - | - | - | - | - | 441 | 441 | - | 516 | 520 | - |
| Critical Hdwy | 4.26 | - | - | 4.26 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.344 | - | - | 2.344 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1048 | - | - | 978 | - | - | 239 | 259 | 562 | 239 | 258 | 620 |
| Stage 1 | - | - | - | - | - | - | 545 | 537 | - | 599 | 580 | - |
| Stage 2 | - | - | - | - | - | - | 599 | 580 | - | 546 | 535 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1048 | - | - | 978 | - | - | 239 | 259 | 562 | 237 | 258 | 620 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 239 | 259 | - | 237 | 258 | - |
| Stage 1 | - | - | - | - | - | - | 545 | 537 | - | 599 | 580 | - |
| Stage 2 | - | - | - | - | - | - | 599 | 580 | - | 542 | 535 | - |

| Approach | EB | WB | NB | SB |
|------------------------|----|----|-------|----|
| HCM Control Delay, s/v | 0 | 0 | 20.35 | 0 |
| HCM LOS | | | C | A |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|------|-----|-----|-----|-----|-----|-------|
| Capacity (veh/h) | 256 | 1048 | - | - | 978 | - | - | - |
| HCM Lane V/C Ratio | 0.082 | - | - | - | - | - | - | - |
| HCM Control Delay (s/veh) | 20.4 | 0 | - | - | 0 | - | - | 0 |
| HCM Lane LOS | C | A | - | - | A | - | - | A |
| HCM 95th %tile Q(veh) | 0.3 | 0 | - | - | 0 | - | - | - |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 8.1 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 0 | 477 | 113 | 276 | 336 | 2 | 26 | 0 | 92 | 0 | 8 | 0 |
| Future Vol, veh/h | 0 | 477 | 113 | 276 | 336 | 2 | 26 | 0 | 92 | 0 | 8 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 13 | 13 | 13 | 8 | 8 | 8 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 502 | 119 | 291 | 354 | 2 | 27 | 0 | 97 | 0 | 8 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|-------|-------|--------|------|-----|
| Conflicting Flow All | 356 | 0 | 0 | 621 | 0 | 0 | 1501 | 1498 | 562 | 1438 | 1557 | 355 |
| Stage 1 | - | - | - | - | - | - | 562 | 562 | - | 936 | 936 | - |
| Stage 2 | - | - | - | - | - | - | 939 | 937 | - | 502 | 621 | - |
| Critical Hdwy | 4.26 | - | - | 4.23 | - | - | 7.18 | 6.58 | 6.28 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.18 | 5.58 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.18 | 5.58 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.344 | - | - | 2.317 | - | - | 3.572 | 4.072 | 3.372 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1129 | - | - | 909 | - | - | 97 | 119 | 515 | 112 | 114 | 694 |
| Stage 1 | - | - | - | - | - | - | 501 | 500 | - | 321 | 347 | - |
| Stage 2 | - | - | - | - | - | - | 309 | 336 | - | 555 | 482 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1129 | - | - | 909 | - | - | 54 | 71 | 515 | 55 | 68 | 694 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 54 | 71 | - | 55 | 68 | - |
| Stage 1 | - | - | - | - | - | - | 501 | 500 | - | 193 | 208 | - |
| Stage 2 | - | - | - | - | - | - | 178 | 202 | - | 451 | 482 | - |

| Approach | EB | WB | NB | SB |
|------------------------|----|------|-------|-------|
| HCM Control Delay, s/v | 0 | 4.86 | 61.58 | 64.84 |
| HCM LOS | | | F | F |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|------|-----|-----|------|-----|-----|-------|
| Capacity (veh/h) | 179 | 1129 | - | - | 729 | - | - | 68 |
| HCM Lane V/C Ratio | 0.696 | - | - | - | 0.32 | - | - | 0.123 |
| HCM Control Delay (s/veh) | 61.6 | 0 | - | - | 10.8 | 0 | - | 64.8 |
| HCM Lane LOS | F | A | - | - | B | A | - | F |
| HCM 95th %tile Q(veh) | 4.2 | 0 | - | - | 1.4 | - | - | 0.4 |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 9.3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 2 | 459 | 51 | 97 | 328 | 0 | 62 | 1 | 176 | 2 | 9 | 0 |
| Future Vol, veh/h | 2 | 459 | 51 | 97 | 328 | 0 | 62 | 1 | 176 | 2 | 9 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 13 | 13 | 13 | 8 | 8 | 8 | 0 | 0 | 0 |
| Mvmt Flow | 2 | 483 | 54 | 102 | 345 | 0 | 65 | 1 | 185 | 2 | 9 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|-------|-------|--------|------|-----|
| Conflicting Flow All | 345 | 0 | 0 | 537 | 0 | 0 | 1068 | 1064 | 510 | 1037 | 1091 | 345 |
| Stage 1 | - | - | - | - | - | - | 514 | 514 | - | 549 | 549 | - |
| Stage 2 | - | - | - | - | - | - | 554 | 549 | - | 488 | 541 | - |
| Critical Hdwy | 4.26 | - | - | 4.23 | - | - | 7.18 | 6.58 | 6.28 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.18 | 5.58 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.18 | 5.58 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.344 | - | - | 2.317 | - | - | 3.572 | 4.072 | 3.372 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1140 | - | - | 978 | - | - | 194 | 218 | 552 | 211 | 217 | 702 |
| Stage 1 | - | - | - | - | - | - | 532 | 525 | - | 523 | 519 | - |
| Stage 2 | - | - | - | - | - | - | 506 | 507 | - | 565 | 524 | - |
| Platoon blocked, % | | - | - | - | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1140 | - | - | 978 | - | - | 161 | 189 | 552 | 121 | 188 | 702 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 161 | 189 | - | 121 | 188 | - |
| Stage 1 | - | - | - | - | - | - | 531 | 524 | - | 456 | 452 | - |
| Stage 2 | - | - | - | - | - | - | 431 | 441 | - | 374 | 523 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|------------------------|------|--|--|------|--|--|-------|--|--|-------|--|--|
| HCM Control Delay, s/v | 0.03 | | | 2.08 | | | 41.35 | | | 27.57 | | |
| HCM LOS | | | | | | | E | | | D | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 337 | 7 | - | - | 411 | - | - | 171 |
| HCM Lane V/C Ratio | 0.746 | 0.002 | - | - | 0.104 | - | - | 0.068 |
| HCM Control Delay (s/veh) | 41.3 | 8.2 | 0 | - | 9.1 | 0 | - | 27.6 |
| HCM Lane LOS | E | A | A | - | A | A | - | D |
| HCM 95th %tile Q(veh) | 5.7 | 0 | - | - | 0.3 | - | - | 0.2 |

HCS Two-Lane Highway Report

Project Information

| | | | |
|---------------------|---|---------------|----------------|
| Analyst | Fathy Abdalla | Date | 9/29/2023 |
| Agency | KCA | Analysis Year | 2052 |
| Jurisdiction | Highlands County | Time Analyzed | AM |
| Project Description | SR 70 Widening from Lonesome Island Rd to CR 721 (No Build) | Units | U.S. Customary |

Segment 1

Vehicle Inputs

| | | | |
|--------------|--------------|-----------------------|-------|
| Segment Type | Passing Zone | Length, ft | 40600 |
| Measured FFS | Measured | Free-Flow Speed, mi/h | 60.0 |

Demand and Capacity

| | | | |
|-------------------------------------|------|----------------------------------|-------|
| Directional Demand Flow Rate, veh/h | 646 | Opposing Demand Flow Rate, veh/h | 621 |
| Peak Hour Factor | 0.95 | Total Trucks, % | 14.70 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.38 |

Intermediate Results

| | | | |
|-----------------------------------|----------|----------------------------------|---------|
| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 60.0 |
| Speed Slope Coefficient (m) | 3.54905 | Speed Power Coefficient (p) | 0.46759 |
| PF Slope Coefficient (m) | -1.27645 | PF Power Coefficient (p) | 0.76142 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 6.8 |
| %Improvement to Percent Followers | 0.0 | %Improvement to Speed | 0.0 |

Subsegment Data

| # | Segment Type | Length, ft | Radius, ft | Superelevation, % | Average Speed, mi/h |
|---|--------------|------------|------------|-------------------|---------------------|
| 1 | Tangent | 40600 | - | - | 57.3 |

Vehicle Results

| | | | |
|------------------------------|------|--|------|
| Average Speed, mi/h | 57.3 | Percent Followers, % | 60.0 |
| Segment Travel Time, minutes | 8.05 | Follower Density (FD), followers/mi/ln | 6.8 |
| Vehicle LOS | C | | |

Facility Results

| T | VMT veh-mi/AP | VHD veh-h/p | Follower Density, followers/ mi/ln | LOS |
|---|------------------|----------------|---------------------------------------|-----|
| 1 | 1180 | 0.92 | 6.8 | C |

HCS Two-Lane Highway Report

Project Information

| | | | |
|---------------------|---|---------------|----------------|
| Analyst | Fathy Abdalla | Date | 9/29/2023 |
| Agency | KCA | Analysis Year | 2052 |
| Jurisdiction | Highlands County | Time Analyzed | PM |
| Project Description | SR 70 Widening from Lonesome Island Rd to CR 721 (No Build) | Units | U.S. Customary |

Segment 1

Vehicle Inputs

| | | | |
|--------------|--------------|-----------------------|-------|
| Segment Type | Passing Zone | Length, ft | 40600 |
| Measured FFS | Measured | Free-Flow Speed, mi/h | 60.0 |

Demand and Capacity

| | | | |
|-------------------------------------|------|----------------------------------|-------|
| Directional Demand Flow Rate, veh/h | 539 | Opposing Demand Flow Rate, veh/h | 447 |
| Peak Hour Factor | 0.95 | Total Trucks, % | 14.70 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.32 |

Intermediate Results

| | | | |
|-----------------------------------|----------|----------------------------------|---------|
| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 60.0 |
| Speed Slope Coefficient (m) | 4.48557 | Speed Power Coefficient (p) | 0.48947 |
| PF Slope Coefficient (m) | -1.25928 | PF Power Coefficient (p) | 0.76897 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 5.1 |
| %Improvement to Percent Followers | 0.0 | %Improvement to Speed | 0.0 |

Subsegment Data

| # | Segment Type | Length, ft | Radius, ft | Superelevation, % | Average Speed, mi/h |
|---|--------------|------------|------------|-------------------|---------------------|
| 1 | Tangent | 40600 | - | - | 57.0 |

Vehicle Results

| | | | |
|------------------------------|------|--|------|
| Average Speed, mi/h | 57.0 | Percent Followers, % | 54.3 |
| Segment Travel Time, minutes | 8.09 | Follower Density (FD), followers/mi/ln | 5.1 |
| Vehicle LOS | C | | |

Facility Results

| T | VMT veh-mi/AP | VHD veh-h/p | Follower Density, followers/ mi/ln | LOS |
|---|------------------|----------------|---------------------------------------|-----|
| 1 | 984 | 0.86 | 5.1 | C |

Synchro, HCS LOS Computer Outputs Design Year 2032 Volumes - Build

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↵ | ↕↗ | | ↵ | ↕↗ | | | ↕↘ | | | ↕↘ | |
| Traffic Vol, veh/h | 2 | 314 | 9 | 8 | 271 | 0 | 5 | 0 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 2 | 314 | 9 | 8 | 271 | 0 | 5 | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | - | 300 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 16 | 16 | 16 | 0 | 0 | 100 | 0 | 0 | 0 |
| Mvmt Flow | 2 | 331 | 9 | 8 | 285 | 0 | 5 | 0 | 0 | 0 | 0 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|-----|-----|--------|-----|-----|
| Conflicting Flow All | 285 | 0 | 0 | 340 | 0 | 0 | 499 | 642 | 170 | 472 | 646 | 143 |
| Stage 1 | - | - | - | - | - | - | 339 | 339 | - | 302 | 302 | - |
| Stage 2 | - | - | - | - | - | - | 159 | 302 | - | 169 | 344 | - |
| Critical Hdwy | 4.42 | - | - | 4.42 | - | - | 7.5 | 6.5 | 8.9 | 7.5 | 6.5 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.5 | 5.5 | - | 6.5 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.5 | 5.5 | - | 6.5 | 5.5 | - |
| Follow-up Hdwy | 2.36 | - | - | 2.36 | - | - | 3.5 | 4 | 4.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1178 | - | - | 1121 | - | - | 459 | 395 | 608 | 480 | 393 | 885 |
| Stage 1 | - | - | - | - | - | - | 654 | 643 | - | 688 | 668 | - |
| Stage 2 | - | - | - | - | - | - | 833 | 668 | - | 822 | 640 | - |
| Platoon blocked, % | | - | - | | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1178 | - | - | 1121 | - | - | 455 | 392 | 608 | 476 | 389 | 885 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 455 | 392 | - | 476 | 389 | - |
| Stage 1 | - | - | - | - | - | - | 653 | 642 | - | 683 | 663 | - |
| Stage 2 | - | - | - | - | - | - | 826 | 663 | - | 820 | 639 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|------------------------|------|--|--|------|--|--|-------|--|--|----|--|--|
| HCM Control Delay, s/v | 0.05 | | | 0.24 | | | 13.01 | | | 0 | | |
| HCM LOS | | | | | | | B | | | A | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 455 | 1178 | - | - | 1121 | - | - | - |
| HCM Lane V/C Ratio | 0.012 | 0.002 | - | - | 0.008 | - | - | - |
| HCM Control Delay (s/veh) | 13 | 8.1 | - | - | 8.2 | - | - | 0 |
| HCM Lane LOS | B | A | - | - | A | - | - | A |
| HCM 95th %tile Q(veh) | 0 | 0 | - | - | 0 | - | - | - |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↵ | ↕ | | ↵ | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 0 | 348 | 3 | 6 | 318 | 2 | 11 | 1 | 1 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 348 | 3 | 6 | 318 | 2 | 11 | 1 | 1 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | - | 300 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 16 | 16 | 16 | 0 | 0 | 100 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 366 | 3 | 6 | 335 | 2 | 12 | 1 | 1 | 0 | 0 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|-----|-----|--------|-----|-----|
| Conflicting Flow All | 337 | 0 | 0 | 369 | 0 | 0 | 548 | 717 | 185 | 532 | 718 | 168 |
| Stage 1 | - | - | - | - | - | - | 368 | 368 | - | 348 | 348 | - |
| Stage 2 | - | - | - | - | - | - | 180 | 349 | - | 184 | 369 | - |
| Critical Hdwy | 4.42 | - | - | 4.42 | - | - | 7.5 | 6.5 | 8.9 | 7.5 | 6.5 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.5 | 5.5 | - | 6.5 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.5 | 5.5 | - | 6.5 | 5.5 | - |
| Follow-up Hdwy | 2.36 | - | - | 2.36 | - | - | 3.5 | 4 | 4.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1124 | - | - | 1091 | - | - | 424 | 358 | 591 | 435 | 357 | 852 |
| Stage 1 | - | - | - | - | - | - | 630 | 625 | - | 646 | 637 | - |
| Stage 2 | - | - | - | - | - | - | 810 | 637 | - | 806 | 624 | - |
| Platoon blocked, % | | - | - | - | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1124 | - | - | 1091 | - | - | 421 | 356 | 591 | 430 | 355 | 852 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 421 | 356 | - | 430 | 355 | - |
| Stage 1 | - | - | - | - | - | - | 630 | 625 | - | 643 | 634 | - |
| Stage 2 | - | - | - | - | - | - | 805 | 633 | - | 803 | 624 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|------------------------|----|--|--|------|--|--|-------|--|--|----|--|--|
| HCM Control Delay, s/v | 0 | | | 0.15 | | | 13.76 | | | 0 | | |
| HCM LOS | | | | | | | B | | | A | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 425 | 1124 | - | - | 1091 | - | - | - |
| HCM Lane V/C Ratio | 0.032 | - | - | - | 0.006 | - | - | - |
| HCM Control Delay (s/veh) | 13.8 | 0 | - | - | 8.3 | - | - | 0 |
| HCM Lane LOS | B | A | - | - | A | - | - | A |
| HCM 95th %tile Q(veh) | 0.1 | 0 | - | - | 0 | - | - | - |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 3.4 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↙ | ↑↑ | ↗ | ↙ | ↑↑ | ↗ | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 5 | 277 | 70 | 207 | 257 | 2 | 18 | 0 | 56 | 0 | 3 | 0 |
| Future Vol, veh/h | 5 | 277 | 70 | 207 | 257 | 2 | 18 | 0 | 56 | 0 | 3 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | 400 | 400 | - | 400 | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 13 | 13 | 13 | 8 | 8 | 8 | 0 | 0 | 0 |
| Mvmt Flow | 5 | 292 | 74 | 218 | 271 | 2 | 19 | 0 | 59 | 0 | 3 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|------|------|--------|------|-----|
| Conflicting Flow All | 273 | 0 | 0 | 365 | 0 | 0 | 875 | 1011 | 146 | 863 | 1082 | 135 |
| Stage 1 | - | - | - | - | - | - | 302 | 302 | - | 706 | 706 | - |
| Stage 2 | - | - | - | - | - | - | 573 | 708 | - | 156 | 376 | - |
| Critical Hdwy | 4.42 | - | - | 4.36 | - | - | 7.66 | 6.66 | 7.06 | 7.5 | 6.5 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.66 | 5.66 | - | 6.5 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.66 | 5.66 | - | 6.5 | 5.5 | - |
| Follow-up Hdwy | 2.36 | - | - | 2.33 | - | - | 3.58 | 4.08 | 3.38 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1192 | - | - | 1115 | - | - | 234 | 229 | 856 | 252 | 219 | 895 |
| Stage 1 | - | - | - | - | - | - | 666 | 648 | - | 397 | 441 | - |
| Stage 2 | - | - | - | - | - | - | 457 | 421 | - | 836 | 620 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1192 | - | - | 1115 | - | - | 185 | 183 | 856 | 188 | 176 | 895 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 185 | 183 | - | 188 | 176 | - |
| Stage 1 | - | - | - | - | - | - | 663 | 645 | - | 320 | 355 | - |
| Stage 2 | - | - | - | - | - | - | 365 | 339 | - | 775 | 617 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|-----------------------------|----|--|--|----|--|--|-------|--|--|-------|--|--|
| HCM Control Delay, s/v 0.11 | | | | 4 | | | 14.55 | | | 25.87 | | |
| HCM LOS | | | | | | | B | | | D | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 455 | 1192 | - | - | 1115 | - | - | 176 |
| HCM Lane V/C Ratio | 0.171 | 0.004 | - | - | 0.195 | - | - | 0.018 |
| HCM Control Delay (s/veh) | 14.6 | 8 | - | - | 9 | - | - | 25.9 |
| HCM Lane LOS | B | A | - | - | A | - | - | D |
| HCM 95th %tile Q(veh) | 0.6 | 0 | - | - | 0.7 | - | - | 0.1 |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 4.1 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↙ | ↑↑ | ↗ | ↙ | ↑↑ | ↗ | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 13 | 342 | 38 | 92 | 299 | 1 | 48 | 1 | 137 | 1 | 6 | 0 |
| Future Vol, veh/h | 13 | 342 | 38 | 92 | 299 | 1 | 48 | 1 | 137 | 1 | 6 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | 400 | 400 | - | 400 | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 13 | 13 | 13 | 8 | 8 | 8 | 0 | 0 | 0 |
| Mvmt Flow | 14 | 360 | 40 | 97 | 315 | 1 | 51 | 1 | 144 | 1 | 6 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|------|------|--------|-----|-----|
| Conflicting Flow All | 316 | 0 | 0 | 400 | 0 | 0 | 742 | 897 | 180 | 716 | 936 | 157 |
| Stage 1 | - | - | - | - | - | - | 387 | 387 | - | 508 | 508 | - |
| Stage 2 | - | - | - | - | - | - | 354 | 509 | - | 208 | 427 | - |
| Critical Hdwy | 4.42 | - | - | 4.36 | - | - | 7.66 | 6.66 | 7.06 | 7.5 | 6.5 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.66 | 5.66 | - | 6.5 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.66 | 5.66 | - | 6.5 | 5.5 | - |
| Follow-up Hdwy | 2.36 | - | - | 2.33 | - | - | 3.58 | 4.08 | 3.38 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1146 | - | - | 1080 | - | - | 293 | 267 | 813 | 321 | 267 | 866 |
| Stage 1 | - | - | - | - | - | - | 592 | 593 | - | 521 | 542 | - |
| Stage 2 | - | - | - | - | - | - | 620 | 521 | - | 780 | 588 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1146 | - | - | 1080 | - | - | 258 | 241 | 813 | 237 | 240 | 866 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 258 | 241 | - | 237 | 240 | - |
| Stage 1 | - | - | - | - | - | - | 585 | 586 | - | 474 | 493 | - |
| Stage 2 | - | - | - | - | - | - | 557 | 475 | - | 633 | 581 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|------------------------|------|--|--|------|--|--|------|--|--|-------|--|--|
| HCM Control Delay, s/v | 0.27 | | | 2.03 | | | 16.1 | | | 20.49 | | |
| HCM LOS | | | | | | | C | | | C | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-------|-----|-----|------|-----|-----|-------|
| Capacity (veh/h) | 518 | 1146 | - | - | 1080 | - | - | 240 |
| HCM Lane V/C Ratio | 0.378 | 0.012 | - | - | 0.09 | - | - | 0.031 |
| HCM Control Delay (s/veh) | 16.1 | 8.2 | - | - | 8.7 | - | - | 20.5 |
| HCM Lane LOS | C | A | - | - | A | - | - | C |
| HCM 95th %tile Q(veh) | 1.7 | 0 | - | - | 0.3 | - | - | 0.1 |

HCS Multilane Highway Report

Project Information

| | | | |
|---------------------|--|---------------|----------------|
| Analyst | Fathy Abdalla | Date | 9/29/2023 |
| Agency | KCA | Analysis Year | 2032 |
| Jurisdiction | Highlands County | Time Analyzed | AM |
| Project Description | SR 70 Widening from Lonesome Island Rd to CR 721 (Build) | Units | U.S. Customary |

Direction 1 Geometric Data

| | | | |
|-----------------------------------|------------|---------------------------------------|-------|
| Direction 1 | SR 70 - WB | | |
| Number of Lanes (N), ln | 2 | Terrain Type | Level |
| Measured or Base Free-Flow Speed | Measured | Percent Grade, % | - |
| Base Free-Flow Speed (BFFS), mi/h | - | Grade Length, mi | - |
| Lane Width, ft | - | Access Point Density, pts/mi | - |
| Median Type | - | Left-Side Lateral Clearance (LCR), ft | - |
| Free-Flow Speed (FFS), mi/h | 65.0 | Total Lateral Clearance (TLC), ft | - |

Direction 1 Adjustment Factors

| | | | |
|-----------------------|--------------|--|-------|
| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| Driver Population SAF | 1.000 | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Driver Population CAF | 1.000 | | |

Direction 1 Demand and Capacity

| | | | |
|-----------------------------|-------|---------------------------------------|-------|
| Volume (V) veh/h | 466 | Heavy Vehicle Adjustment Factor (fhv) | 0.872 |
| Peak Hour Factor | 0.95 | Flow Rate (Vp), pc/h/ln | 282 |
| Total Trucks, % | 14.70 | Capacity (c), pc/h/ln | 2300 |
| Single-Unit Trucks (SUT), % | - | Adjusted Capacity (cadj), pc/h/ln | 2300 |
| Tractor-Trailers (TT), % | - | Volume-to-Capacity Ratio (v/c) | 0.12 |

Direction 1 Speed and Density

| | | | |
|--------------------------------------|---|-------------------------|------|
| Lane Width Adjustment (fLW) | - | Average Speed (S), mi/h | 65.0 |
| Total Lateral Clearance Adj. (fLLC) | - | Density (D), pc/mi/ln | 4.3 |
| Median Type Adjustment (fM) | - | Level of Service (LOS) | A |
| Access Point Density Adjustment (fA) | - | | |

| Direction 2 Geometric Data | | | |
|--|--------------|--|-------|
| Direction 2 | SR 70 - EB | | |
| Number of Lanes (N), ln | 2 | Terrain Type | Level |
| Measured or Base Free-Flow Speed | Measured | Percent Grade, % | - |
| Base Free-Flow Speed (BFFS), mi/h | - | Grade Length, mi | - |
| Lane Width, ft | - | Access Point Density, pts/mi | - |
| Median Type | - | Left-Side Lateral Clearance (LCR), ft | - |
| Free-Flow Speed (FFS), mi/h | 65.0 | Total Lateral Clearance (TLC), ft | - |
| Direction 2 Adjustment Factors | | | |
| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| Driver Population SAF | 1.000 | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Driver Population CAF | 1.000 | | |
| Direction 2 Demand and Capacity | | | |
| Volume (V) veh/h | 352 | Heavy Vehicle Adjustment Factor (fHV) | 0.872 |
| Peak Hour Factor | 0.95 | Flow Rate (Vp), pc/h/ln | 212 |
| Total Trucks, % | 14.70 | Capacity (c), pc/h/ln | 2300 |
| Single-Unit Trucks (SUT), % | - | Adjusted Capacity (cadj), pc/h/ln | 2300 |
| Tractor-Trailers (TT), % | - | Volume-to-Capacity Ratio (v/c) | 0.09 |
| Direction 2 Speed and Density | | | |
| Lane Width Adjustment (fLW) | - | Average Speed (S), mi/h | 65.0 |
| Total Lateral Clearance Adj. (fLLC) | - | Density (D), pc/mi/ln | 3.3 |
| Median Type Adjustment (fM) | - | Level of Service (LOS) | A |
| Access Point Density Adjustment (fA) | - | | |

HCS Multilane Highway Report

Project Information

| | | | |
|---------------------|--|---------------|----------------|
| Analyst | Fathy Abdalla | Date | 9/29/2023 |
| Agency | KCA | Analysis Year | 2032 |
| Jurisdiction | Highlands County | Time Analyzed | PM |
| Project Description | SR 70 Widening from Lonesome Island Rd to CR 721 (Build) | Units | U.S. Customary |

Direction 1 Geometric Data

| | | | |
|-----------------------------------|------------|---------------------------------------|-------|
| Direction 1 | SR 70 - WB | | |
| Number of Lanes (N), ln | 2 | Terrain Type | Level |
| Measured or Base Free-Flow Speed | Measured | Percent Grade, % | - |
| Base Free-Flow Speed (BFFS), mi/h | - | Grade Length, mi | - |
| Lane Width, ft | - | Access Point Density, pts/mi | - |
| Median Type | - | Left-Side Lateral Clearance (LCR), ft | - |
| Free-Flow Speed (FFS), mi/h | 65.0 | Total Lateral Clearance (TLC), ft | - |

Direction 1 Adjustment Factors

| | | | |
|-----------------------|--------------|--|-------|
| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| Driver Population SAF | 1.000 | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Driver Population CAF | 1.000 | | |

Direction 1 Demand and Capacity

| | | | |
|-----------------------------|-------|---------------------------------------|-------|
| Volume (V) veh/h | 392 | Heavy Vehicle Adjustment Factor (fHV) | 0.872 |
| Peak Hour Factor | 0.95 | Flow Rate (Vp), pc/h/ln | 236 |
| Total Trucks, % | 14.70 | Capacity (c), pc/h/ln | 2300 |
| Single-Unit Trucks (SUT), % | - | Adjusted Capacity (cadj), pc/h/ln | 2300 |
| Tractor-Trailers (TT), % | - | Volume-to-Capacity Ratio (v/c) | 0.10 |

Direction 1 Speed and Density

| | | | |
|--------------------------------------|---|-------------------------|------|
| Lane Width Adjustment (fLW) | - | Average Speed (S), mi/h | 65.0 |
| Total Lateral Clearance Adj. (fLLC) | - | Density (D), pc/mi/ln | 3.6 |
| Median Type Adjustment (fM) | - | Level of Service (LOS) | A |
| Access Point Density Adjustment (fA) | - | | |

| Direction 2 Geometric Data | | | |
|--|--------------|--|-------|
| Direction 2 | SR 70 - EB | | |
| Number of Lanes (N), ln | 2 | Terrain Type | Level |
| Measured or Base Free-Flow Speed | Measured | Percent Grade, % | - |
| Base Free-Flow Speed (BFFS), mi/h | - | Grade Length, mi | - |
| Lane Width, ft | - | Access Point Density, pts/mi | - |
| Median Type | - | Left-Side Lateral Clearance (LCR), ft | - |
| Free-Flow Speed (FFS), mi/h | 65.0 | Total Lateral Clearance (TLC), ft | - |
| Direction 2 Adjustment Factors | | | |
| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| Driver Population SAF | 1.000 | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Driver Population CAF | 1.000 | | |
| Direction 2 Demand and Capacity | | | |
| Volume (V) veh/h | 393 | Heavy Vehicle Adjustment Factor (fHV) | 0.872 |
| Peak Hour Factor | 0.95 | Flow Rate (Vp), pc/h/ln | 237 |
| Total Trucks, % | 14.70 | Capacity (c), pc/h/ln | 2300 |
| Single-Unit Trucks (SUT), % | - | Adjusted Capacity (cadj), pc/h/ln | 2300 |
| Tractor-Trailers (TT), % | - | Volume-to-Capacity Ratio (v/c) | 0.10 |
| Direction 2 Speed and Density | | | |
| Lane Width Adjustment (fLW) | - | Average Speed (S), mi/h | 65.0 |
| Total Lateral Clearance Adj. (fLLC) | - | Density (D), pc/mi/ln | 3.6 |
| Median Type Adjustment (fM) | - | Level of Service (LOS) | A |
| Access Point Density Adjustment (fA) | - | | |

Synchro, HCS LOS Computer Outputs Design Year 2052 Volumes - Build

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↵ | ↕↗ | | ↵ | ↕↗ | | | ↕↗ | | | ↕↗ | |
| Traffic Vol, veh/h | 4 | 608 | 18 | 16 | 537 | 0 | 9 | 0 | 1 | 0 | 0 | 0 |
| Future Vol, veh/h | 4 | 608 | 18 | 16 | 537 | 0 | 9 | 0 | 1 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | - | 300 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 16 | 16 | 16 | 0 | 0 | 100 | 0 | 0 | 0 |
| Mvmt Flow | 4 | 640 | 19 | 17 | 565 | 0 | 9 | 0 | 1 | 0 | 0 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|------|-----|--------|------|-----|
| Conflicting Flow All | 565 | 0 | 0 | 659 | 0 | 0 | 974 | 1257 | 329 | 927 | 1266 | 283 |
| Stage 1 | - | - | - | - | - | - | 658 | 658 | - | 599 | 599 | - |
| Stage 2 | - | - | - | - | - | - | 316 | 599 | - | 328 | 667 | - |
| Critical Hdwy | 4.42 | - | - | 4.42 | - | - | 7.5 | 6.5 | 8.9 | 7.5 | 6.5 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.5 | 5.5 | - | 6.5 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.5 | 5.5 | - | 6.5 | 5.5 | - |
| Follow-up Hdwy | 2.36 | - | - | 2.36 | - | - | 3.5 | 4 | 4.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 912 | - | - | 836 | - | - | 209 | 173 | 448 | 226 | 170 | 720 |
| Stage 1 | - | - | - | - | - | - | 424 | 464 | - | 460 | 494 | - |
| Stage 2 | - | - | - | - | - | - | 675 | 494 | - | 664 | 460 | - |
| Platoon blocked, % | | - | - | - | - | - | | | | | | |
| Mov Cap-1 Maneuver | 912 | - | - | 836 | - | - | 204 | 168 | 448 | 220 | 166 | 720 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 204 | 168 | - | 220 | 166 | - |
| Stage 1 | - | - | - | - | - | - | 423 | 462 | - | 451 | 484 | - |
| Stage 2 | - | - | - | - | - | - | 661 | 484 | - | 659 | 458 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|------------------------|------|--|--|------|--|--|-------|--|--|----|--|--|
| HCM Control Delay, s/v | 0.06 | | | 0.27 | | | 22.54 | | | 0 | | |
| HCM LOS | | | | | | | C | | | A | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-------|-----|-----|------|-----|-----|-------|
| Capacity (veh/h) | 216 | 912 | - | - | 836 | - | - | - |
| HCM Lane V/C Ratio | 0.049 | 0.005 | - | - | 0.02 | - | - | - |
| HCM Control Delay (s/veh) | 22.5 | 9 | - | - | 9.4 | - | - | 0 |
| HCM Lane LOS | C | A | - | - | A | - | - | A |
| HCM 95th %tile Q(veh) | 0.2 | 0 | - | - | 0.1 | - | - | - |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.5 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↵ | ↕ | | ↵ | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 0 | 623 | 6 | 11 | 552 | 3 | 16 | 2 | 3 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 623 | 6 | 11 | 552 | 3 | 16 | 2 | 3 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | - | 300 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 16 | 16 | 16 | 0 | 0 | 100 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 656 | 6 | 12 | 581 | 3 | 17 | 2 | 3 | 0 | 0 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|------|-----|--------|------|-----|
| Conflicting Flow All | 584 | 0 | 0 | 662 | 0 | 0 | 973 | 1266 | 331 | 935 | 1268 | 292 |
| Stage 1 | - | - | - | - | - | - | 659 | 659 | - | 606 | 606 | - |
| Stage 2 | - | - | - | - | - | - | 314 | 607 | - | 329 | 662 | - |
| Critical Hdwy | 4.42 | - | - | 4.42 | - | - | 7.5 | 6.5 | 8.9 | 7.5 | 6.5 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.5 | 5.5 | - | 6.5 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.5 | 5.5 | - | 6.5 | 5.5 | - |
| Follow-up Hdwy | 2.36 | - | - | 2.36 | - | - | 3.5 | 4 | 4.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 896 | - | - | 834 | - | - | 210 | 170 | 447 | 223 | 170 | 710 |
| Stage 1 | - | - | - | - | - | - | 424 | 464 | - | 456 | 490 | - |
| Stage 2 | - | - | - | - | - | - | 677 | 489 | - | 664 | 462 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 896 | - | - | 834 | - | - | 207 | 168 | 447 | 216 | 168 | 710 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 207 | 168 | - | 216 | 168 | - |
| Stage 1 | - | - | - | - | - | - | 424 | 464 | - | 450 | 483 | - |
| Stage 2 | - | - | - | - | - | - | 668 | 483 | - | 656 | 462 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|------------------------|----|--|--|------|--|--|------|--|--|----|--|--|
| HCM Control Delay, s/v | 0 | | | 0.18 | | | 23.3 | | | 0 | | |
| HCM LOS | | | | | | | C | | | A | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-----|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 219 | 896 | - | - | 834 | - | - | - |
| HCM Lane V/C Ratio | 0.101 | - | - | - | 0.014 | - | - | - |
| HCM Control Delay (s/veh) | 23.3 | 0 | - | - | 9.4 | - | - | 0 |
| HCM Lane LOS | C | A | - | - | A | - | - | A |
| HCM 95th %tile Q(veh) | 0.3 | 0 | - | - | 0 | - | - | - |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 29 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↘ | ↗ | ↗ | ↘ | ↗ | ↗ | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 10 | 582 | 147 | 361 | 447 | 3 | 31 | 0 | 110 | 0 | 8 | 0 |
| Future Vol, veh/h | 10 | 582 | 147 | 361 | 447 | 3 | 31 | 0 | 110 | 0 | 8 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | 400 | 400 | - | 400 | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 13 | 13 | 13 | 8 | 8 | 8 | 0 | 0 | 0 |
| Mvmt Flow | 11 | 613 | 155 | 380 | 471 | 3 | 33 | 0 | 116 | 0 | 8 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|------|------|--------|------|-----|
| Conflicting Flow All | 474 | 0 | 0 | 767 | 0 | 0 | 1633 | 1867 | 306 | 1558 | 2019 | 235 |
| Stage 1 | - | - | - | - | - | - | 634 | 634 | - | 1231 | 1231 | - |
| Stage 2 | - | - | - | - | - | - | 999 | 1234 | - | 327 | 788 | - |
| Critical Hdwy | 4.42 | - | - | 4.36 | - | - | 7.66 | 6.66 | 7.06 | 7.5 | 6.5 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.66 | 5.66 | - | 6.5 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.66 | 5.66 | - | 6.5 | 5.5 | - |
| Follow-up Hdwy | 2.36 | - | - | 2.33 | - | - | 3.58 | 4.08 | 3.38 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 992 | - | - | 774 | - | - | 63 | 67 | 672 | 78 | 59 | 773 |
| Stage 1 | - | - | - | - | - | - | 420 | 457 | - | 191 | 252 | - |
| Stage 2 | - | - | - | - | - | - | 250 | 236 | - | 665 | 405 | - |
| Platoon blocked, % | | - | - | - | - | - | | | | | | |
| Mov Cap-1 Maneuver | 992 | - | - | 774 | - | - | ~ 26 | 34 | 672 | 32 | 30 | 773 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | ~ 26 | 34 | - | 32 | 30 | - |
| Stage 1 | - | - | - | - | - | - | 415 | 452 | - | 97 | 128 | - |
| Stage 2 | - | - | - | - | - | - | 119 | 120 | - | 545 | 401 | - |

| Approach | EB | WB | NB | SB |
|------------------------|------|------|-----------|--------|
| HCM Control Delay, s/v | 0.12 | 6.26 | \$ 303.49 | 168.59 |
| HCM LOS | | | F | F |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|----------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 106 | 992 | - | - | 774 | - | - | 30 |
| HCM Lane V/C Ratio | 1.406 | 0.011 | - | - | 0.491 | - | - | 0.284 |
| HCM Control Delay (s/veh) | \$ 303.5 | 8.7 | - | - | 14.1 | - | - | 168.6 |
| HCM Lane LOS | F | A | - | - | B | - | - | F |
| HCM 95th %tile Q(veh) | 10.6 | 0 | - | - | 2.7 | - | - | 0.9 |

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 19.5 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↘ | ↑↑ | ↗ | ↘ | ↑↑ | ↗ | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 24 | 639 | 71 | 141 | 463 | 2 | 62 | 1 | 176 | 2 | 9 | 0 |
| Future Vol, veh/h | 24 | 639 | 71 | 141 | 463 | 2 | 62 | 1 | 176 | 2 | 9 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | 400 | 400 | - | 400 | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 13 | 13 | 13 | 8 | 8 | 8 | 0 | 0 | 0 |
| Mvmt Flow | 25 | 673 | 75 | 148 | 487 | 2 | 65 | 1 | 185 | 2 | 9 | 0 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|------|------|--------|------|-----|
| Conflicting Flow All | 489 | 0 | 0 | 747 | 0 | 0 | 1268 | 1509 | 336 | 1172 | 1582 | 244 |
| Stage 1 | - | - | - | - | - | - | 723 | 723 | - | 784 | 784 | - |
| Stage 2 | - | - | - | - | - | - | 545 | 786 | - | 387 | 798 | - |
| Critical Hdwy | 4.42 | - | - | 4.36 | - | - | 7.66 | 6.66 | 7.06 | 7.5 | 6.5 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.66 | 5.66 | - | 6.5 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.66 | 5.66 | - | 6.5 | 5.5 | - |
| Follow-up Hdwy | 2.36 | - | - | 2.33 | - | - | 3.58 | 4.08 | 3.38 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 978 | - | - | 788 | - | - | 119 | 113 | 642 | 150 | 110 | 763 |
| Stage 1 | - | - | - | - | - | - | 370 | 415 | - | 357 | 407 | - |
| Stage 2 | - | - | - | - | - | - | 475 | 387 | - | 613 | 401 | - |
| Platoon blocked, % | | - | - | | - | - | | | | | | |
| Mov Cap-1 Maneuver | 978 | - | - | 788 | - | - | 86 | 89 | 642 | 84 | 87 | 763 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 86 | 89 | - | 84 | 87 | - |
| Stage 1 | - | - | - | - | - | - | 360 | 404 | - | 290 | 330 | - |
| Stage 2 | - | - | - | - | - | - | 375 | 314 | - | 424 | 391 | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|------------------------|------|--|--|------|--|--|--------|--|--|------|--|--|
| HCM Control Delay, s/v | 0.29 | | | 2.47 | | | 119.99 | | | 53.1 | | |
| HCM LOS | | | | | | | F | | | F | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 237 | 978 | - | - | 788 | - | - | 86 |
| HCM Lane V/C Ratio | 1.061 | 0.026 | - | - | 0.188 | - | - | 0.134 |
| HCM Control Delay (s/veh) | 120 | 8.8 | - | - | 10.6 | - | - | 53.1 |
| HCM Lane LOS | F | A | - | - | B | - | - | F |
| HCM 95th %tile Q(veh) | 10.7 | 0.1 | - | - | 0.7 | - | - | 0.4 |

HCS Multilane Highway Report

Project Information

| | | | |
|---------------------|--|---------------|----------------|
| Analyst | Fathy Abdalla | Date | 9/29/2023 |
| Agency | KCA | Analysis Year | 2052 |
| Jurisdiction | Highlands County | Time Analyzed | AM |
| Project Description | SR 70 Widening from Lonesome Island Rd to CR 721 (Build) | Units | U.S. Customary |

Direction 1 Geometric Data

| | | | |
|-----------------------------------|------------|---------------------------------------|-------|
| Direction 1 | SR 70 - WB | | |
| Number of Lanes (N), ln | 2 | Terrain Type | Level |
| Measured or Base Free-Flow Speed | Measured | Percent Grade, % | - |
| Base Free-Flow Speed (BFFS), mi/h | - | Grade Length, mi | - |
| Lane Width, ft | - | Access Point Density, pts/mi | - |
| Median Type | - | Left-Side Lateral Clearance (LCR), ft | - |
| Free-Flow Speed (FFS), mi/h | 65.0 | Total Lateral Clearance (TLC), ft | - |

Direction 1 Adjustment Factors

| | | | |
|-----------------------|--------------|--|-------|
| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| Driver Population SAF | 1.000 | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Driver Population CAF | 1.000 | | |

Direction 1 Demand and Capacity

| | | | |
|-----------------------------|-------|---------------------------------------|-------|
| Volume (V) veh/h | 811 | Heavy Vehicle Adjustment Factor (fHV) | 0.872 |
| Peak Hour Factor | 0.95 | Flow Rate (Vp), pc/h/ln | 490 |
| Total Trucks, % | 14.70 | Capacity (c), pc/h/ln | 2300 |
| Single-Unit Trucks (SUT), % | - | Adjusted Capacity (cadj), pc/h/ln | 2300 |
| Tractor-Trailers (TT), % | - | Volume-to-Capacity Ratio (v/c) | 0.21 |

Direction 1 Speed and Density

| | | | |
|--------------------------------------|---|-------------------------|------|
| Lane Width Adjustment (fLW) | - | Average Speed (S), mi/h | 65.0 |
| Total Lateral Clearance Adj. (fLLC) | - | Density (D), pc/mi/ln | 7.5 |
| Median Type Adjustment (fM) | - | Level of Service (LOS) | A |
| Access Point Density Adjustment (fA) | - | | |

| Direction 2 Geometric Data | | | |
|--|--------------|--|-------|
| Direction 2 | SR 70 - EB | | |
| Number of Lanes (N), ln | 2 | Terrain Type | Level |
| Measured or Base Free-Flow Speed | Measured | Percent Grade, % | - |
| Base Free-Flow Speed (BFFS), mi/h | - | Grade Length, mi | - |
| Lane Width, ft | - | Access Point Density, pts/mi | - |
| Median Type | - | Left-Side Lateral Clearance (LCR), ft | - |
| Free-Flow Speed (FFS), mi/h | 65.0 | Total Lateral Clearance (TLC), ft | - |
| Direction 2 Adjustment Factors | | | |
| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| Driver Population SAF | 1.000 | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Driver Population CAF | 1.000 | | |
| Direction 2 Demand and Capacity | | | |
| Volume (V) veh/h | 739 | Heavy Vehicle Adjustment Factor (fHV) | 0.872 |
| Peak Hour Factor | 0.95 | Flow Rate (Vp), pc/h/ln | 446 |
| Total Trucks, % | 14.70 | Capacity (c), pc/h/ln | 2300 |
| Single-Unit Trucks (SUT), % | - | Adjusted Capacity (cadj), pc/h/ln | 2300 |
| Tractor-Trailers (TT), % | - | Volume-to-Capacity Ratio (v/c) | 0.19 |
| Direction 2 Speed and Density | | | |
| Lane Width Adjustment (fLW) | - | Average Speed (S), mi/h | 65.0 |
| Total Lateral Clearance Adj. (fLLC) | - | Density (D), pc/mi/ln | 6.9 |
| Median Type Adjustment (fM) | - | Level of Service (LOS) | A |
| Access Point Density Adjustment (fA) | - | | |

HCS Multilane Highway Report

Project Information

| | | | |
|---------------------|--|---------------|----------------|
| Analyst | Fathy Abdalla | Date | 9/29/2023 |
| Agency | KCA | Analysis Year | 2052 |
| Jurisdiction | Highlands County | Time Analyzed | PM |
| Project Description | SR 70 Widening from Lonesome Island Rd to CR 721 (Build) | Units | U.S. Customary |

Direction 1 Geometric Data

| | | | |
|-----------------------------------|------------|---------------------------------------|-------|
| Direction 1 | SR 70 - WB | | |
| Number of Lanes (N), ln | 2 | Terrain Type | Level |
| Measured or Base Free-Flow Speed | Measured | Percent Grade, % | - |
| Base Free-Flow Speed (BFFS), mi/h | - | Grade Length, mi | - |
| Lane Width, ft | - | Access Point Density, pts/mi | - |
| Median Type | - | Left-Side Lateral Clearance (LCR), ft | - |
| Free-Flow Speed (FFS), mi/h | 65.0 | Total Lateral Clearance (TLC), ft | - |

Direction 1 Adjustment Factors

| | | | |
|-----------------------|--------------|--|-------|
| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| Driver Population SAF | 1.000 | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Driver Population CAF | 1.000 | | |

Direction 1 Demand and Capacity

| | | | |
|-----------------------------|-------|---------------------------------------|-------|
| Volume (V) veh/h | 606 | Heavy Vehicle Adjustment Factor (fhv) | 0.872 |
| Peak Hour Factor | 0.95 | Flow Rate (Vp), pc/h/ln | 366 |
| Total Trucks, % | 14.70 | Capacity (c), pc/h/ln | 2300 |
| Single-Unit Trucks (SUT), % | - | Adjusted Capacity (cadj), pc/h/ln | 2300 |
| Tractor-Trailers (TT), % | - | Volume-to-Capacity Ratio (v/c) | 0.16 |

Direction 1 Speed and Density

| | | | |
|--------------------------------------|---|-------------------------|------|
| Lane Width Adjustment (fLW) | - | Average Speed (S), mi/h | 65.0 |
| Total Lateral Clearance Adj. (fLLC) | - | Density (D), pc/mi/ln | 5.6 |
| Median Type Adjustment (fM) | - | Level of Service (LOS) | A |
| Access Point Density Adjustment (fA) | - | | |

| Direction 2 Geometric Data | | | |
|--|--------------|--|-------|
| Direction 2 | SR 70 - EB | | |
| Number of Lanes (N), ln | 2 | Terrain Type | Level |
| Measured or Base Free-Flow Speed | Measured | Percent Grade, % | - |
| Base Free-Flow Speed (BFFS), mi/h | - | Grade Length, mi | - |
| Lane Width, ft | - | Access Point Density, pts/mi | - |
| Median Type | - | Left-Side Lateral Clearance (LCR), ft | - |
| Free-Flow Speed (FFS), mi/h | 65.0 | Total Lateral Clearance (TLC), ft | - |
| Direction 2 Adjustment Factors | | | |
| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| Driver Population SAF | 1.000 | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Driver Population CAF | 1.000 | | |
| Direction 2 Demand and Capacity | | | |
| Volume (V) veh/h | 734 | Heavy Vehicle Adjustment Factor (fHV) | 0.872 |
| Peak Hour Factor | 0.95 | Flow Rate (Vp), pc/h/ln | 443 |
| Total Trucks, % | 14.70 | Capacity (c), pc/h/ln | 2300 |
| Single-Unit Trucks (SUT), % | - | Adjusted Capacity (cadj), pc/h/ln | 2300 |
| Tractor-Trailers (TT), % | - | Volume-to-Capacity Ratio (v/c) | 0.19 |
| Direction 2 Speed and Density | | | |
| Lane Width Adjustment (fLW) | - | Average Speed (S), mi/h | 65.0 |
| Total Lateral Clearance Adj. (fLLC) | - | Density (D), pc/mi/ln | 6.8 |
| Median Type Adjustment (fM) | - | Level of Service (LOS) | A |
| Access Point Density Adjustment (fA) | - | | |

Synchro, HCS LOS Computer Outputs Design Year 2052 Volumes - RCUT Build

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 4.1 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↘ | ↑↑ | ↗ | ↘ | ↑↑ | ↗ | | | ↗ | | | ↗ |
| Traffic Vol, veh/h | 10 | 582 | 147 | 361 | 447 | 3 | 0 | 0 | 141 | 0 | 0 | 8 |
| Future Vol, veh/h | 10 | 582 | 147 | 361 | 447 | 3 | 0 | 0 | 141 | 0 | 0 | 8 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | 400 | 400 | - | 400 | - | - | 0 | - | - | 0 |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 13 | 13 | 13 | 8 | 8 | 8 | 0 | 0 | 0 |
| Mvmt Flow | 11 | 613 | 155 | 380 | 471 | 3 | 0 | 0 | 148 | 0 | 0 | 8 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|--------|---|---|--------|---|------|--------|---|-----|
| Conflicting Flow All | 474 | 0 | 0 | 767 | 0 | 0 | - | - | 306 | - | - | 235 |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | - | - | - | - | - | - |
| Critical Hdwy | 4.42 | - | - | 4.36 | - | - | - | - | 7.06 | - | - | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | - | - | - | - | - | - |
| Follow-up Hdwy | 2.36 | - | - | 2.33 | - | - | - | - | 3.38 | - | - | 3.3 |
| Pot Cap-1 Maneuver | 992 | - | - | 774 | - | - | 0 | 0 | 672 | 0 | 0 | 773 |
| Stage 1 | - | - | - | - | - | - | 0 | 0 | - | 0 | 0 | - |
| Stage 2 | - | - | - | - | - | - | 0 | 0 | - | 0 | 0 | - |
| Platoon blocked, % | | - | - | - | - | - | | | | | | |
| Mov Cap-1 Maneuver | 992 | - | - | 774 | - | - | - | - | 672 | - | - | 773 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | - | - | - | - | - | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|------------------------|------|--|--|------|--|--|-------|--|--|------|--|--|
| HCM Control Delay, s/v | 0.12 | | | 6.26 | | | 11.87 | | | 9.71 | | |
| HCM LOS | | | | | | | B | | | A | | |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 672 | 992 | - | - | 774 | - | - | 773 |
| HCM Lane V/C Ratio | 0.221 | 0.011 | - | - | 0.491 | - | - | 0.011 |
| HCM Control Delay (s/veh) | 11.9 | 8.7 | - | - | 14.1 | - | - | 9.7 |
| HCM Lane LOS | B | A | - | - | B | - | - | A |
| HCM 95th %tile Q(veh) | 0.8 | 0 | - | - | 2.7 | - | - | 0 |

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↘ | ↗ | ↗ | ↘ | ↗ | ↗ | | | ↗ | | | ↗ |
| Traffic Vol, veh/h | 24 | 639 | 71 | 141 | 463 | 2 | 0 | 0 | 216 | 0 | 0 | 11 |
| Future Vol, veh/h | 24 | 639 | 71 | 141 | 463 | 2 | 0 | 0 | 216 | 0 | 0 | 11 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 400 | - | 400 | 400 | - | 400 | - | - | 0 | - | - | 0 |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 16 | 16 | 16 | 13 | 13 | 13 | 8 | 8 | 8 | 0 | 0 | 0 |
| Mvmt Flow | 25 | 673 | 75 | 148 | 487 | 2 | 0 | 0 | 227 | 0 | 0 | 12 |

| Major/Minor | Major1 | | Major2 | | Minor1 | | | Minor2 | | | | |
|----------------------|--------|---|--------|------|--------|---|---|--------|------|---|---|-----|
| Conflicting Flow All | 489 | 0 | 0 | 747 | 0 | 0 | - | - | 336 | - | - | 244 |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | - | - | - | - | - | - |
| Critical Hdwy | 4.42 | - | - | 4.36 | - | - | - | - | 7.06 | - | - | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | - | - | - | - | - | - |
| Follow-up Hdwy | 2.36 | - | - | 2.33 | - | - | - | - | 3.38 | - | - | 3.3 |
| Pot Cap-1 Maneuver | 978 | - | - | 788 | - | - | 0 | 0 | 642 | 0 | 0 | 763 |
| Stage 1 | - | - | - | - | - | - | 0 | 0 | - | 0 | 0 | - |
| Stage 2 | - | - | - | - | - | - | 0 | 0 | - | 0 | 0 | - |
| Platoon blocked, % | | - | - | - | - | - | | | | | | |
| Mov Cap-1 Maneuver | 978 | - | - | 788 | - | - | - | - | 642 | - | - | 763 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | - | - | - | - | - | - |

| Approach | EB | WB | NB | SB |
|------------------------|------|------|-------|------|
| HCM Control Delay, s/v | 0.29 | 2.47 | 13.65 | 9.79 |
| HCM LOS | | | B | A |

| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|---------------------------|-------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 642 | 978 | - | - | 788 | - | - | 763 |
| HCM Lane V/C Ratio | 0.354 | 0.026 | - | - | 0.188 | - | - | 0.015 |
| HCM Control Delay (s/veh) | 13.6 | 8.8 | - | - | 10.6 | - | - | 9.8 |
| HCM Lane LOS | B | A | - | - | B | - | - | A |
| HCM 95th %tile Q(veh) | 1.6 | 0.1 | - | - | 0.7 | - | - | 0 |

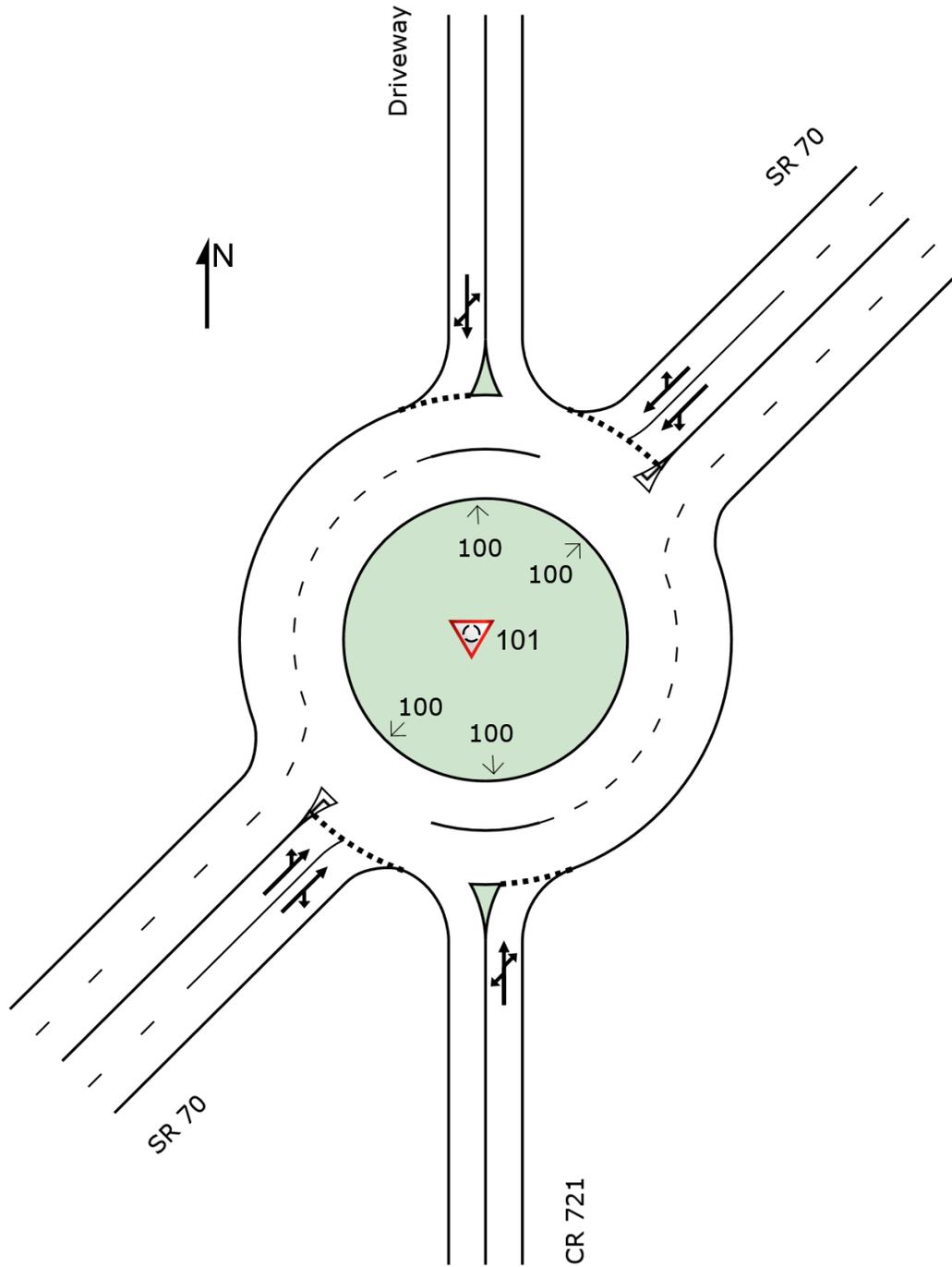
**SIDRA LOS Computer Outputs
Design Year 2052 Volumes - Roundabout Build**

SITE LAYOUT

Site: 101 [2052 AM CR 721 (Site Folder: General)]

New Site
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



MOVEMENT SUMMARY

Site: 101 [2052 AM CR 721 (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.5.224

New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | | |
|------------------------------|------|-----------|--------------|------|---------------|------|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID | Turn | Mov Class | Demand Flows | | Arrival Flows | | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue | | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
| | | | [Total HV] | % | [Total HV] | % | | | | [Veh. veh | Dist] | | | | |
| South: CR 721 | | | | | | | | | | | | | | | |
| 3b | L3 | All MCs | 32 | 7.5 | 32 | 7.5 | 0.226 | 8.2 | LOS A | 0.7 | 19.7 | 0.59 | 0.52 | 0.59 | 31.2 |
| 8 | T1 | All MCs | 1 | 7.5 | 1 | 7.5 | 0.226 | 8.2 | LOS A | 0.7 | 19.7 | 0.59 | 0.52 | 0.59 | 31.8 |
| 18a | R1 | All MCs | 116 | 7.5 | 116 | 7.5 | 0.226 | 8.2 | LOS A | 0.7 | 19.7 | 0.59 | 0.52 | 0.59 | 31.8 |
| Approach | | | 148 | 7.5 | 148 | 7.5 | 0.226 | 8.2 | LOS A | 0.7 | 19.7 | 0.59 | 0.52 | 0.59 | 31.7 |
| NorthEast: SR 70 | | | | | | | | | | | | | | | |
| 1ax | L1 | All MCs | 380 | 12.5 | 380 | 12.5 | 0.354 | 6.1 | LOS A | 1.8 | 50.1 | 0.20 | 0.06 | 0.20 | 30.8 |
| 6x | T1 | All MCs | 471 | 12.5 | 471 | 12.5 | 0.354 | 6.1 | LOS A | 1.8 | 50.1 | 0.20 | 0.06 | 0.20 | 33.0 |
| 16bx | R3 | All MCs | 3 | 12.5 | 3 | 12.5 | 0.354 | 6.1 | LOS A | 1.8 | 50.1 | 0.20 | 0.06 | 0.20 | 32.6 |
| Approach | | | 854 | 12.5 | 854 | 12.5 | 0.354 | 6.1 | LOS A | 1.8 | 50.1 | 0.20 | 0.06 | 0.20 | 32.0 |
| North: Driveway | | | | | | | | | | | | | | | |
| 7b | L3 | All MCs | 1 | 7.5 | 1 | 7.5 | 0.021 | 7.4 | LOS A | 0.1 | 1.5 | 0.58 | 0.52 | 0.58 | 31.7 |
| 4 | T1 | All MCs | 8 | 7.5 | 8 | 7.5 | 0.021 | 7.4 | LOS A | 0.1 | 1.5 | 0.58 | 0.52 | 0.58 | 32.4 |
| 14a | R1 | All MCs | 1 | 7.5 | 1 | 7.5 | 0.021 | 7.4 | LOS A | 0.1 | 1.5 | 0.58 | 0.52 | 0.58 | 32.4 |
| Approach | | | 11 | 7.5 | 11 | 7.5 | 0.021 | 7.4 | LOS A | 0.1 | 1.5 | 0.58 | 0.52 | 0.58 | 32.3 |
| SouthWest: SR 70 | | | | | | | | | | | | | | | |
| 5ax | L1 | All MCs | 11 | 16.0 | 11 | 16.0 | 0.511 | 12.0 | LOS B | 3.2 | 91.2 | 0.66 | 0.62 | 0.95 | 29.8 |
| 2x | T1 | All MCs | 613 | 16.0 | 613 | 16.0 | 0.511 | 12.0 | LOS B | 3.2 | 91.2 | 0.66 | 0.62 | 0.95 | 30.5 |
| 12bx | R3 | All MCs | 155 | 16.0 | 155 | 16.0 | 0.511 | 12.0 | LOS B | 3.2 | 91.2 | 0.66 | 0.62 | 0.95 | 29.9 |
| Approach | | | 778 | 16.0 | 778 | 16.0 | 0.511 | 12.0 | LOS B | 3.2 | 91.2 | 0.66 | 0.62 | 0.95 | 30.4 |
| All Vehicles | | | 1791 | 13.6 | 1791 | 13.6 | 0.511 | 8.8 | LOS A | 3.2 | 91.2 | 0.43 | 0.35 | 0.56 | 31.2 |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglach M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Project: c:\pwworkingdir\kca-pw.bentley.com_kca-pw-01\craig.singer\dms55591\SR70_CR721.sip9

MOVEMENT SUMMARY

Site: 101 [2052 PM CR 721 (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.5.224

New Site
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | | |
|------------------------------|------|-----------|--------------|------|---------------|------|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID | Turn | Mov Class | Demand Flows | | Arrival Flows | | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue | | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
| | | | [Total HV] | % | [Total HV] | % | | | | [Veh. veh | Dist] | | | | |
| South: CR 721 | | | | | | | | | | | | | | | |
| 3b | L3 | All MCs | 65 | 7.5 | 65 | 7.5 | 0.417 | 12.2 | LOS B | 1.8 | 47.8 | 0.68 | 0.71 | 0.93 | 29.4 |
| 8 | T1 | All MCs | 1 | 7.5 | 1 | 7.5 | 0.417 | 12.2 | LOS B | 1.8 | 47.8 | 0.68 | 0.71 | 0.93 | 30.0 |
| 18a | R1 | All MCs | 185 | 7.5 | 185 | 7.5 | 0.417 | 12.2 | LOS B | 1.8 | 47.8 | 0.68 | 0.71 | 0.93 | 30.0 |
| Approach | | | 252 | 7.5 | 252 | 7.5 | 0.417 | 12.2 | LOS B | 1.8 | 47.8 | 0.68 | 0.71 | 0.93 | 29.8 |
| NorthEast: SR 70 | | | | | | | | | | | | | | | |
| 1ax | L1 | All MCs | 148 | 12.5 | 148 | 12.5 | 0.280 | 5.7 | LOS A | 1.3 | 34.7 | 0.27 | 0.12 | 0.27 | 31.7 |
| 6x | T1 | All MCs | 487 | 12.5 | 487 | 12.5 | 0.280 | 5.7 | LOS A | 1.3 | 34.7 | 0.27 | 0.12 | 0.27 | 33.1 |
| 16bx | R3 | All MCs | 2 | 12.5 | 2 | 12.5 | 0.280 | 5.7 | LOS A | 1.3 | 34.7 | 0.27 | 0.12 | 0.27 | 32.8 |
| Approach | | | 638 | 12.5 | 638 | 12.5 | 0.280 | 5.7 | LOS A | 1.3 | 34.7 | 0.27 | 0.12 | 0.27 | 32.7 |
| North: Driveway | | | | | | | | | | | | | | | |
| 7b | L3 | All MCs | 2 | 7.5 | 2 | 7.5 | 0.020 | 6.0 | LOS A | 0.1 | 1.6 | 0.54 | 0.45 | 0.54 | 32.1 |
| 4 | T1 | All MCs | 9 | 7.5 | 9 | 7.5 | 0.020 | 6.0 | LOS A | 0.1 | 1.6 | 0.54 | 0.45 | 0.54 | 32.8 |
| 14a | R1 | All MCs | 1 | 7.5 | 1 | 7.5 | 0.020 | 6.0 | LOS A | 0.1 | 1.6 | 0.54 | 0.45 | 0.54 | 32.8 |
| Approach | | | 13 | 7.5 | 13 | 7.5 | 0.020 | 6.0 | LOS A | 0.1 | 1.6 | 0.54 | 0.45 | 0.54 | 32.7 |
| SouthWest: SR 70 | | | | | | | | | | | | | | | |
| 5ax | L1 | All MCs | 25 | 16.0 | 25 | 16.0 | 0.382 | 7.5 | LOS A | 1.8 | 50.5 | 0.41 | 0.22 | 0.41 | 31.6 |
| 2x | T1 | All MCs | 673 | 16.0 | 673 | 16.0 | 0.382 | 7.5 | LOS A | 1.8 | 50.5 | 0.41 | 0.22 | 0.41 | 32.4 |
| 12bx | R3 | All MCs | 75 | 16.0 | 75 | 16.0 | 0.382 | 7.5 | LOS A | 1.8 | 50.5 | 0.41 | 0.22 | 0.41 | 31.8 |
| Approach | | | 773 | 16.0 | 773 | 16.0 | 0.382 | 7.5 | LOS A | 1.8 | 50.5 | 0.41 | 0.22 | 0.41 | 32.3 |
| All Vehicles | | | 1675 | 13.3 | 1675 | 13.3 | 0.417 | 7.5 | LOS A | 1.8 | 50.5 | 0.40 | 0.26 | 0.43 | 32.1 |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglach M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Project: c:\pwworkingdir\kca-pw.bentley.com_kca-pw-01\craig singer\dms55591\SR70_CR721.sip9

APPENDIX I: Intersection Control Evaluation

PROFESSIONAL ENGINEER CERTIFICATE

I hereby certify that I am a registered professional engineer in the State of Florida practicing with Kisinger Campo & Associates, and that I have supervised the preparation of, and approved the analysis, findings, opinions, conclusions, and technical advice reported in:

REPORT: Intersection Control Evaluation Memorandum
PROJECT: SR 70 from Lonesome Island Road to CR 721
LOCATION: Highlands County
FPID NO.: 449851-1
CLIENT: FDOT District One

The following duly authorized engineering business performed the engineering work represented by this report:

Kisinger Campo & Associates, Corp.
201 N. Franklin St., Suite 400
Tampa, FL 33602
Telephone: (813) 871-5331

I, M. Fathy Abdalla, Florida P.E. Number 63914, have prepared this Intersection Control Evaluation (ICE) Memorandum for SR 70 at CR 721. This ICE memo contains detailed engineering information that fulfills the purpose and need for this project.

I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of transportation engineering as applied through design standards and criteria set forth by the federal, state, and local regulatory agencies as well as professional judgement and experience.

Name: M. Fathy Abdalla, P.E.

Signature: _____
M. Fathy Abdalla 2024.07.03
13:13:24-04'00'

P.E. Number: 63914

Date: _____

This report has been digitally signed and sealed by M. Fathy Abdalla, P.E. on the date indicated here. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

SR 70 ICE Stage 1 Analysis Memorandum

TO: Kyle Purvis, PE; Susan C. Joel, PE, PTOE, RSP1
FROM: M. Fathy Abdalla, Ph.D., PE, PTOE
CC: Jeffery Novotny, PE, AICP, RSP1
DATE: July 2nd, 2024
RE: SR 70 ICE Stage 1 Analysis Memorandum

Introduction

This Intersection Control Evaluation (ICE) Stage 1 Analysis Memorandum – State Road (SR) 70 from Lonesome Island Rd. to County Road (CR) 721 in Highlands County, FL was prepared for Florida Department of Transportation (FDOT) District One by Kisinger Campo and Associates (KCA). The purpose of this Memorandum is to receive concurrence on the Stage 1 ICE analysis for the intersection of SR 70 at CR 721 based on an Opening Year of 2032 and a Design Year of 2052. The FDOT District One is conducting a Project Development and Environment (PD&E) study for proposed improvements to the SR 70 corridor in Highlands County. The intent is to provide additional roadway capacity and enhance safety along the SR 70 corridor, a major east-west roadway spanning the state. The project limits extend approximately 7.6 miles from Lonesome Island Road to the southern leg of CR 721 in Highlands County. The purpose of this project is to address traffic safety conditions on SR 70 from Lonesome Island Road to the southern leg of CR 721 within Highlands County. This project is needed to improve traffic safety conditions, emergency evacuation, and incident response times. Other goals of the project are to maintain important east-west connectivity within the regional transportation network and accommodate freight activity within the area.

SR 70 in this area has a context classification of C2-Rural and an access classification of Access Class 03. The only signalized intersection within the project limits is SR 70 at CR 721 which operates under flashing signal control. Figure 1.1 depicts the intersection of SR 70 and CR 721.

Figure 1 Existing Intersection Conditions



CR 721 at SR 70 is a Two-Way Stop-Controlled (TWSC) intersection consisting of two overhead yellow/red flashing signals along each approach. The existing signals are mast arm-mounted and give priority to the eastbound and westbound approaches. All approaches consist of one shared through left-turn right-turn lane. There are no existing pedestrian signals, crosswalks, curb ramps, or sidewalks along any approaches to the intersection. Along the westbound approach, there exists an unmarked paved shoulder that may serve as a bike lane. Along the eastbound approach, there exists a wide, unmarked paved shoulder that may serve as a right-turn lane. The existing posted speed limit on CR 721 is 45 mph. Additionally, there is a posted speed limit of 60 mph with an advisory speed of 45 mph along SR 70 through the intersection. The proposed recommendations along SR 70 include widening from a two-lane undivided roadway to a four-lane divided roadway with a median.

Based on the SR 70 Design Traffic Technical Memorandum (DTTM), the established truck percentage (T-Factor) along SR 70 and CR 721 is 32.0% and 15.0%, respectively. The design hour truck (DHT) percentage is taken as half of the 24-hour truck percentage, per the 2019 FDOT Project Traffic Forecasting Handbook. DHT percentages of 16% and 7.5% will be used for SR 70 and CR 721, respectively.

The intersection of SR 70 and CR 721 has been the site of 19 reported crashes between 2018 and 2022. Among these crashes, rear-ends were the most frequent, accounting for 21% of the total. Rear end crashes often result from road users operating their vehicles carelessly or negligently. There were two fatal crashes reported in the study period. The first fatal crash was reported in 2018 as a “fell/jumped from motor vehicle” crash on CR 721 near the intersection under daylight and dry conditions, the initial cause was reported as running off roadway. This crash cannot be attributed to the roadway characteristics with the available information. The second fatal crash was reported in 2019 as a head on crash on SR 70 near CR 721 under daylight and dry conditions, the initial cause was reported as improper passing.

Signal Warrant Analysis

A Traffic Signal Warrant Analysis was prepared for the intersection of SR 70 at CR 721 to determine if a signal is warranted based on Opening Year 2032 conditions. None of the nine signal warrants were satisfied. As a result, this Intersection Control Evaluation will not consider signalized alternatives.

Traffic Forecast and Analysis

Forecasted AADTs were developed for the Design Year 2052 for the No-Build and Build scenarios and can be found attached. Future AADTs were developed using growth rates for the project area provided by the attached SR 70 Design Traffic Technical Memorandum (DTTM). This information was used to develop an annual growth rate that was used to calculate future AADTs. Design Year 2052 and Opening Year 2032 traffic volumes have been established at the intersection and used in the analysis of the intersection.

Alternative Analysis

Two alternatives provided an adequate Volume-to-Capacity (V/C) Ratio in the CAP-X analysis, the alternatives can be found in Table 1. The top SPICE outputs for the Crash Prediction Rank are the 1NS X 2EW Roundabout and the Unsignalized Restricted Crossing U-Turn (RCUT) E-W. The top SPICE outputs for the Safe System Intersection (SSI) are the 1NS X 2EW Roundabout and the Unsignalized Restricted Crossing U-Turn (RCUT) E-W. The 1NS X 2EW Roundabout, the Unsignalized Restricted Crossing U-Turn (RCUT) E-W, and the Minor Road Stop alternatives are recommended to be advanced to Stage 2 of the ICE. Stage 2 will occur during the design phase which is tentatively scheduled for after 2027.

Table 1 ICE Summary

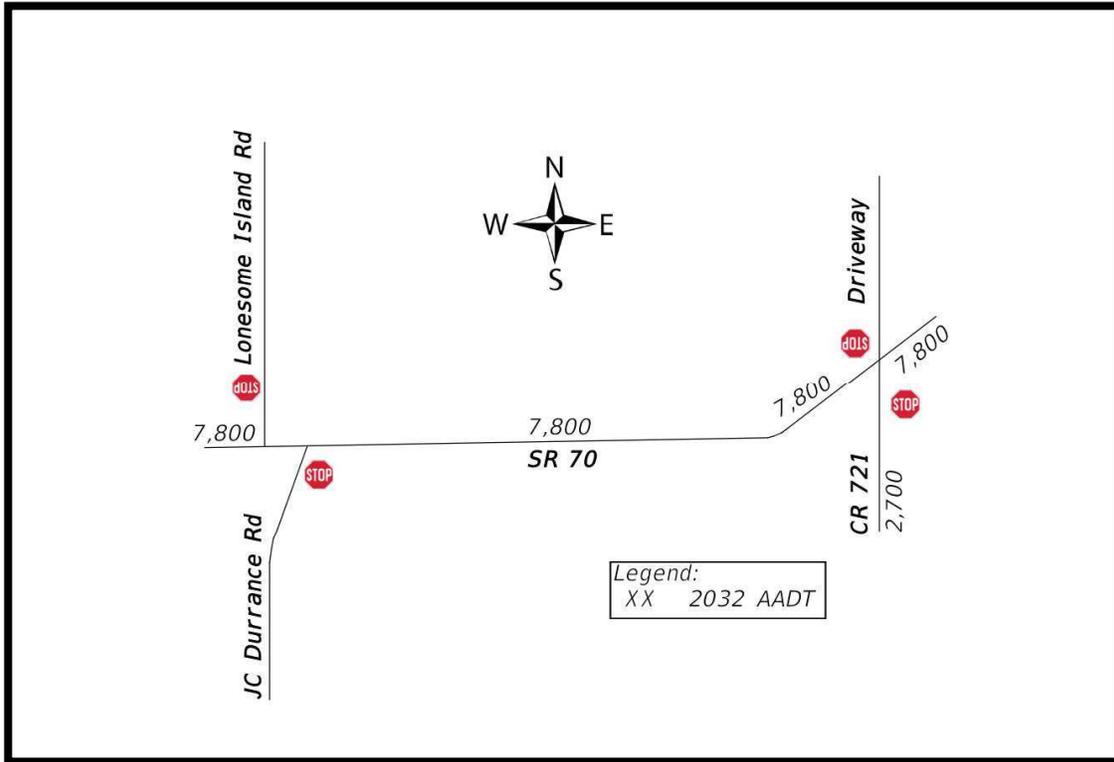
| Type of Intersection | V/C Ratio | | Crash Prediction Rank | SSI Rank |
|---|-----------|------|-----------------------|----------|
| | AM | PM | | |
| 1NS X 2EW Roundabout | 0.46 | 0.37 | 1 | 1 |
| Unsignalized Restricted Crossing U-Turn E-W | 0.60 | 0.74 | 2 | 2 |
| Unsignalized Thru-Cut E-W | 3.40 | 1.66 | - | 3 |
| Minor Road Stop | 7.44 | 3.78 | 3 | 4 |

Attachments

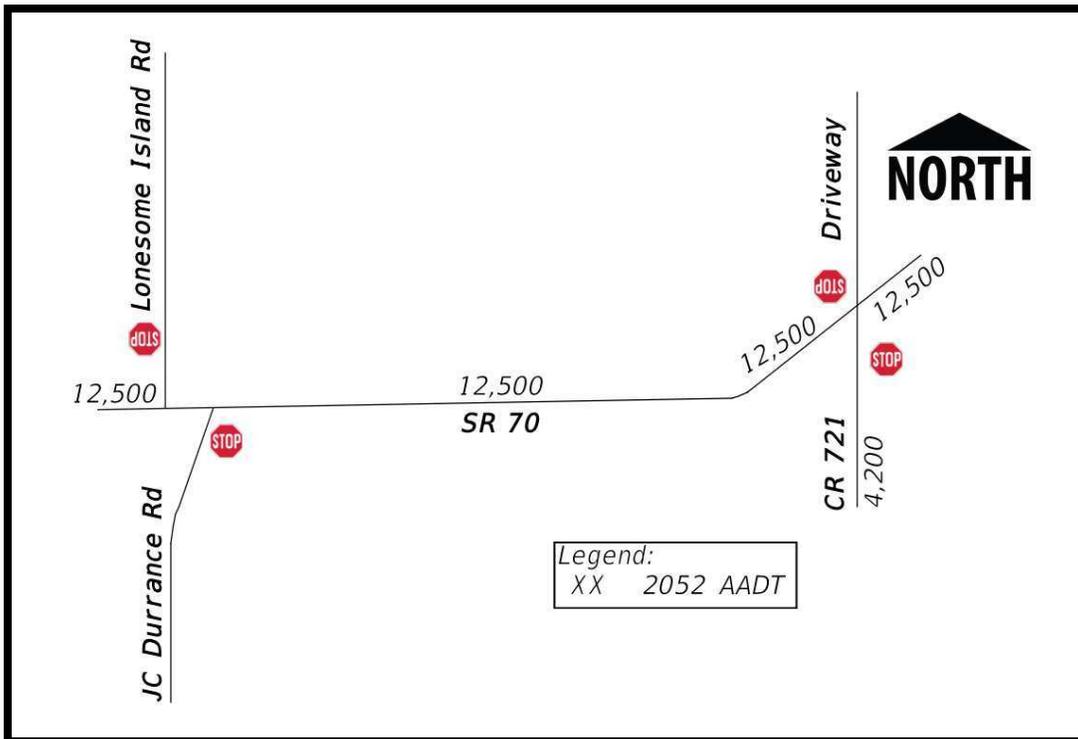
Attachments included in this submittal are the Traffic Signal Warrant Analysis report, the SR 70 Design Traffic Technical Memorandum, Future Traffic Volumes, 2045 AM and PM CAP-X worksheets, SPICE worksheets, and the FDOT ICE Stage 1 Form.

APPENDIX C - Future Traffic Volumes

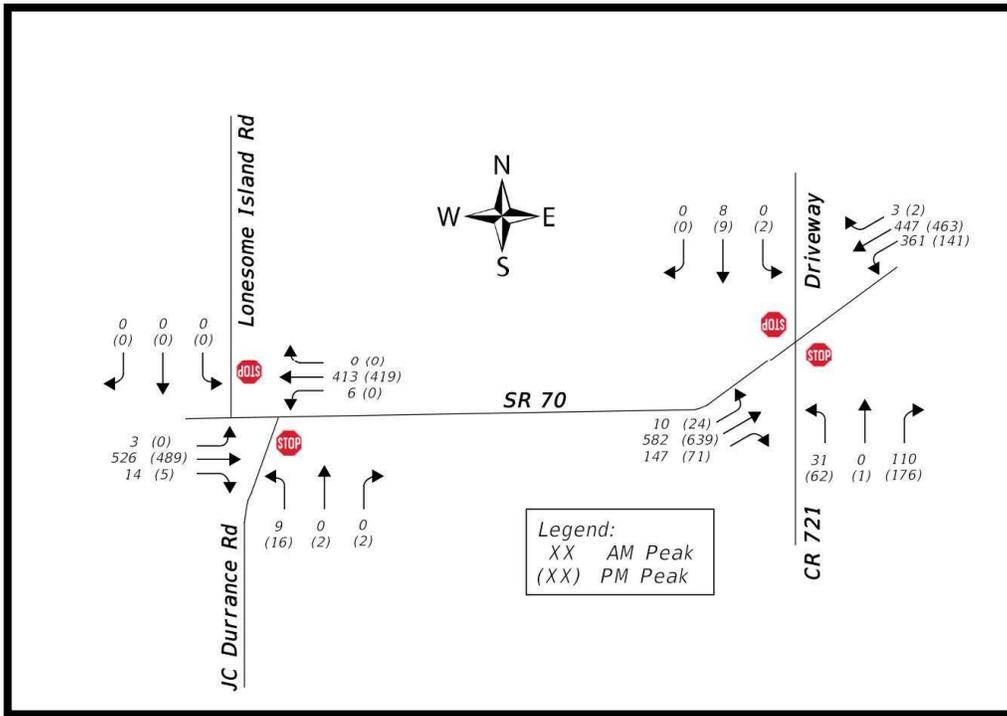
SR 70 Opening Year 2032 Build AADT



SR 70 Design Year 2052 Build AADT



SR 70 Design Year 2052 Turning Movement Volumes



APPENDIX D - CAP-X Analysis

Capacity Analysis for Planning of Junctions

Summary Report - Page 1 of 2

| | |
|------------------------------|---|
| Project Name: | SR-70 PD&E |
| Project Number: | 449851-1 |
| Location: | SR 70 at CR 721 Highlands County, Florida |
| Date: | 2052 AM |
| Number of Intersection Legs: | 4 |
| Major Street Direction: | East-West |

| Traffic Volume Demand | | | | | | |
|---------------------------------|---|---|---|---|----------------|---------------|
| | Volume (Veh/hr) | | | | Percent (%) | |
| | U-Turn  | Left  | Thru  | Right  | Heavy Vehicles | Volume Growth |
| Eastbound | 0 | 10 | 582 | 147 | 16.00% | 0.00% |
| Westbound | 0 | 361 | 447 | 3 | 16.00% | 0.00% |
| Southbound | 0 | 0 | 8 | 0 | 7.50% | 0.00% |
| Northbound | 0 | 31 | 0 | 110 | 7.50% | 0.00% |
| Adjustment Factor | 0.80 | 0.95 | | 0.85 | | |
| Suggested | 0.80 | 0.95 | | 0.85 | | |
| Truck to PCE Factor | | | | Suggested = 2.00 | 2.00 | |
| FDOT Context Zone | | C2-Rural | | | | |
| E-W / Crossing East-West Legs | | Low | Low | Low | | |
| N-S / Crossing North-South Legs | | Low | Low | Low | | |
| Critical Lane Volume Threshold | | 2-phase signal | | Suggested = 1800 | 1800 | |
| | | 3-phase signal | | Suggested = 1750 | 1750 | |
| | | 4-phase signal | | Suggested = 1700 | 1700 | |

Capacity Analysis for Planning of Junctions

Summary Report - Page 2 of 2

| TYPE OF INTERSECTION | Overall v/c Ratio | V/C Ranking | Pedestrian Accommodations | Bicycle Accommodations |
|---|-------------------|-------------|---------------------------|------------------------|
| 1NS X 2EW | 0.46 | 1 | 5.00 | 4.37 |
| Unsignalized Restricted Crossing U-Turn E-W | 0.60 | 2 | 2.47 | 3.23 |
| Unsignalized ThruCut E-W | 3.40 | 3 | 3.17 | 3.96 |
| Two-Way Stop Control E-W | 7.44 | 4 | 2.26 | 3.54 |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |

Capacity Analysis for Planning of Junctions

Summary Report - Page 1 of 2

| | |
|------------------------------|---|
| Project Name: | SR-70 PD&E |
| Project Number: | 449851-1 |
| Location: | SR 70 at CR 721 Highlands County, Florida |
| Date: | 2052 PM |
| Number of Intersection Legs: | 4 |
| Major Street Direction: | East-West |

| Traffic Volume Demand | | | | | | |
|---------------------------------|---|---|---|---|----------------|---------------|
| | Volume (Veh/hr) | | | | Percent (%) | |
| | U-Turn  | Left  | Thru  | Right  | Heavy Vehicles | Volume Growth |
| Eastbound | 0 | 24 | 639 | 71 | 16.00% | 0.00% |
| Westbound | 0 | 141 | 463 | 2 | 16.00% | 0.00% |
| Southbound | 0 | 2 | 9 | 0 | 7.50% | 0.00% |
| Northbound | 0 | 62 | 1 | 176 | 7.50% | 0.00% |
| Adjustment Factor | 0.80 | 0.95 | | 0.85 | | |
| Suggested | 0.80 | 0.95 | | 0.85 | | |
| Truck to PCE Factor | | | | Suggested = 2.00 | 2.00 | |
| FDOT Context Zone | | C2-Rural | | | | |
| E-W / Crossing East-West Legs | | Low | Low | Low | | |
| N-S / Crossing North-South Legs | | Low | Low | Low | | |
| Critical Lane Volume Threshold | | 2-phase signal | | Suggested = 1800 | 1800 | |
| | | 3-phase signal | | Suggested = 1750 | 1750 | |
| | | 4-phase signal | | Suggested = 1700 | 1700 | |

Capacity Analysis for Planning of Junctions

Summary Report - Page 2 of 2

| TYPE OF INTERSECTION | Overall v/c Ratio | V/C Ranking | Pedestrian Accommodations | Bicycle Accommodations |
|---|-------------------|-------------|---------------------------|------------------------|
| 1NS X 2EW | 0.37 | 1 | 5.01 | 4.41 |
| Unsignalized Restricted Crossing U-Turn E-W | 0.74 | 2 | 2.47 | 3.23 |
| Unsignalized ThruCut E-W | 1.66 | 3 | 3.19 | 3.96 |
| Two-Way Stop Control E-W | 3.78 | 4 | 2.26 | 3.54 |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- |

APPENDIX E - SPICE Analysis

Control Strategy Selection and Inputs

Specify the Facility Level Inputs and the Control Strategies to be Included in the SPICE Analysis.

| Intersection Type | At-Grade Intersection |
|---|----------------------------|
| Analysis Year | Opening and Design Year |
| Opening Year | 2032 |
| Design Year | 2052 |
| Facility Type | On Rural Multilane Highway |
| Number of Legs | 4-leg |
| 1-Way/2-Way | |
| # of Major Street Lanes (both directions) | |
| Major Street Approach Speed | |
| Opening Year - Major Road AADT | 7,800 |
| Opening Year - Minor Road AADT | 2,700 |
| Design Year - Major Road AADT | 12,500 |
| Design Year - Minor Road AADT | 4,200 |

For more information on how to determine these values, see the "Definitions" worksheet

| Control Strategy | Include | Base Intersection |
|--|---------|-------------------|
| Traffic Signal | No | -- |
| Traffic Signal (Alternative Configuration) | No | -- |
| Minor Road Stop Control | Yes | -- |
| All Way Stop Control | No | -- |
| 1-Lane Roundabout | No | -- |
| 2-Lane Roundabout | Yes | -- |
| Displaced Left Turn (DLT) | No | Traffic Signal |
| Median U-Turn (MUT) | No | Traffic Signal |
| Signalized Restricted Crossing U-Turn (RCUT) | No | -- |
| Unsignalized Restricted Crossing U-Turn (RCUT) | Yes | -- |
| Signalized Thru-Cut* | No | -- |
| Unsignalized Thru-Cut* | Yes | -- |
| Bowtie* | No | -- |
| Continuous Green-T Intersection | No | Traffic Signal |
| Jughandle | No | Traffic Signal |
| Other 1* | No | Traffic Signal |
| Other 2* | No | Minor Road Stop |

No SPF Available

No SPF Available

Opening Year AADT Outside of SPF Development Range

*SSI Only, No Crash Prediction Available
 *SSI Only, No Crash Prediction Available
 *SSI Only, No Crash Prediction Available

*Please Select
 *Please Select

| Florida Department of Transportation Safety Performance for Intersection Control Evaluation Tool Results Summary of crash prediction results for each alternative | | | | | | | | | | | |
|--|---|---|----------------------------|--------------------------|-----------------------|-----------------------------------|---------------|----------------------|--------------|-------------|------|
| Project Information | | | | | | | | | | | |
| Project Name: | SR-70 PD&E | Intersection Type | At-Grade Intersection | | | | | | | | |
| Agency: | SR 70 at CR 721 Highlands County, Florida | Opening Year | 2032 | | | | | | | | |
| Project Reference: | Kisinger Campo & Associates Inc. | Design Year | 2052 | | | | | | | | |
| City: | Highlands County | Facility Type | On Rural Multilane Highway | | | | | | | | |
| State: | Florida | Number of Legs | 4-leg | | | | | | | | |
| Date: | 7/2/2024 | 1.5Way/2-Way | | | | | | | | | |
| Analyst: | IR | # of Major Street Lanes (both directions) | | | | | | | | | |
| | | Major Street Approach Speed | | | | | | | | | |
| Crash Prediction Summary | | | | | | | | | | | |
| Control Strategy | Crash Type | Opening Year | Design Year | Total Project Life Cycle | Crash Prediction Rank | AADT Within SPF Prediction Range? | | Source of Prediction | Opening Year | Design Year | Rank |
| | | | | | | (Open Year) | (Design Year) | | | | |
| Minor Road Stop | Total | 1.96 | 3.56 | 57.53 | 3 | Yes | Yes | Calibrated SPF | 90 | 76 | 4 |
| | Fatal & Injury | 0.71 | 1.35 | 21.42 | | | | | | | |
| 2-lane Roundabout | Total | 1.52 | 2.60 | 43.09 | 1 | Yes | Yes | Uncalibrated SPF | 100 | 99 | 1 |
| | Fatal & Injury | 0.31 | 0.56 | 9.04 | | | | | | | |
| Unsignalized RCUT | Total | 2.49 | 3.21 | 59.84 | 2 | Yes | Yes | Uncalibrated SPF | 92 | 82 | 2 |
| | Fatal & Injury | 0.48 | 0.68 | 12.27 | | | | | | | |
| Unsignalized Thru-Cut | Total | No SPF | No SPF | No SPF | -- | N/A | N/A | N/A | 91 | 79 | 3 |
| | Fatal & Injury | No SPF | No SPF | No SPF | | | | | | | |

APPENDIX F - ICE Forms

Florida Department of Transportation
Intersection Control Evaluation (ICE) Form
Stage 1: Screening

To fulfill the requirements of Stage 1 (Screening) of FDOT's ICE procedures, complete the following form and append all supporting documentation. Completed forms are to be submitted to the District Traffic Operations Engineer (DTOE) and District Design Engineer (DDE) for the project's approval.

| | | | | | |
|---|--|-----------------------------|------------------------------------|----------|-----------|
| Project Name | SR-70 PD&E | | FDOT Project # | 449851-1 | |
| Submitted By | Fathy Abdalla Ph.D., PE, PTOE | Agency/Company | Kisinger Campo and Associates Inc. | Date | 6/3/2024 |
| Email | FAbdalla@kcaeng.com | FDOT District | District 1 | County | Highlands |
| Project Locality (City/Town/Village) | Brighton | | | | |
| Intersection Type | At-Grade Intersection | FDOT Context Classification | C2 - Rural | | |
| Project Funding Source | Federal | Project Type | Corridor Improvement Project | | |
| Project Purpose (What is the catalyst for this project and why is it being undertaken?) | Proposed widening of a two-lane facility to a four-lane, divided facility and/or the inclusion of operational improvements along 7.6 miles of SR 70 from Lonesome Island Road to the southern leg of CR 721 in Highlands County. The purpose is to address traffic safety conditions on SR 70 from Lonesome Island Road to the southern leg of CR 721 within Highlands County. The project seeks to maintain important east-west connectivity within the regional transportation network and accommodate freight activity within the area. | | | | |
| Project Setting Description (Describe the area surrounding the intersection) | Within the project limits SR 70 has a context classification of C2-Rural and an access classification of Access Class 03. The only signalized intersection within the project limits is SR 70 at CR 721 which operates under flashing signal control. There is farmland in all four quadrants of the intersection. | | | | |
| Multimodal Context (Describe the pedestrian, bicycle, and transit activity in the area and the potential for activity based on surrounding land uses and development patterns) | In the project area, there are currently no pedestrian signals, crosswalks, bike lanes, curb ramps, or sidewalks. However, the unmarked shoulder could potentially function as a bike lane. A 12-ft shared use path is proposed along the south side of SR 70. Additionally, heavy vehicle traffic within the project limits exceeds the statewide average. | | | | |

| Major Street Information | | | | | | | | | | |
|---|--|------------------------------|----------------------------------|--|---|---------------------------------|----------|---------------------------------|-----|--|
| Route #: | SR 70 | Route Name(s) | SR 70 | | | | Milepost | 29.216 | | |
| Existing Control Type | Two-way Stop-Control | | Existing AADT | 7,800 | | Design Year AADT | 12,500 | | | |
| Design Vehicle | Florida Interstate Semitrailer (WB-62FL) | | Control Vehicle | Florida Interstate Semitrailer (WB-62FL) | | | | | | |
| Primary Functional Classification | | | Rural Principal Arterial - Other | | | Design Speed (mph) | 60 | | | |
| Secondary Functional Classification (if app.) | | | | | | Target Speed (mph) [if app.] | | | | |
| Approach #1 | Direction | Eastbound | | Number of Lanes | | Study Period #1 Traffic Volumes | | Study Period #2 Traffic Volumes | | |
| | Sidewalks along: | Neither side of the approach | | Left-Turn | 1 | | | | | |
| | Crosswalk on Approach? | No | | Left-Through | 0 | Weekday AM Peak | | Weekday PM Peak | | |
| | On-Street Bike Facilities? | No | | Through | 2 | Left | 10 | Left | 24 | |
| | Multi-Use Path? | Yes | | Left-Through-Right | 0 | Through | 582 | Through | 639 | |
| | Scheduled Bus Service? | No | | Through-Right | 0 | Right | 147 | Right | 71 | |
| | Bus Stop on Approach? | No | | Right-Turn | 1 | Daily Truck % | | 16.0% | | |
| Approach #2 | Direction | Westbound | | Number of Lanes | | Study Period #1 Traffic Volumes | | Study Period #2 Traffic Volumes | | |
| | Sidewalks along: | Neither side of the approach | | Left-Turn | 1 | | | | | |
| | Crosswalk on Approach? | No | | Left-Through | 0 | Weekday AM Peak | | Weekday PM Peak | | |
| | On-Street Bike Facilities? | No | | Through | 2 | Left | 361 | Left | 141 | |
| | Multi-Use Path? | No | | Left-Through-Right | 0 | Through | 447 | Through | 463 | |
| | Scheduled Bus Service? | No | | Through-Right | 0 | Right | 3 | Right | 2 | |
| | Bus Stop on Approach? | No | | Right-Turn | 1 | Daily Truck % | | 16.0% | | |

| Minor Street Information | | | | | | | | | | |
|---|--|------------------------------|-----------------------|--|---|---------------------------------|--------------------|---------------------------------|-----|--|
| Route #: | CR 721 | Route Name(s) | CR 721 | | | | Milepost (if app.) | N/A | | |
| Existing Control Type | Two-way Stop-Control | | Existing AADT | 2,700 | | Design Year AADT | 4,200 | | | |
| Design Vehicle | Florida Interstate Semitrailer (WB-62FL) | | Control Vehicle | Florida Interstate Semitrailer (WB-62FL) | | | | | | |
| Primary Functional Classification | | | Rural Major Collector | | | Design Speed (mph) | 45 | | | |
| Secondary Functional Classification (if app.) | | | | | | Target Speed (mph) [if app.] | | | | |
| Approach #1 | Direction | Northbound | | Number of Lanes | | Study Period #1 Traffic Volumes | | Study Period #2 Traffic Volumes | | |
| | Sidewalks along: | Neither side of the approach | | Left-Turn | 0 | Weekday AM Peak | | Weekday PM Peak | | |
| | Crosswalk on Approach? | No | | Left-Through | 0 | Left | 31 | Left | 62 | |
| | On-Street Bike Facilities? | No | | Through | 0 | Through | 0 | Through | 1 | |
| | Multi-Use Path? | No | | Left-Through-Right | 1 | Right | 110 | Right | 176 | |
| | Scheduled Bus Service? | No | | Through-Right | 0 | Daily Truck % | | 7.5% | | |
| | Bus Stop on Approach? | No | | Right-Turn | 0 | | | | | |
| Approach #2 | Direction | Southbound | | Number of Lanes | | Study Period #1 Traffic Volumes | | Study Period #2 Traffic Volumes | | |
| | Sidewalks along: | Neither side of the approach | | Left-Turn | 0 | Weekday AM Peak | | Weekday PM Peak | | |
| | Crosswalk on Approach? | No | | Left-Through | 0 | Left | 0 | Left | 2 | |
| | On-Street Bike Facilities? | No | | Through | 0 | Through | 8 | Through | 9 | |
| | Multi-Use Path? | No | | Left-Through-Right | 1 | Right | 0 | Right | 0 | |
| | Scheduled Bus Service? | No | | Through-Right | 0 | Daily Truck % | | 7.5% | | |
| | Bus Stop on Approach? | No | | Right-Turn | 0 | | | | | |
| Approach #3 | Direction | | | Number of Lanes | | Study Period #1 Traffic Volumes | | Study Period #2 Traffic Volumes | | |
| | Sidewalks along: | | | Left-Turn | | Weekday AM Peak | | Weekday PM Peak | | |
| | Crosswalk on Approach? | | | Left-Through | | Left | | Left | | |
| | On-Street Bike Facilities? | | | Through | | Through | | Through | | |
| | Multi-Use Path? | | | Left-Through-Right | | Right | | Right | | |
| | Scheduled Bus Service? | | | Through-Right | | Daily Truck % | | | | |
| | Bus Stop on Approach? | | | Right-Turn | | | | | | |

| Crash History (Existing Intersections Only) |
|--|
| Append the most recent five-years of crash data for the intersection from the CAR System. If the crash data evidences any issues relating to safety performance, discuss briefly here: |
| The study area's highest-ranking crash types include opposing sideswipe and guardrail face crashes (both 15%), animal and rear-end crashes (both 13%). There were two fatal crashes reported in the study period. The first fatal crash was reported in 2018 as a "fell/jumped from motor vehicle" crash on CR 721 near the intersection under daylight and dry conditions, the initial cause was reported as running off roadway. This crash cannot be attributed to the roadway characteristics with the available information. The second fatal crash was reported in 2019 as a head on crash on SR 70 near CR 721 under daylight and dry conditions, the initial cause was reported as improper passing. |

| Control Strategy Evaluation | | | | | | | | |
|--|-----------------|-----------------|------------------|-------------------|-----------------------|----------|--------------------------|---|
| Provide a brief justification as to why each of the following control strategies should be advanced or not. Justification should consider potential environmental impacts. | | | | | | | | |
| Control Strategy | CAP-X Outputs | | | | SPICE Outputs | | Strategy to be Advanced? | Justification |
| | V/C Ratio | | Ped Accom. Score | Bike Accom. Score | Crash Prediction Rank | SSI Rank | | |
| | Weekday AM Peak | Weekday PM Peak | | | | | | |
| Two-Way Stop-Control | 7.44 | 3.78 | 2.26 | 3.54 | 3 | 4 | Yes | Base Alternative. |
| All-Way Stop-Control | | | | | | | No | Does not provide adequate capacity. |
| Signalized Control | | | | | | | No | Signal is not warranted. |
| Roundabout (1-lane) | | | | | | | No | SR 70 widening can not be accomodated by a 1-lane roundabout. |
| Roundabout (2-lane) | 0.46 | 0.37 | 5.00 | 4.37 | 1 | 1 | Yes | Provides adequate capacity. |
| Median U-Turn | | | | | | | No | Signal is not warranted. |
| Median U-Turn (Partial) | | | | | | | No | Signal is not warranted. |
| Restricted Crossing U-turn (Signalized) | | | | | | | No | Signal is not warranted. |
| Restricted Crossing U-turn (Unsignalized) | 0.60 | 0.74 | 2.47 | 3.23 | 2 | 2 | Yes | Provides adequate capacity. |
| Jughandle (Forward Ramps) | | | | | | | No | Not feasible due to lack of right-of -way |
| Jughandle (Reverse Ramps) | | | | | | | No | Not feasible due to lack of right-of -way |
| Thru-Cut (Signalized) | | | | | | | No | Signal is not warranted. |

| | | | | | | | | |
|----------------------------|------|------|------|------|-----|---|----|------------------------------------|
| Thru-Cut (Unsignalized) | 3.40 | 1.66 | 3.17 | 3.96 | N/A | 3 | No | Does not provide adequate capacity |
|----------------------------|------|------|------|------|-----|---|----|------------------------------------|

| | | | | |
|---|--|-----------|--|------|
| Resolution | | | | |
| <i>To be filled out by FDOT District Traffic Operations Engineer and District Design Engineer</i> | | | | |
| Project Determination | Multiple Viable Alternatives Identified: Continue to Stage 2 | | | |
| Comments | | | | |
| DTE Name | | Signature | | Date |
| DDE Name | | Signature | | Date |

APPENDIX J: HSM Spreadsheets and Costs

The **HSM** includes Safety Performance Functions (SPFs) for many roadway segment and intersection applications. SPFs are equations used to estimate or predict the expected average crash frequency per year at a location as a function of traffic volume and roadway characteristics. Adjust SPFs to local conditions by applying calibration factors shown in **Table 122.6.3**. The use of HSMSPF and Crash Modification Factors (CMF), with an Empirical Bayes (EB) adjustment, provides research-based solutions for use in Benefit/Cost comparisons. Crash distributions presented in **Table 122.6.4** and KABCO costs as specified in **Table 122.6.2** should be used in determining benefits from an **HSM** analysis.

Table 122.6.3 HSM Calibration Factors for Florida

| Type Facility | | Abbreviation | Calibration Factor (Cx) | |
|--|---|-----------------|-------------------------|--|
| FDOT Roadway Calibration Factors | | | | |
| Rural | 2-lane Undivided | R2U | 1.00 | Existing & No-build Build |
| | 4-lane Divided | R4D | 0.68 | |
| Urban | 2-lane Undivided | U2U | 1.02 | Existing & No-build Existing & No-build Build Build |
| | 3-lane with a Center Two-Way Left Turn Lane | U32LT | 1.04 | |
| | 4-lane Undivided | U4U | 0.73 | |
| | 4-lane Divided | U4D | 1.63 | |
| | 5-lane with a Center Two-Way Left Turn Lane | U52LT | 0.70 | |
| FDOT Intersection Calibration Factors | | | | |
| Rural | 2-lane 3-Leg Stop-Controlled | RTL3ST | 1.27 | Existing & No-build Existing & No-build |
| | 2-lane 4-Leg Stop-Controlled | RTL4ST | 0.74 | |
| | 2-lane 4-Leg Signalized | RTL4SG | 0.92 | Build Build |
| | Multilane 3-Leg Stop-Controlled | RML3ST | 2.20 | |
| | Multilane 4-Leg Stop-Controlled | RML4ST | 1.64 | |
| | Multilane 4-Leg Signalized | RML4SG | 0.45 | |
| Urban | 3-Leg Stop-Controlled Intersection | USA3ST | 1.14 | Build Build |
| | 4-Leg Stop-Controlled Intersection | USA4ST | 1.87 | |
| | 3-Leg Signalized w/o Ped. CMFs | USA3SG w/o Ped. | 2.58 | |
| | 3-Leg Signalized w/ Ped. CMFs | USA3SG w/ Ped. | 2.50 | |
| | 4-Leg Signalized | USA4SG | 2.27 | |

No-Build 2032

| Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments | | | | | |
|--|--|--|----------------------|--------------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | Lonesome Island Rd to Jc Durrance Rd | |
| Date Performed | 08/11/23 | | Jurisdiction | FDOT District One | |
| Input Data | | | Analysis Year | 2032 | |
| Base Conditions | | | Site Conditions | | |
| Length of segment, L (mi) | -- | | 0.085227273 | | |
| AADT (veh/day) | AADT _{MAX} = 17,800 (veh/day) | | 7,800 | | |
| Lane width (ft.) | 12 | | 10 | | |
| Shoulder width (ft.) | 6 | | Right Shld: 4 | Left Shld: 4 | |
| Shoulder type | Paved | | Right Shld: Paved | Left Shld: Paved | |
| Length of horizontal curve (mi) | 0 | | 0.0 | | |
| Radius of curvature (ft.) | 0 | | 0 | | |
| Spiral transition curve (present/not present) | Not Present | | Not Present | | |
| Superelevation variance (ft./ft.) | < 0.01 | | | | |
| Grade (%) | 0 | | 0 | | |
| Driveway density (driveways/mile) | 5 | | 0 | | |
| Centerline rumble strips (present/not present) | Not Present | | Not Present | | |
| Passing lanes [present (1 lane) / present (2 lane) / not present] | Not Present | | Not Present | | |
| Two-way left-turn lane (present/not present) | Not Present | | Not Present | | |
| Roadside hazard rating (1-7 scale) | 3 | | 4 | | |
| Segment lighting (present/not present) | Not Present | | Not Present | | |
| Auto speed enforcement (present/not present) | Not Present | | Not Present | | |
| Calibration Factor, Cr | 1 | | 1.00 | | |

| Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments | | | | | | | | | | | | |
|--|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|-----------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combine d CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | (1)x(2)x...x(11)x(12) |
| 1.17 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.361 |

| Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments | | | | | | | |
|---|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 0.178 | 2.77 | 1.000 | 0.178 | 1.36 | 1.00 | 0.242 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 0.057 | 1.36 | 1.00 | 0.078 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 0.121 | 1.36 | 1.00 | 0.164 |

| Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments | | | | | | |
|--|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 0.242 | 1.000 | 0.078 | 1.000 | 0.164 |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 0.029 | 0.038 | 0.003 | 0.184 | 0.030 |
| Collision with bicycle | 0.002 | 0.000 | 0.004 | 0.000 | 0.001 | 0.000 |
| Collision with pedestrian | 0.003 | 0.001 | 0.007 | 0.001 | 0.001 | 0.000 |
| Overtuned | 0.025 | 0.006 | 0.037 | 0.003 | 0.015 | 0.002 |
| Ran off road | 0.521 | 0.126 | 0.545 | 0.042 | 0.505 | 0.083 |
| Other single-vehicle collision | 0.021 | 0.005 | 0.007 | 0.001 | 0.029 | 0.005 |
| Total single-vehicle crashes | 0.693 | 0.168 | 0.638 | 0.050 | 0.735 | 0.121 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.021 | 0.100 | 0.008 | 0.072 | 0.012 |
| Head-on collision | 0.016 | 0.004 | 0.034 | 0.003 | 0.003 | 0.000 |
| Rear-end collision | 0.142 | 0.034 | 0.164 | 0.013 | 0.122 | 0.020 |
| Sideswipe collision | 0.037 | 0.009 | 0.038 | 0.003 | 0.038 | 0.006 |
| Other multiple-vehicle collision | 0.027 | 0.007 | 0.026 | 0.002 | 0.030 | 0.005 |
| Total multiple-vehicle crashes | 0.307 | 0.074 | 0.362 | 0.028 | 0.265 | 0.043 |

| Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments | | | | |
|---|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) | (5) |
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 0.2 | 0.085227273 | 2.8 |
| Fatal and Injury (FI) | 0.321 | 0.1 | 0.085227273 | 0.9 |
| Property Damage Only (PDO) | 0.679 | 0.2 | 0.085227273 | 1.9 |

No-Build 2032

Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments

| General Information | | Location Information | |
|---|-----------------------------------|----------------------|---------------------------------------|
| Analyst | Darlene Lam | Roadway | SR 70 |
| Agency or Company | American Consulting Professionals | Roadway Section | Jc Durrance Rd to Greenbrier Ln |
| Date Performed | 08/11/23 | Jurisdiction | FDOT District One |
| | | Analysis Year | 2032 |
| Input Data | | Base Conditions | Site Conditions |
| Length of segment, L (mi) | | -- | 1.637121212 |
| AADT (veh/day) | $AADT_{MAX} = 17,800$ (veh/day) | -- | 7,800 |
| Lane width (ft.) | | 12 | 10 |
| Shoulder width (ft.) | | 6 | Right Shld: 4 Left Shld: 4 |
| Shoulder type | | Paved | Right Shld: Paved Left Shld: Paved |
| Length of horizontal curve (mi) | | 0 | 0.0 |
| Radius of curvature (ft.) | | 0 | 0 |
| Spiral transition curve (present/not present) | | Not Present | Not Present |
| Superelevation variance (ft./ft.) | | < 0.01 | 0 |
| Grade (%) | | 0 | 0 |
| Driveway density (driveways/mile) | | 5 | 1.2 |
| Centerline rumble strips (present/not present) | | Not Present | Not Present |
| Passing lanes [present (1 lane) / present (2 lane) / not present] | | Not Present | Not Present |
| Two-way left-turn lane (present/not present) | | Not Present | Not Present |
| Roadside hazard rating (1-7 scale) | | 3 | 4 |
| Segment lighting (present/not present) | | Not Present | Not Present |
| Auto speed enforcement (present/not present) | | Not Present | Not Present |
| Calibration Factor, Cr | | 1 | 1.00 |

Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|---------------------|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|---|
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | $(1) \times (2) \times \dots \times (11) \times (12)$ |
| 1.17 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.361 |

Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|----------------------------|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 3,412 | 0.14 | 1,000 | 3,412 | 1.36 | 1.00 | 4,644 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 1,095 | 1.36 | 1.00 | 1,491 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 2,317 | 1.36 | 1.00 | 3,153 |

Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|----------------------------------|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 4,644 | 1.000 | 1,491 | 1.000 | 3,153 |
| | | (2)x(3)TOTAL | | (4)x(5)FI | | (6)x(7)PDO |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 0.562 | 0.038 | 0.057 | 0.184 | 0.580 |
| Collision with bicycle | 0.002 | 0.009 | 0.004 | 0.006 | 0.001 | 0.003 |
| Collision with pedestrian | 0.003 | 0.014 | 0.007 | 0.010 | 0.001 | 0.003 |
| Overtuned | 0.025 | 0.116 | 0.037 | 0.055 | 0.015 | 0.047 |
| Ran off road | 0.521 | 2.419 | 0.545 | 0.812 | 0.505 | 1.592 |
| Other single-vehicle collision | 0.021 | 0.098 | 0.007 | 0.010 | 0.029 | 0.091 |
| Total single-vehicle crashes | 0.693 | 3.218 | 0.638 | 0.951 | 0.735 | 2.317 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.395 | 0.100 | 0.149 | 0.072 | 0.227 |
| Head-on collision | 0.016 | 0.074 | 0.034 | 0.051 | 0.003 | 0.009 |
| Rear-end collision | 0.142 | 0.659 | 0.164 | 0.244 | 0.122 | 0.385 |
| Sideswipe collision | 0.037 | 0.172 | 0.038 | 0.057 | 0.038 | 0.120 |
| Other multiple-vehicle collision | 0.027 | 0.125 | 0.026 | 0.039 | 0.030 | 0.095 |
| Total multiple-vehicle crashes | 0.307 | 1.426 | 0.362 | 0.540 | 0.265 | 0.836 |

Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) |
|----------------------------|--|--|-----------------------------|------------------------------|
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 4.6 | 1.637121212 | 2.8 |
| Fatal and Injury (FI) | 0.321 | 1.5 | 1.637121212 | 0.9 |
| Property Damage Only (PDO) | 0.679 | 3.2 | 1.637121212 | 1.9 |

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| Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments | | | | | |
|--|--|--|----------------------|----------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | Greenbrier Ln to DC Bar Ranch Rd | |
| Date Performed | 08/11/23 | | Jurisdiction | FDOT District One | |
| Input Data | | | Analysis Year | 2032 | |
| Base Conditions | | | Site Conditions | | |
| Length of segment, L (mi) | -- | | 1.001325758 | | |
| AADT (veh/day) | AADT _{MAX} = 17,800 (veh/day) | | 7,800 | | |
| Lane width (ft.) | 12 | | 10 | | |
| Shoulder width (ft.) | 6 | | Right Shld: 4 | Left Shld: 4 | |
| Shoulder type | Paved | | Right Shld: Paved | Left Shld: Paved | |
| Length of horizontal curve (mi) | 0 | | 0.0 | | |
| Radius of curvature (ft.) | 0 | | 0 | | |
| Spiral transition curve (present/not present) | Not Present | | Not Present | | |
| Superelevation variance (ft./ft.) | < 0.01 | | 0 | | |
| Grade (%) | 0 | | 0 | | |
| Driveway density (driveways/mile) | 5 | | 0 | | |
| Centerline rumble strips (present/not present) | Not Present | | Not Present | | |
| Passing lanes [present (1 lane) / present (2 lane) / not present] | Not Present | | Not Present | | |
| Two-way left-turn lane (present/not present) | Not Present | | Not Present | | |
| Roadside hazard rating (1-7 scale) | 3 | | 4 | | |
| Segment lighting (present/not present) | Not Present | | Not Present | | |
| Auto speed enforcement (present/not present) | Not Present | | Not Present | | |
| Calibration Factor, Cr | 1 | | 1.00 | | |

| Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments | | | | | | | | | | | | |
|--|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|-----------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | (1)x(2)x...x(11)x(12) |
| 1.17 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.361 |

| Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments | | | | | | | |
|---|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 2.087 | 0.24 | 1.000 | 2.087 | 1.36 | 1.00 | 2.840 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 0.670 | 1.36 | 1.00 | 0.912 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 1.417 | 1.36 | 1.00 | 1.928 |

| Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments | | | | | | |
|--|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 2.840 | 1.000 | 0.912 | 1.000 | 1.928 |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 0.344 | 0.038 | 0.035 | 0.184 | 0.355 |
| Collision with bicycle | 0.002 | 0.006 | 0.004 | 0.004 | 0.001 | 0.002 |
| Collision with pedestrian | 0.003 | 0.009 | 0.007 | 0.006 | 0.001 | 0.002 |
| Overtaken | 0.025 | 0.071 | 0.037 | 0.034 | 0.015 | 0.029 |
| Ran off road | 0.521 | 1.480 | 0.545 | 0.497 | 0.505 | 0.974 |
| Other single-vehicle collision | 0.021 | 0.060 | 0.007 | 0.006 | 0.029 | 0.056 |
| Total single-vehicle crashes | 0.693 | 1.968 | 0.638 | 0.582 | 0.735 | 1.417 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.241 | 0.100 | 0.091 | 0.072 | 0.139 |
| Head-on collision | 0.016 | 0.045 | 0.034 | 0.031 | 0.003 | 0.006 |
| Rear-end collision | 0.142 | 0.403 | 0.164 | 0.150 | 0.122 | 0.235 |
| Sideswipe collision | 0.037 | 0.105 | 0.038 | 0.035 | 0.038 | 0.073 |
| Other multiple-vehicle collision | 0.027 | 0.077 | 0.026 | 0.024 | 0.030 | 0.058 |
| Total multiple-vehicle crashes | 0.307 | 0.872 | 0.362 | 0.330 | 0.265 | 0.511 |

| Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments | | | | |
|---|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) | (5) |
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 2.8 | 1.001325758 | 2.8 |
| Fatal and Injury (FI) | 0.321 | 0.9 | 1.001325758 | 0.9 |
| Property Damage Only (PDO) | 0.679 | 1.9 | 1.001325758 | 1.9 |

No-Build 2032

Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments

| General Information | | Location Information | |
|---|--|----------------------|----------------------------|
| Analyst | Darlene Lam | Roadway | SR 70 |
| Agency or Company | American Consulting Professionals | Roadway Section | DC Bar Ranch Rd to Lyke Rd |
| Date Performed | 08/11/23 | Jurisdiction | FDOT District One |
| Input Data | | Analysis Year | 2032 |
| Length of segment, L (mi) | -- | Base Conditions | Site Conditions |
| AADT (veh/day) | AADT _{MAX} = 17,800 (veh/day) | -- | 2.574621212 |
| Lane width (ft.) | 12 | 12 | 10 |
| Shoulder width (ft.) | 6 | Right Shld: 4 | Left Shld: 4 |
| Shoulder type | Paved | Right Shld: Paved | Left Shld: Paved |
| Length of horizontal curve (mi) | 0 | 0.0 | |
| Radius of curvature (ft.) | 0 | 0 | |
| Spiral transition curve (present/not present) | Not Present | Not Present | |
| Superelevation variance (ft./ft.) | < 0.01 | 0 | |
| Grade (%) | 0 | 0 | |
| Driveway density (driveways/mile) | 5 | 1.6 | |
| Centerline rumble strips (present/not present) | Not Present | Not Present | |
| Passing lanes [present (1 lane) / present (2 lane) / not present] | Not Present | Not Present | |
| Two-way left-turn lane (present/not present) | Not Present | Not Present | |
| Roadside hazard rating (1-7 scale) | 3 | 4 | |
| Segment lighting (present/not present) | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | Not Present | Not Present | |
| Calibration Factor, Cr | 1 | 1.00 | |

Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|---------------------|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|-----------------------|
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | (1)x(2)x...x(11)x(12) |
| 1.17 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.361 |

Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|----------------------------|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 5.365 | 0.09 | 1.000 | 5.365 | 1.36 | 1.00 | 7.303 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 1.722 | 1.36 | 1.00 | 2.344 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 3.643 | 1.36 | 1.00 | 4.959 |

Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|----------------------------------|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 7.303 | 1.000 | 2.344 | 1.000 | 4.959 |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 0.884 | 0.038 | 0.089 | 0.184 | 0.912 |
| Collision with bicycle | 0.002 | 0.015 | 0.004 | 0.009 | 0.001 | 0.005 |
| Collision with pedestrian | 0.003 | 0.022 | 0.007 | 0.016 | 0.001 | 0.005 |
| Overtuned | 0.025 | 0.183 | 0.037 | 0.087 | 0.015 | 0.074 |
| Ran off road | 0.521 | 3.805 | 0.545 | 1.278 | 0.505 | 2.504 |
| Other single-vehicle collision | 0.021 | 0.153 | 0.007 | 0.016 | 0.029 | 0.144 |
| Total single-vehicle crashes | 0.693 | 5.061 | 0.638 | 1.496 | 0.735 | 3.645 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.621 | 0.100 | 0.234 | 0.072 | 0.357 |
| Head-on collision | 0.016 | 0.117 | 0.034 | 0.080 | 0.003 | 0.015 |
| Rear-end collision | 0.142 | 1.037 | 0.164 | 0.384 | 0.122 | 0.605 |
| Sideswipe collision | 0.037 | 0.270 | 0.038 | 0.089 | 0.038 | 0.188 |
| Other multiple-vehicle collision | 0.027 | 0.197 | 0.026 | 0.061 | 0.030 | 0.149 |
| Total multiple-vehicle crashes | 0.307 | 2.242 | 0.362 | 0.849 | 0.265 | 1.314 |

Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) |
|----------------------------|--|--|-----------------------------|------------------------------|
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 7.3 | 2.574621212 | 2.8 |
| Fatal and Injury (FI) | 0.321 | 2.3 | 2.574621212 | 0.9 |
| Property Damage Only (PDO) | 0.679 | 5.0 | 2.574621212 | 1.9 |

No-Build 2032

Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments

| General Information | | Location Information | |
|---|-----------------------------------|----------------------|---------------------------------------|
| Analyst | Darlene Lam | Roadway | SR 70 |
| Agency or Company | American Consulting Professionals | Roadway Section | Lyke Rd to Southern Leg of CR 721 |
| Date Performed | 08/11/23 | Jurisdiction | FDOT District One |
| Input Data | | Analysis Year | 2032 |
| Length of segment, L (mi) | | Base Conditions | Site Conditions |
| AADT (veh/day) | | -- | 2.362310606 |
| AADT _{MAX} = 17,800 (veh/day) | | -- | 7,800 |
| Lane width (ft.) | | 12 | 10 |
| Shoulder width (ft.) | | 6 | Right Shld: 4 Left Shld: 4 |
| Shoulder type | | Paved | Right Shld: Paved Left Shld: Paved |
| Length of horizontal curve (mi) | | 0 | 0.3 |
| Radius of curvature (ft.) | | 0 | 2865 |
| Spiral transition curve (present/not present) | | Not Present | Not Present |
| Superelevation variance (ft./ft.) | | < 0.01 | 0 |
| Grade (%) | | 0 | 0 |
| Driveway density (driveways/mile) | | 5 | 2.1 |
| Centerline rumble strips (present/not present) | | Not Present | Not Present |
| Passing lanes [present (1 lane) / present (2 lane) / not present] | | Not Present | Not Present |
| Two-way left-turn lane (present/not present) | | Not Present | Not Present |
| Roadside hazard rating (1-7 scale) | | 3 | 4 |
| Segment lighting (present/not present) | | Not Present | Not Present |
| Auto speed enforcement (present/not present) | | Not Present | Not Present |
| Calibration Factor, Cr | | 1 | 1.00 |

Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|---------------------|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|-----------------------|
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMR 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | (1)x(2)x...x(11)x(12) |
| 1.17 | 1.09 | 1.05 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.433 |

Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|----------------------------|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 4.923 | 0.10 | 1.000 | 4.923 | 1.43 | 1.00 | 7.056 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 1.580 | 1.43 | 1.00 | 2.265 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 3.343 | 1.43 | 1.00 | 4.791 |

Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|----------------------------------|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 7.056 | 1.000 | 2.265 | 1.000 | 4.791 |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 0.854 | 0.038 | 0.086 | 0.184 | 0.882 |
| Collision with bicycle | 0.002 | 0.014 | 0.004 | 0.009 | 0.001 | 0.005 |
| Collision with pedestrian | 0.003 | 0.021 | 0.007 | 0.016 | 0.001 | 0.005 |
| Overtuned | 0.025 | 0.176 | 0.037 | 0.084 | 0.015 | 0.072 |
| Ran off road | 0.521 | 3.676 | 0.545 | 1.234 | 0.505 | 2.420 |
| Other single-vehicle collision | 0.021 | 0.148 | 0.007 | 0.016 | 0.029 | 0.139 |
| Total single-vehicle crashes | 0.693 | 4.890 | 0.638 | 1.445 | 0.735 | 3.522 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.600 | 0.100 | 0.227 | 0.072 | 0.345 |
| Head-on collision | 0.016 | 0.113 | 0.034 | 0.077 | 0.003 | 0.014 |
| Rear-end collision | 0.142 | 1.002 | 0.164 | 0.371 | 0.122 | 0.585 |
| Sideswipe collision | 0.037 | 0.261 | 0.038 | 0.086 | 0.038 | 0.182 |
| Other multiple-vehicle collision | 0.027 | 0.191 | 0.026 | 0.059 | 0.030 | 0.144 |
| Total multiple-vehicle crashes | 0.307 | 2.166 | 0.362 | 0.820 | 0.265 | 1.270 |

Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) |
|----------------------------|--|--|-----------------------------|------------------------------|
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 7.1 | 2.362310606 | 3.0 |
| Fatal and Injury (FI) | 0.321 | 2.3 | 2.362310606 | 1.0 |
| Property Damage Only (PDO) | 0.679 | 4.8 | 2.362310606 | 2.0 |

No-Build 2032

| Worksheet 2A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|---|--|--|--|----------------------------|
| General Information | | Location Information | | |
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/11/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 JC Durrance Rd FDOT District One 2032 | |
| Input Data | | Base Conditions | Site Conditions | |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST | |
| AADT _{major} (veh/day) | AADT _{MAX} = 19,500 (veh/day) | -- | 7,800 | |
| AADT _{minor} (veh/day) | AADT _{MAX} = 4,300 (veh/day) | -- | 200 | |
| Intersection skew angle (degrees) [If 4ST, does skew differ for minor legs?] | No | 0 | Skew for Leg 1 (All): | Skew for Leg 2 (4ST only): |
| Number of signalized or uncontrolled approaches with a left-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Number of signalized or uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Intersection lighting (present/not present) | | Not Present | Not Present | |
| Calibration Factor, C _i | | 1.00 | 1.27 | |

| Worksheet 2B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|--|---|--|---|---|
| (1) CMF for Intersection Skew Angle CMF ₁₁ from Equations 10-22 or 10-23 | (2) CMF for Left-Turn Lanes CMF ₂₁ from Table 10-13 | (3) CMF for Right-Turn Lanes CMF ₃₁ from Table 10-14 | (4) CMF for Lighting CMF ₄₁ from Equation 10-24 | (5) Combined CMF CMF _{COMB} (1)*(2)*(3)*(4) |
| 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

| Worksheet 2C -- Intersection Crashes for Rural Two-Lane Two-Way Roadway Intersections | | | | | | | |
|---|--|---|---|--|--|---|---|
| (1) Crash Severity Level | (2) N _{adj 3ST, 4ST or 4SG} from Equations 10-8, 10-9, or 10-10 | (3) Overdispersion Parameter, k from Section 10.6.2 | (4) Crash Severity Distribution from Table 10-5 | (5) N _{adj 3ST, 4ST or 4SG by Severity Distribution} (2) _{TOTAL} * (4) | (6) Combined CMFs from (5) of Worksheet 2B | (7) Calibration Factor, C _i | (8) Predicted average crash frequency, N _{predicted int} (5)*(6)*(7) |
| Total | 0.832 | 0.54 | 1.000 | 0.832 | 1.00 | 1.27 | 1.057 |
| Fatal and Injury (FI) | -- | -- | 0.415 | 0.345 | 1.00 | 1.27 | 0.438 |
| Property Damage Only (PDO) | -- | -- | 0.585 | 0.487 | 1.00 | 1.27 | 0.618 |

| Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Road Intersections | | | | | | |
|--|---|---|--|--|---|---|
| (1) Collision Type | (2) Proportion of Collision Type _{TOTAL} from Table 10-6 | (3) N _{predicted int (TOTAL)} (crashes/year) | (4) Proportion of Collision Type _{FI} from Table 10-6 | (5) N _{predicted int (FI)} (crashes/year) | (6) Proportion of Collision Type _{PDO} from Table 10-6 | (7) N _{predicted int (PDO)} (crashes/year) |
| Total | 1.000 | 1.057 | 1.000 | 0.438 | 1.000 | 0.618 |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.019 | 0.020 | 0.008 | 0.004 | 0.026 | 0.016 |
| Collision with bicycle | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Collision with pedestrian | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Overturned | 0.013 | 0.014 | 0.022 | 0.010 | 0.007 | 0.004 |
| Ran off road | 0.244 | 0.258 | 0.240 | 0.105 | 0.247 | 0.153 |
| Other single-vehicle collision | 0.016 | 0.017 | 0.011 | 0.005 | 0.020 | 0.012 |
| Total single-vehicle crashes | 0.294 | 0.311 | 0.283 | 0.124 | 0.302 | 0.187 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.237 | 0.250 | 0.275 | 0.121 | 0.210 | 0.130 |
| Head-on collision | 0.052 | 0.055 | 0.081 | 0.036 | 0.032 | 0.020 |
| Rear-end collision | 0.278 | 0.294 | 0.260 | 0.114 | 0.292 | 0.180 |
| Sideswipe collision | 0.097 | 0.102 | 0.051 | 0.022 | 0.131 | 0.081 |
| Other multiple-vehicle collision | 0.042 | 0.044 | 0.050 | 0.022 | 0.033 | 0.020 |
| Total multiple-vehicle crashes | 0.706 | 0.746 | 0.717 | 0.314 | 0.698 | 0.431 |

| Worksheet 2E -- Summary Results for Rural Two-Lane Two-Way Road Intersections | | |
|---|--|--|
| (1) Crash severity level | (2) Crash Severity Distribution (proportion) (4) from Worksheet 2C | (3) Predicted average crash frequency (crashes / year) (8) from Worksheet 2C |
| Total | 1.000 | 1.1 |
| Fatal and Injury (FI) | 0.415 | 0.4 |
| Property Damage Only (PDO) | 0.585 | 0.6 |

No-Build 2032

| Worksheet 2A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|---|--|--|---|--|
| General Information | | Location Information | | |
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/11/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Greenbrier Ln FDOT District One 2032 | |
| Input Data | | Base Conditions | Site Conditions | |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST | |
| AADT _{major} (veh/day) | AADT _{MAX} = 19,500 (veh/day) | -- | 7,800 | |
| AADT _{minor} (veh/day) | AADT _{MAX} = 4,300 (veh/day) | -- | 150 | |
| Intersection skew angle (degrees) [If 4ST, does skew differ for minor legs?] | No | 0 | Skew for Leg 1 (All): Skew for Leg 2 (4ST only): | |
| Number of signalized or uncontrolled approaches with a left-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Number of signalized or uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Intersection lighting (present/not present) | | Not Present | Not Present | |
| Calibration Factor, C _i | | 1.00 | 1.27 | |

| Worksheet 2B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|--|---|--|---|---|
| (1) CMF for Intersection Skew Angle CMF ₁₁ from Equations 10-22 or 10-23 | (2) CMF for Left-Turn Lanes CMF ₂₁ from Table 10-13 | (3) CMF for Right-Turn Lanes CMF ₃₁ from Table 10-14 | (4) CMF for Lighting CMF ₄₁ from Equation 10-24 | (5) Combined CMF CMF _{COMB} (1)*(2)*(3)*(4) |
| 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

| Worksheet 2C -- Intersection Crashes for Rural Two-Lane Two-Way Roadway Intersections | | | | | | | |
|---|--|---|---|--|--|---|---|
| (1) Crash Severity Level | (2) N _{adj 3ST, 4ST or 4SG} from Equations 10-8, 10-9, or 10-10 | (3) Overdispersion Parameter, k from Section 10.6.2 | (4) Crash Severity Distribution from Table 10-5 | (5) N _{adj 3ST, 4ST or 4SG by Severity Distribution} (2) _{TOTAL} * (4) | (6) Combined CMFs from (5) of Worksheet 2B | (7) Calibration Factor, C _i | (8) Predicted average crash frequency, N _{predicted int} (5)*(6)*(7) |
| Total | 0.723 | 0.54 | 1.000 | 0.723 | 1.00 | 1.27 | 0.918 |
| Fatal and Injury (FI) | -- | -- | 0.415 | 0.300 | 1.00 | 1.27 | 0.381 |
| Property Damage Only (PDO) | -- | -- | 0.585 | 0.423 | 1.00 | 1.27 | 0.537 |

| Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Road Intersections | | | | | | |
|--|---|---|--|--|---|---|
| (1) Collision Type | (2) Proportion of Collision Type _{TOTAL} from Table 10-6 | (3) N _{predicted int (TOTAL)} (crashes/year) | (4) Proportion of Collision Type _{FI} from Table 10-6 | (5) N _{predicted int (FI)} (crashes/year) | (6) Proportion of Collision Type _{PDO} from Table 10-6 | (7) N _{predicted int (PDO)} (crashes/year) |
| Total | 1.000 | 0.918 | 1.000 | 0.381 | 1.000 | 0.537 |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.019 | 0.017 | 0.008 | 0.003 | 0.026 | 0.014 |
| Collision with bicycle | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Collision with pedestrian | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Overturned | 0.013 | 0.012 | 0.022 | 0.008 | 0.007 | 0.004 |
| Ran off road | 0.244 | 0.224 | 0.240 | 0.091 | 0.247 | 0.133 |
| Other single-vehicle collision | 0.016 | 0.015 | 0.011 | 0.004 | 0.020 | 0.011 |
| Total single-vehicle crashes | 0.294 | 0.270 | 0.283 | 0.108 | 0.302 | 0.162 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.237 | 0.217 | 0.275 | 0.105 | 0.210 | 0.113 |
| Head-on collision | 0.052 | 0.048 | 0.081 | 0.031 | 0.032 | 0.017 |
| Rear-end collision | 0.278 | 0.255 | 0.260 | 0.099 | 0.292 | 0.157 |
| Sideswipe collision | 0.097 | 0.089 | 0.051 | 0.019 | 0.131 | 0.070 |
| Other multiple-vehicle collision | 0.042 | 0.039 | 0.050 | 0.019 | 0.033 | 0.018 |
| Total multiple-vehicle crashes | 0.706 | 0.648 | 0.717 | 0.273 | 0.698 | 0.375 |

| Worksheet 2E -- Summary Results for Rural Two-Lane Two-Way Road Intersections | | |
|---|--|--|
| (1) Crash severity level | (2) Crash Severity Distribution (proportion) (4) from Worksheet 2C | (3) Predicted average crash frequency (crashes / year) (8) from Worksheet 2C |
| Total | 1.000 | 0.9 |
| Fatal and Injury (FI) | 0.415 | 0.4 |
| Property Damage Only (PDO) | 0.585 | 0.5 |

No-Build 2032

| Worksheet 2A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|---|--|--|---|--|
| General Information | | Location Information | | |
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/11/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 DC Bar Ranch Rd FDOT District One 2032 | |
| Input Data | | Base Conditions | Site Conditions | |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST | |
| AADT _{major} (veh/day) | AADT _{MAX} = 19,500 (veh/day) | -- | 7,800 | |
| AADT _{minor} (veh/day) | AADT _{MAX} = 4,300 (veh/day) | -- | 150 | |
| Intersection skew angle (degrees) [If 4ST, does skew differ for minor legs?] | No | 0 | Skew for Leg 1 (All): Skew for Leg 2 (4ST only): | |
| Number of signalized or uncontrolled approaches with a left-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Number of signalized or uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Intersection lighting (present/not present) | | Not Present | Not Present | |
| Calibration Factor, C _i | | 1.00 | 1.27 | |

| Worksheet 2B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|--|---|--|---|---|
| (1) CMF for Intersection Skew Angle CMF ₁₁ from Equations 10-22 or 10-23 | (2) CMF for Left-Turn Lanes CMF ₂₁ from Table 10-13 | (3) CMF for Right-Turn Lanes CMF ₃₁ from Table 10-14 | (4) CMF for Lighting CMF ₄₁ from Equation 10-24 | (5) Combined CMF CMF _{COMB} (1)*(2)*(3)*(4) |
| 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

| Worksheet 2C -- Intersection Crashes for Rural Two-Lane Two-Way Roadway Intersections | | | | | | | |
|---|--|---|---|--|--|---|---|
| (1) Crash Severity Level | (2) N _{adj 3ST, 4ST or 4SG} from Equations 10-8, 10-9, or 10-10 | (3) Overdispersion Parameter, k from Section 10.6.2 | (4) Crash Severity Distribution from Table 10-5 | (5) N _{adj 3ST, 4ST or 4SG} by Severity Distribution (2) _{TOTAL} * (4) | (6) Combined CMFs from (5) of Worksheet 2B | (7) Calibration Factor, C _i | (8) Predicted average crash frequency, N _{predicted int} (5)*(6)*(7) |
| Total | 0.723 | 0.54 | 1.000 | 0.723 | 1.00 | 1.27 | 0.918 |
| Fatal and Injury (FI) | -- | -- | 0.415 | 0.300 | 1.00 | 1.27 | 0.381 |
| Property Damage Only (PDO) | -- | -- | 0.585 | 0.423 | 1.00 | 1.27 | 0.537 |

| Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Road Intersections | | | | | | |
|--|---|---|--|--|---|---|
| (1) Collision Type | (2) Proportion of Collision Type _{TOTAL} from Table 10-6 | (3) N _{predicted int (TOTAL)} (crashes/year) | (4) Proportion of Collision Type _{FI} from Table 10-6 | (5) N _{predicted int (FI)} (crashes/year) | (6) Proportion of Collision Type _{PDO} from Table 10-6 | (7) N _{predicted int (PDO)} (crashes/year) |
| Total | 1.000 | 0.918 | 1.000 | 0.381 | 1.000 | 0.537 |
| | | (2)x(3) _{TOTAL} | | (4)x(5) _{FI} | | (6)x(7) _{PDO} |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.019 | 0.017 | 0.008 | 0.003 | 0.026 | 0.014 |
| Collision with bicycle | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Collision with pedestrian | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Overturned | 0.013 | 0.012 | 0.022 | 0.008 | 0.007 | 0.004 |
| Ran off road | 0.244 | 0.224 | 0.240 | 0.091 | 0.247 | 0.133 |
| Other single-vehicle collision | 0.016 | 0.015 | 0.011 | 0.004 | 0.020 | 0.011 |
| Total single-vehicle crashes | 0.294 | 0.270 | 0.283 | 0.108 | 0.302 | 0.162 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.237 | 0.217 | 0.275 | 0.105 | 0.210 | 0.113 |
| Head-on collision | 0.052 | 0.048 | 0.081 | 0.031 | 0.032 | 0.017 |
| Rear-end collision | 0.278 | 0.255 | 0.260 | 0.099 | 0.292 | 0.157 |
| Sideswipe collision | 0.097 | 0.089 | 0.051 | 0.019 | 0.131 | 0.070 |
| Other multiple-vehicle collision | 0.042 | 0.039 | 0.050 | 0.019 | 0.033 | 0.018 |
| Total multiple-vehicle crashes | 0.706 | 0.648 | 0.717 | 0.273 | 0.698 | 0.375 |

| Worksheet 2E -- Summary Results for Rural Two-Lane Two-Way Road Intersections | | |
|---|--|--|
| (1) Crash severity level | (2) Crash Severity Distribution (proportion) (4) from Worksheet 2C | (3) Predicted average crash frequency (crashes / year) (8) from Worksheet 2C |
| Total | 1.000 | 0.9 |
| Fatal and Injury (FI) | 0.415 | 0.4 |
| Property Damage Only (PDO) | 0.585 | 0.5 |

No-Build 2032

| Worksheet 2A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|---|--|--|---|--|
| General Information | | Location Information | | |
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/11/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Lykes Rd FDOT District One 2032 | |
| Input Data | | Base Conditions | Site Conditions | |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST | |
| AADT _{major} (veh/day) | AADT _{MAX} = 19,500 (veh/day) | -- | 7,800 | |
| AADT _{minor} (veh/day) | AADT _{MAX} = 4,300 (veh/day) | -- | 150 | |
| Intersection skew angle (degrees) [If 4ST, does skew differ for minor legs?] | No | 0 | Skew for Leg 1 (All): Skew for Leg 2 (4ST only): | |
| Number of signalized or uncontrolled approaches with a left-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Number of signalized or uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Intersection lighting (present/not present) | | Not Present | Not Present | |
| Calibration Factor, C _i | | 1.00 | 1.27 | |

| Worksheet 2B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|--|---|--|---|---|
| (1) CMF for Intersection Skew Angle CMF ₁₁ from Equations 10-22 or 10-23 | (2) CMF for Left-Turn Lanes CMF ₂₁ from Table 10-13 | (3) CMF for Right-Turn Lanes CMF ₃₁ from Table 10-14 | (4) CMF for Lighting CMF ₄₁ from Equation 10-24 | (5) Combined CMF CMF _{COMB} (1)*(2)*(3)*(4) |
| 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

| Worksheet 2C -- Intersection Crashes for Rural Two-Lane Two-Way Roadway Intersections | | | | | | | |
|---|--|---|---|--|--|---|---|
| (1) Crash Severity Level | (2) N _{adj 3ST, 4ST or 4SG} from Equations 10-8, 10-9, or 10-10 | (3) Overdispersion Parameter, k from Section 10.6.2 | (4) Crash Severity Distribution from Table 10-5 | (5) N _{adj 3ST, 4ST or 4SG by Severity Distribution} (2) _{TOTAL} * (4) | (6) Combined CMFs from (5) of Worksheet 2B | (7) Calibration Factor, C _i | (8) Predicted average crash frequency, N _{predicted int} (5)*(6)*(7) |
| Total | 0.723 | 0.54 | 1.000 | 0.723 | 1.00 | 1.27 | 0.918 |
| Fatal and Injury (FI) | -- | -- | 0.415 | 0.300 | 1.00 | 1.27 | 0.381 |
| Property Damage Only (PDO) | -- | -- | 0.585 | 0.423 | 1.00 | 1.27 | 0.537 |

| Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Road Intersections | | | | | | |
|--|---|---|--|--|---|---|
| (1) Collision Type | (2) Proportion of Collision Type _{TOTAL} from Table 10-6 | (3) N _{predicted int (TOTAL)} (crashes/year) | (4) Proportion of Collision Type _{FI} from Table 10-6 | (5) N _{predicted int (FI)} (crashes/year) | (6) Proportion of Collision Type _{PDO} from Table 10-6 | (7) N _{predicted int (PDO)} (crashes/year) |
| Total | 1.000 | 0.918 | 1.000 | 0.381 | 1.000 | 0.537 |
| | | (2)x(3) _{TOTAL} | | (4)x(5) _{FI} | | (6)x(7) _{PDO} |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.019 | 0.017 | 0.008 | 0.003 | 0.026 | 0.014 |
| Collision with bicycle | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Collision with pedestrian | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Overturned | 0.013 | 0.012 | 0.022 | 0.008 | 0.007 | 0.004 |
| Ran off road | 0.244 | 0.224 | 0.240 | 0.091 | 0.247 | 0.133 |
| Other single-vehicle collision | 0.016 | 0.015 | 0.011 | 0.004 | 0.020 | 0.011 |
| Total single-vehicle crashes | 0.294 | 0.270 | 0.283 | 0.108 | 0.302 | 0.162 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.237 | 0.217 | 0.275 | 0.105 | 0.210 | 0.113 |
| Head-on collision | 0.052 | 0.048 | 0.081 | 0.031 | 0.032 | 0.017 |
| Rear-end collision | 0.278 | 0.255 | 0.260 | 0.099 | 0.292 | 0.157 |
| Sideswipe collision | 0.097 | 0.089 | 0.051 | 0.019 | 0.131 | 0.070 |
| Other multiple-vehicle collision | 0.042 | 0.039 | 0.050 | 0.019 | 0.033 | 0.018 |
| Total multiple-vehicle crashes | 0.706 | 0.648 | 0.717 | 0.273 | 0.698 | 0.375 |

| Worksheet 2E -- Summary Results for Rural Two-Lane Two-Way Road Intersections | | |
|---|--|--|
| (1) Crash severity level | (2) Crash Severity Distribution (proportion) (4) from Worksheet 2C | (3) Predicted average crash frequency (crashes / year) (8) from Worksheet 2C |
| Total | 1.000 | 0.9 |
| Fatal and Injury (FI) | 0.415 | 0.4 |
| Property Damage Only (PDO) | 0.585 | 0.5 |

No-Build 2032

| Worksheet 2A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|---|--|--|--|-------------------------------|
| General Information | | Location Information | | |
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/11/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Southern Leg of CR 721 FDOT District One 2032 | |
| Input Data | | Base Conditions | Site Conditions | |
| Intersection type (3ST, 4ST, 4SG) | | -- | 4ST | |
| AADT _{major} (veh/day) | AADT _{MAX} = 14,700 (veh/day) | -- | 7,800 | |
| AADT _{minor} (veh/day) | AADT _{MAX} = 3,500 (veh/day) | -- | 2,700 | |
| Intersection skew angle (degrees) [If 4ST, does skew differ for minor legs?] | Yes | 0 | Skew for Leg 1 (All): 36 | Skew for Leg 2 (4ST only): 36 |
| Number of signalized or uncontrolled approaches with a left-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Number of signalized or uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Intersection lighting (present/not present) | | Not Present | Not Present | |
| Calibration Factor, C _i | | 1.00 | 0.74 | |

| Worksheet 2B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|--|---|--|---|---|
| (1) CMF for Intersection Skew Angle CMF ₁₁ from Equations 10-22 or 10-23 | (2) CMF for Left-Turn Lanes CMF ₂₁ from Table 10-13 | (3) CMF for Right-Turn Lanes CMF ₃₁ from Table 10-14 | (4) CMF for Lighting CMF ₄₁ from Equation 10-24 | (5) Combined CMF CMF _{COMB} (1)*(2)*(3)*(4) |
| 1.21 | 1.00 | 1.00 | 1.00 | 1.21 |

| Worksheet 2C -- Intersection Crashes for Rural Two-Lane Two-Way Roadway Intersections | | | | | | | |
|---|--|---|---|--|--|---|---|
| (1) Crash Severity Level | (2) N _{adj 3ST, 4ST or 4SG} from Equations 10-8, 10-9, or 10-10 | (3) Overdispersion Parameter, k from Section 10.6.2 | (4) Crash Severity Distribution from Table 10-5 | (5) N _{adj 3ST, 4ST or 4SG by Severity Distribution} (2) _{TOTAL} * (4) | (6) Combined CMFs from (5) of Worksheet 2B | (7) Calibration Factor, C _i | (8) Predicted average crash frequency, N _{predicted int} (5)*(6)*(7) |
| Total | 5,138 | 0.24 | 1,000 | 5,138 | 1.21 | 0.74 | 4,618 |
| Fatal and Injury (FI) | -- | -- | 0.431 | 2,215 | 1.21 | 0.74 | 1,991 |
| Property Damage Only (PDO) | -- | -- | 0.569 | 2,924 | 1.21 | 0.74 | 2,628 |

| Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Road Intersections | | | | | | |
|--|---|---|--|--|---|---|
| (1) Collision Type | (2) Proportion of Collision Type _{TOTAL} from Table 10-6 | (3) N _{predicted int (TOTAL)} (crashes/year) | (4) Proportion of Collision Type _{FI} from Table 10-6 | (5) N _{predicted int (FI)} (crashes/year) | (6) Proportion of Collision Type _{PDO} from Table 10-6 | (7) N _{predicted int (PDO)} (crashes/year) |
| | | (8) _{TOTAL} from Worksheet 2C | | (8) _{FI} from Worksheet 2C | | (8) _{PDO} from Worksheet 2C |
| Total | 1.000 | 4,618 | 1.000 | 1,991 | 1.000 | 2,628 |
| | | (2)x(3) _{TOTAL} | | (4)x(5) _{FI} | | (6)x(7) _{PDO} |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.010 | 0.046 | 0.006 | 0.012 | 0.014 | 0.037 |
| Collision with bicycle | 0.001 | 0.005 | 0.001 | 0.002 | 0.001 | 0.003 |
| Collision with pedestrian | 0.001 | 0.005 | 0.001 | 0.002 | 0.001 | 0.003 |
| Overturned | 0.005 | 0.023 | 0.006 | 0.012 | 0.004 | 0.011 |
| Ran off road | 0.122 | 0.563 | 0.094 | 0.187 | 0.144 | 0.378 |
| Other single-vehicle collision | 0.008 | 0.037 | 0.004 | 0.008 | 0.010 | 0.026 |
| Total single-vehicle crashes | 0.147 | 0.679 | 0.112 | 0.223 | 0.174 | 0.457 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.431 | 1,991 | 0.532 | 1,059 | 0.354 | 0.930 |
| Head-on collision | 0.040 | 0.185 | 0.060 | 0.119 | 0.025 | 0.066 |
| Rear-end collision | 0.242 | 1,118 | 0.210 | 0.418 | 0.266 | 0.699 |
| Sideswipe collision | 0.101 | 0.466 | 0.044 | 0.088 | 0.144 | 0.378 |
| Other multiple-vehicle collision | 0.039 | 0.180 | 0.042 | 0.084 | 0.037 | 0.097 |
| Total multiple-vehicle crashes | 0.853 | 3,939 | 0.888 | 1,768 | 0.826 | 2,171 |

| Worksheet 2E -- Summary Results for Rural Two-Lane Two-Way Road Intersections | | |
|---|--|--|
| (1) Crash severity level | (2) Crash Severity Distribution (proportion) (4) from Worksheet 2C | (3) Predicted average crash frequency (crashes / year) (8) from Worksheet 2C |
| Total | 1.000 | 4.6 |
| Fatal and Injury (FI) | 0.431 | 2.0 |
| Property Damage Only (PDO) | 0.569 | 2.6 |

No-Build 2032

Worksheet 3A -- Predicted and Observed Crashes by Severity and Site Type Using the Site-Specific EB Method

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|--------------------------|--|----------------------|-----------------------|---|-----------------------------|---|--|
| Site type | Predicted average crash frequency (crashes/year) | | | Observed crashes, $N_{observed}$ (crashes/year) | Overdispersion Parameter, k | Weighted adjustment, w Equation A-5 from Part C Appendix | Expected average crash frequency, Equation A-4 from Part C Appendix |
| | $N_{predicted}$ (TOTAL) | $N_{predicted}$ (FI) | $N_{predicted}$ (PDO) | | | | |
| ROADWAY SEGMENTS | | | | | | | |
| Segment1 | 0.242 | 0.078 | 0.164 | | 2.769 | 0.599 | 0.1 |
| Segment2 | 4.644 | 1.491 | 3.153 | | 0.144 | 0.599 | 2.8 |
| Segment3 | 2.840 | 0.912 | 1.928 | | 0.236 | 0.599 | 1.7 |
| Segment4 | 7.303 | 2.344 | 4.959 | | 0.092 | 0.599 | 4.4 |
| Segment5 | 7.056 | 2.265 | 4.791 | | 0.100 | 0.587 | 4.1 |
| Segment6 | | | | | | 1.000 | 0.0 |
| Segment7 | | | | | | 1.000 | 0.0 |
| Segment8 | | | | | | 1.000 | 0.0 |
| INTERSECTIONS | | | | | | | |
| Intersection1 | 0.918 | 0.381 | 0.537 | | 0.540 | 0.669 | 0.6 |
| Intersection2 | 1.057 | 0.438 | 0.618 | | 0.540 | 0.637 | 0.7 |
| Intersection3 | 0.918 | 0.381 | 0.537 | | 0.540 | 0.669 | 0.6 |
| Intersection4 | 0.918 | 0.381 | 0.537 | | 0.540 | 0.669 | 0.6 |
| Intersection5 | 0.918 | 0.381 | 0.537 | | 0.540 | 0.669 | 0.6 |
| Intersection6 | 4.618 | 1.991 | 2.628 | | 0.240 | 0.474 | 2.2 |
| Intersection7 | | | | | | 1.000 | 0.0 |
| Intersection8 | | | | | | 1.000 | 0.0 |
| COMBINED (sum of column) | 31.430 | 11.042 | 20.389 | 0 | -- | -- | 18.5 |

Worksheet 3B -- Site-Specific EB Method Summary Results

| (1) | (2) | (3) |
|----------------------------|---|--|
| Crash severity level | $N_{predicted}$ | $N_{expected}$ |
| Total | (2) _{COMB} from Worksheet 3A 31.430 | (8) _{COMB} from Worksheet 3A 18.5 |
| Fatal and Injury (FI) | (3) _{COMB} from Worksheet 3A 11.042 | (3) _{TOTAL} * (2) _{FI} / (2) _{TOTAL} 6.5 |
| Property Damage Only (PDO) | (4) _{COMB} from Worksheet 3A 20.389 | (3) _{TOTAL} * (2) _{PDO} / (2) _{TOTAL} 12.0 |

No-Build 2032

Worksheet 4A -- Predicted and Observed Crashes by Severity and Site Type Using the Project-Level EB Method

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|-------------------------|--|----------------------|-----------------------|---|-----------------------------|--------------------------|------------------------------|---------------|---------------|---------------|---------------|---------------|
| Site type | Predicted average crash frequency (crashes/year) | | | Observed crashes, $N_{observed}$ (crashes/year) | Overdispersion Parameter, k | N_{w0} | N_{w1} | W_0 | N_0 | w_1 | N_1 | N_{pcomb} |
| | $N_{predicted}$ (TOTAL) | $N_{predicted}$ (FI) | $N_{predicted}$ (PDO) | | | Equation A-8 $(6)*(2)^2$ | Equation A-9 $sqrt((6)*(2))$ | Equation A-10 | Equation A-11 | Equation A-12 | Equation A-13 | Equation A-14 |
| ROADWAY SEGMENTS | | | | | | | | | | | | |
| Segment 1 | 0.242 | 0.078 | 0.164 | -- | 2.769 | 0.162 | 0.818 | -- | -- | -- | -- | -- |
| Segment 2 | 4.644 | 1.491 | 3.153 | -- | 0.144 | 3.108 | 0.818 | -- | -- | -- | -- | -- |
| Segment 3 | 2.840 | 0.912 | 1.928 | -- | 0.236 | 1.901 | 0.818 | -- | -- | -- | -- | -- |
| Segment 4 | 7.303 | 2.344 | 4.959 | -- | 0.092 | 4.888 | 0.818 | -- | -- | -- | -- | -- |
| Segment 5 | 7.056 | 2.265 | 4.791 | -- | 0.100 | 4.974 | 0.840 | -- | -- | -- | -- | -- |
| Segment 6 | | | | -- | | | | -- | -- | -- | -- | -- |
| Segment 7 | | | | -- | | | | -- | -- | -- | -- | -- |
| Segment 8 | | | | -- | | | | -- | -- | -- | -- | -- |
| INTERSECTIONS | | | | | | | | | | | | |
| Intersection 1 | 0.918 | 0.381 | 0.537 | -- | 0.540 | 0.455 | 0.704 | -- | -- | -- | -- | -- |
| Intersection 2 | 1.057 | 0.438 | 0.618 | -- | 0.540 | 0.603 | 0.755 | -- | -- | -- | -- | -- |
| Intersection 3 | 0.918 | 0.381 | 0.537 | -- | 0.540 | 0.455 | 0.704 | -- | -- | -- | -- | -- |
| Intersection 4 | 0.918 | 0.381 | 0.537 | -- | 0.540 | 0.455 | 0.704 | -- | -- | -- | -- | -- |
| Intersection 5 | 0.918 | 0.381 | 0.537 | -- | 0.540 | 0.455 | 0.704 | -- | -- | -- | -- | -- |
| Intersection 6 | 4.618 | 1.991 | 2.628 | -- | 0.240 | 5.119 | 1.053 | -- | -- | -- | -- | -- |
| Intersection 7 | | | | -- | | | | -- | -- | -- | -- | -- |
| Intersection 8 | | | | -- | | | | -- | -- | -- | -- | -- |
| COMBINED | 31.430 | 11.042 | 20.389 | | -- | 22.575 | 8.736 | 0.582 | 18.292 | 0.782 | 24.594 | 21.443 |

Worksheet 4B -- Project-Level EB Method Summary Results

| (1) | (2) | (3) |
|----------------------------|---|--|
| Crash severity level | $N_{predicted}$ | $N_{expected}$ |
| Total | (2) _{COMB} from Worksheet 4A 31.430 | (13) _{COMB} from Worksheet 4A 21.4 |
| Fatal and injury (FI) | (3) _{COMB} from Worksheet 4A 11.042 | (3) _{TOTAL} * (2) _{FI} / (2) _{TOTAL} 7.5 |
| Property damage only (PDO) | (4) _{COMB} from Worksheet 4A 20.389 | (3) _{TOTAL} * (2) _{PDO} / (2) _{TOTAL} 13.9 |

No-Build 2052

| Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments | | | | | |
|--|---|--|----------------------|--------------------------------------|------------------|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | African Consulting Professionals a Consor Com | | Roadway Section | Lonesome Island Rd to Jc Durrance Rd | |
| Date Performed | 08/11/23 | | Jurisdiction | FDOT District One | |
| Input Data | | | Analysis Year | 2052 | |
| Base Conditions | | | Site Conditions | | |
| Length of segment, L (mi) | -- | | 0.085227273 | | |
| AADT (veh/day) | AADT _{MAX} = 17,800 (veh/day) | | 12,500 | | |
| Lane width (ft.) | 12 | | 10 | | |
| Shoulder width (ft.) | 6 | | Right Shld: | 4 | Left Shld: 4 |
| Shoulder type | Paved | | Right Shld: | Paved | Left Shld: Paved |
| Length of horizontal curve (mi) | 0 | | 0.0 | | |
| Radius of curvature (ft.) | 0 | | 0 | | |
| Spiral transition curve (present/not present) | Not Present | | 0.74 | | |
| Superelevation variance (ft./ft.) | < 0.01 | | | | |
| Grade (%) | 0 | | 0 | | |
| Driveway density (driveways/mile) | 5 | | 0 | | |
| Centerline rumble strips (present/not present) | Not Present | | Not Present | | |
| Passing lanes [present (1 lane) / present (2 lane) / not present]] | Not Present | | Not Present | | |
| Two-way left-turn lane (present/not present) | Not Present | | Not Present | | |
| Roadside hazard rating (1-7 scale) | 3 | | 4 | | |
| Segment lighting (present/not present) | Not Present | | Not Present | | |
| Auto speed enforcement (present/not present) | Not Present | | Not Present | | |
| Calibration Factor, Cr | 1 | | 1.00 | | |

| Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments | | | | | | | | | | | | |
|--|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|-----------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | (1)x(2)x...x(11)x(12) |
| 1.17 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.361 |

| Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments | | | | | | | |
|---|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 0.285 | 2.77 | 1.000 | 0.285 | 1.36 | 1.00 | 0.387 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 0.091 | 1.36 | 1.00 | 0.124 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 0.193 | 1.36 | 1.00 | 0.263 |

| Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments | | | | | | |
|--|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 0.387 | 1.000 | 0.124 | 1.000 | 0.263 |
| | | (2)x(3)TOTAL | | (4)x(5)FI | | (6)x(7)PDO |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 0.047 | 0.038 | 0.005 | 0.184 | 0.048 |
| Collision with bicycle | 0.002 | 0.001 | 0.004 | 0.000 | 0.001 | 0.000 |
| Collision with pedestrian | 0.003 | 0.001 | 0.007 | 0.001 | 0.001 | 0.000 |
| Overtuned | 0.025 | 0.010 | 0.037 | 0.005 | 0.015 | 0.004 |
| Ran off road | 0.521 | 0.202 | 0.545 | 0.068 | 0.505 | 0.133 |
| Other single-vehicle collision | 0.021 | 0.008 | 0.007 | 0.001 | 0.029 | 0.008 |
| Total single-vehicle crashes | 0.693 | 0.268 | 0.638 | 0.079 | 0.735 | 0.193 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.033 | 0.100 | 0.012 | 0.072 | 0.019 |
| Head-on collision | 0.016 | 0.006 | 0.034 | 0.004 | 0.003 | 0.001 |
| Rear-end collision | 0.142 | 0.055 | 0.164 | 0.020 | 0.122 | 0.032 |
| Sideswipe collision | 0.037 | 0.014 | 0.038 | 0.005 | 0.038 | 0.010 |
| Other multiple-vehicle collision | 0.027 | 0.010 | 0.026 | 0.003 | 0.030 | 0.008 |
| Total multiple-vehicle crashes | 0.307 | 0.119 | 0.362 | 0.045 | 0.265 | 0.070 |

| Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments | | | | |
|---|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) | (5) |
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 0.4 | 0.085227273 | 4.5 |
| Fatal and Injury (FI) | 0.321 | 0.1 | 0.085227273 | 1.5 |
| Property Damage Only (PDO) | 0.679 | 0.3 | 0.085227273 | 3.1 |

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Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments

| General Information | | Location Information | |
|---|---|----------------------|---------------------------------------|
| Analyst | Darlene Lam | Roadway | SR 70 |
| Agency or Company | African Consulting Professionals a Consor Com | Roadway Section | Jc Durrance Rd to Greenbrier Ln |
| Date Performed | 08/11/23 | Jurisdiction | FDOT District One |
| | | Analysis Year | 2052 |
| Input Data | | Base Conditions | Site Conditions |
| Length of segment, L (mi) | | -- | 1.637121212 |
| AADT (veh/day) | $AADT_{MAX} = 17,800$ (veh/day) | -- | 12,500 |
| Lane width (ft.) | | 12 | 10 |
| Shoulder width (ft.) | | 6 | Right Shld: 4 Left Shld: 4 |
| Shoulder type | | Paved | Right Shld: Paved Left Shld: Paved |
| Length of horizontal curve (mi) | | 0 | 0.0 |
| Radius of curvature (ft.) | | 0 | 0 |
| Spiral transition curve (present/not present) | | Not Present | 0.74 |
| Superelevation variance (ft./ft.) | | < 0.01 | 0 |
| Grade (%) | | 0 | 0 |
| Driveway density (driveways/mile) | | 5 | 1.2 |
| Centerline rumble strips (present/not present) | | Not Present | Not Present |
| Passing lanes [present (1 lane) / present (2 lane) / not present] | | Not Present | Not Present |
| Two-way left-turn lane (present/not present) | | Not Present | Not Present |
| Roadside hazard rating (1-7 scale) | | 3 | 4 |
| Segment lighting (present/not present) | | Not Present | Not Present |
| Auto speed enforcement (present/not present) | | Not Present | Not Present |
| Calibration Factor, Cr | | 1 | 1.00 |

Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|---------------------|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|-----------------------|
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | (1)x(2)x...x(11)x(12) |
| 1.17 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.361 |

Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|----------------------------|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 5.467 | 0.14 | 1.000 | 5.467 | 1.36 | 1.00 | 7.442 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 1.755 | 1.36 | 1.00 | 2.389 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 3.712 | 1.36 | 1.00 | 5.053 |

Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|----------------------------------|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 7.442 | 1.000 | 2.389 | 1.000 | 5.053 |
| | | (2)x(3)TOTAL | | (4)x(5)FI | | (6)x(7)PDO |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 0.900 | 0.038 | 0.091 | 0.184 | 0.930 |
| Collision with bicycle | 0.002 | 0.015 | 0.004 | 0.010 | 0.001 | 0.005 |
| Collision with pedestrian | 0.003 | 0.022 | 0.007 | 0.017 | 0.001 | 0.005 |
| Overtuned | 0.025 | 0.186 | 0.037 | 0.088 | 0.015 | 0.076 |
| Ran off road | 0.521 | 3.877 | 0.545 | 1.302 | 0.505 | 2.552 |
| Other single-vehicle collision | 0.021 | 0.156 | 0.007 | 0.017 | 0.029 | 0.147 |
| Total single-vehicle crashes | 0.693 | 5.157 | 0.638 | 1.524 | 0.735 | 3.714 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.633 | 0.100 | 0.239 | 0.072 | 0.364 |
| Head-on collision | 0.016 | 0.119 | 0.034 | 0.081 | 0.003 | 0.015 |
| Rear-end collision | 0.142 | 1.057 | 0.164 | 0.392 | 0.122 | 0.616 |
| Sideswipe collision | 0.037 | 0.275 | 0.038 | 0.091 | 0.038 | 0.192 |
| Other multiple-vehicle collision | 0.027 | 0.201 | 0.026 | 0.062 | 0.030 | 0.152 |
| Total multiple-vehicle crashes | 0.307 | 2.285 | 0.362 | 0.865 | 0.265 | 1.339 |

Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) |
|----------------------------|--|--|-----------------------------|------------------------------|
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 7.4 | 1.637121212 | 4.5 |
| Fatal and Injury (FI) | 0.321 | 2.4 | 1.637121212 | 1.5 |
| Property Damage Only (PDO) | 0.679 | 5.1 | 1.637121212 | 3.1 |

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Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments

| General Information | | Location Information | |
|--|---|----------------------|----------------------------------|
| Analyst | Darlene Lam | Roadway | SR 70 |
| Agency or Company | African Consulting Professionals a Consor Com | Roadway Section | Greenbrier Ln to DC Bar Ranch Rd |
| Date Performed | 08/11/23 | Jurisdiction | FDOT District One |
| Input Data | | Analysis Year | 2052 |
| Length of segment, L (mi) | -- | Base Conditions | Site Conditions |
| AADT (veh/day) | AADT _{MAX} = 17,800 (veh/day) | -- | 1.001325758 |
| Lane width (ft.) | 12 | 12 | 10 |
| Shoulder width (ft.) | 6 | Right Shld: 4 | Left Shld: 4 |
| Shoulder type | Paved | Right Shld: Paved | Left Shld: Paved |
| Length of horizontal curve (mi) | 0 | 0.0 | |
| Radius of curvature (ft.) | 0 | 0 | |
| Spiral transition curve (present/not present) | Not Present | 0.74 | |
| Superelevation variance (ft./ft.) | < 0.01 | 0 | |
| Grade (%) | 0 | 0 | |
| Driveway density (driveways/mile) | 5 | 0 | |
| Centerline rumble strips (present/not present) | Not Present | Not Present | |
| Passing lanes [present (1 lane) / present (2 lane) / not present]] | Not Present | Not Present | |
| Two-way left-turn lane (present/not present) | Not Present | Not Present | |
| Roadside hazard rating (1-7 scale) | 3 | 4 | |
| Segment lighting (present/not present) | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | Not Present | Not Present | |
| Calibration Factor, Cr | 1 | 1.00 | |

Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|---------------------|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|-----------------------|
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMR 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | (1)x(2)x...x(11)x(12) |
| 1.17 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.361 |

Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|----------------------------|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 3.344 | 0.24 | 1.000 | 3.344 | 1.36 | 1.00 | 4.552 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 1.073 | 1.36 | 1.00 | 1.461 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 2.271 | 1.36 | 1.00 | 3.091 |

Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|----------------------------------|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 4.552 | 1.000 | 1.461 | 1.000 | 3.091 |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 0.551 | 0.038 | 0.056 | 0.184 | 0.569 |
| Collision with bicycle | 0.002 | 0.009 | 0.004 | 0.006 | 0.001 | 0.003 |
| Collision with pedestrian | 0.003 | 0.014 | 0.007 | 0.010 | 0.001 | 0.003 |
| Overtuned | 0.025 | 0.114 | 0.037 | 0.054 | 0.015 | 0.046 |
| Ran off road | 0.521 | 2.371 | 0.545 | 0.796 | 0.505 | 1.561 |
| Other single-vehicle collision | 0.021 | 0.096 | 0.007 | 0.010 | 0.029 | 0.090 |
| Total single-vehicle crashes | 0.693 | 3.154 | 0.638 | 0.932 | 0.735 | 2.272 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.387 | 0.100 | 0.146 | 0.072 | 0.223 |
| Head-on collision | 0.016 | 0.073 | 0.034 | 0.050 | 0.003 | 0.009 |
| Rear-end collision | 0.142 | 0.646 | 0.164 | 0.240 | 0.122 | 0.377 |
| Sideswipe collision | 0.037 | 0.168 | 0.038 | 0.056 | 0.038 | 0.117 |
| Other multiple-vehicle collision | 0.027 | 0.123 | 0.026 | 0.038 | 0.030 | 0.093 |
| Total multiple-vehicle crashes | 0.307 | 1.397 | 0.362 | 0.529 | 0.265 | 0.819 |

Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) |
|----------------------------|--|--|-----------------------------|------------------------------|
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 4.6 | 1.001325758 | 4.5 |
| Fatal and Injury (FI) | 0.321 | 1.5 | 1.001325758 | 1.5 |
| Property Damage Only (PDO) | 0.679 | 3.1 | 1.001325758 | 3.1 |

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Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments

| General Information | | Location Information | |
|---|---|----------------------|------------------------------------|
| Analyst | Darlene Lam | Roadway | SR 70 |
| Agency or Company | African Consulting Professionals a Consor Com | Roadway Section | DC Bar Ranch Rd to Lyke Rd |
| Date Performed | 08/11/23 | Jurisdiction | FDOT District One |
| | | Analysis Year | 2052 |
| Input Data | | Base Conditions | Site Conditions |
| Length of segment, L (mi) | | -- | 2.574621212 |
| AADT (veh/day) | $AADT_{MAX} = 17,800$ (veh/day) | -- | 12,500 |
| Lane width (ft.) | | 12 | 10 |
| Shoulder width (ft.) | | 6 | Right Shld: 4 Left Shld: 4 |
| Shoulder type | | Paved | Right Shld: Paved Left Shld: Paved |
| Length of horizontal curve (mi) | | 0 | 0.0 |
| Radius of curvature (ft.) | | 0 | 0 |
| Spiral transition curve (present/not present) | | Not Present | 0.74 |
| Superelevation variance (ft./ft.) | | < 0.01 | 0 |
| Grade (%) | | 0 | 0 |
| Driveway density (driveways/mile) | | 5 | 1.6 |
| Centerline rumble strips (present/not present) | | Not Present | Not Present |
| Passing lanes [present (1 lane) / present (2 lane) / not present] | | Not Present | Not Present |
| Two-way left-turn lane (present/not present) | | Not Present | Not Present |
| Roadside hazard rating (1-7 scale) | | 3 | 4 |
| Segment lighting (present/not present) | | Not Present | Not Present |
| Auto speed enforcement (present/not present) | | Not Present | Not Present |
| Calibration Factor, Cr | | 1 | 1.00 |

Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|---------------------|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|-----------------------|
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | (1)x(2)x...x(11)x(12) |
| 1.17 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.361 |

Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|----------------------------|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 8.598 | 0.09 | 1.000 | 8.598 | 1.36 | 1.00 | 11.703 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 2.760 | 1.36 | 1.00 | 3.757 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 5.838 | 1.36 | 1.00 | 7.946 |

Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|----------------------------------|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 11.703 | 1.000 | 3.757 | 1.000 | 7.946 |
| | | (2)x(3)TOTAL | | (4)x(5)FI | | (6)x(7)PDO |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 1.416 | 0.038 | 0.143 | 0.184 | 1.462 |
| Collision with bicycle | 0.002 | 0.023 | 0.004 | 0.015 | 0.001 | 0.008 |
| Collision with pedestrian | 0.003 | 0.035 | 0.007 | 0.026 | 0.001 | 0.008 |
| Overtuned | 0.025 | 0.293 | 0.037 | 0.139 | 0.015 | 0.119 |
| Ran off road | 0.521 | 6.097 | 0.545 | 2.047 | 0.505 | 4.013 |
| Other single-vehicle collision | 0.021 | 0.246 | 0.007 | 0.026 | 0.029 | 0.230 |
| Total single-vehicle crashes | 0.693 | 8.110 | 0.638 | 2.397 | 0.735 | 5.841 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.995 | 0.100 | 0.376 | 0.072 | 0.572 |
| Head-on collision | 0.016 | 0.187 | 0.034 | 0.128 | 0.003 | 0.024 |
| Rear-end collision | 0.142 | 1.662 | 0.164 | 0.616 | 0.122 | 0.969 |
| Sideswipe collision | 0.037 | 0.433 | 0.038 | 0.143 | 0.038 | 0.302 |
| Other multiple-vehicle collision | 0.027 | 0.316 | 0.026 | 0.098 | 0.030 | 0.238 |
| Total multiple-vehicle crashes | 0.307 | 3.593 | 0.362 | 1.360 | 0.265 | 2.106 |

Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) |
|----------------------------|--|--|-----------------------------|------------------------------|
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 11.7 | 2.574621212 | 4.5 |
| Fatal and Injury (FI) | 0.321 | 3.8 | 2.574621212 | 1.5 |
| Property Damage Only (PDO) | 0.679 | 7.9 | 2.574621212 | 3.1 |

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Worksheet 1A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Segments

| General Information | | Location Information | |
|---|---|----------------------|-----------------------------------|
| Analyst | Darlene Lam | Roadway | SR 70 |
| Agency or Company | African Consulting Professionals a Consor Com | Roadway Section | Lyke Rd to Southern Leg of CR 721 |
| Date Performed | 08/11/23 | Jurisdiction | FDOT District One |
| Input Data | | Analysis Year | 2052 |
| Length of segment, L (mi) | -- | Base Conditions | Site Conditions |
| AADT (veh/day) | AADT _{MAX} = 17,800 (veh/day) | -- | 2.362310606 |
| Lane width (ft.) | 12 | 12 | 10 |
| Shoulder width (ft.) | 6 | 6 | 4 |
| Shoulder type | Paved | Right Shld: Paved | Left Shld: Paved |
| Length of horizontal curve (mi) | 0 | 0 | 0.3 |
| Radius of curvature (ft.) | 0 | 0 | 2865 |
| Spiral transition curve (present/not present) | Not Present | Not Present | Not Present |
| Superelevation variance (ft./ft.) | < 0.01 | 0 | 0 |
| Grade (%) | 0 | 0 | 0 |
| Driveway density (driveways/mile) | 5 | 5 | 2.1 |
| Centerline rumble strips (present/not present) | Not Present | Not Present | Not Present |
| Passing lanes [present (1 lane) / present (2 lane) / not present] | Not Present | Not Present | Not Present |
| Two-way left-turn lane (present/not present) | Not Present | Not Present | Not Present |
| Roadside hazard rating (1-7 scale) | 3 | 3 | 4 |
| Segment lighting (present/not present) | Not Present | Not Present | Not Present |
| Auto speed enforcement (present/not present) | Not Present | Not Present | Not Present |
| Calibration Factor, Cr | 1 | 1 | 1.00 |

Worksheet 1B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|---------------------|---------------------------------|---------------------------|---------------------------------------|------------------|--------------------------|----------------------------------|-----------------------|--------------------------------|-------------------------|---------------------|-------------------------------------|-----------------------|
| CMF for Lane Width | CMF for Shoulder Width and Type | CMF for Horizontal Curves | CMF for Super-elevation | CMF for Grades | CMF for Driveway Density | CMF for Centerline Rumble Strips | CMF for Passing Lanes | CMF for Two-Way Left-Turn Lane | CMF for Roadside Design | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF 6r | CMF 7r | CMF 8r | CMF 9r | CMF 10r | CMF 11r | CMF 12r | CMF comb |
| from Equation 10-11 | from Equation 10-12 | from Equation 10-13 | from Equations 10-14, 10-15, or 10-16 | from Table 10-11 | from Equation 10-17 | from Section 10.7.1 | from Section 10.7.1 | from Equation 10-18 & 10-19 | from Equation 10-20 | from Equation 10-21 | from Section 10.7.1 | (1)x(2)x...x(11)x(12) |
| 1.17 | 1.09 | 1.05 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.07 | 1.00 | 1.00 | 1.433 |

Worksheet 1C -- Roadway Segment Crashes for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|----------------------------|--------------------|-----------------------------|------------------------------|-----------------------------------|------------------------|------------------------|--------------------------------------|
| Crash Severity Level | N spf rs | Overdispersion Parameter, k | Crash Severity Distribution | N spf rs by Severity Distribution | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N |
| | from Equation 10-6 | from Equation 10-7 | from Table 10-3 (proportion) | (2)TOTAL x (4) | (13) from Worksheet 1B | | (5)x(6)x(7) |
| Total | 7.889 | 0.10 | 1.000 | 7.889 | 1.43 | 1.00 | 11.308 |
| Fatal and Injury (FI) | -- | -- | 0.321 | 2.532 | 1.43 | 1.00 | 3.630 |
| Property Damage Only (PDO) | -- | -- | 0.679 | 5.357 | 1.43 | 1.00 | 7.678 |

Worksheet 1D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|----------------------------------|-------------------------------------|---------------------------------------|----------------------------------|------------------------------------|-----------------------------------|-------------------------------------|
| Collision Type | Proportion of Collision Type(TOTAL) | N predicted rs (TOTAL) (crashes/year) | Proportion of Collision Type(FI) | N predicted rs (FI) (crashes/year) | Proportion of Collision Type(PDO) | N predicted rs (PDO) (crashes/year) |
| | from Table 10-4 | (8)TOTAL from Worksheet 1C | from Table 10-4 | (8)FI from Worksheet 1C | from Table 10-4 | (8)PDO from Worksheet 1C |
| Total | 1.000 | 11.308 | 1.000 | 3.630 | 1.000 | 7.678 |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.121 | 1.368 | 0.038 | 0.138 | 0.184 | 1.413 |
| Collision with bicycle | 0.002 | 0.023 | 0.004 | 0.015 | 0.001 | 0.008 |
| Collision with pedestrian | 0.003 | 0.034 | 0.007 | 0.025 | 0.001 | 0.008 |
| Overtuned | 0.025 | 0.283 | 0.037 | 0.134 | 0.015 | 0.115 |
| Ran off road | 0.521 | 5.892 | 0.545 | 1.978 | 0.505 | 3.878 |
| Other single-vehicle collision | 0.021 | 0.237 | 0.007 | 0.025 | 0.029 | 0.223 |
| Total single-vehicle crashes | 0.693 | 7.837 | 0.638 | 2.316 | 0.735 | 5.644 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.085 | 0.961 | 0.100 | 0.363 | 0.072 | 0.553 |
| Head-on collision | 0.016 | 0.181 | 0.034 | 0.123 | 0.003 | 0.023 |
| Rear-end collision | 0.142 | 1.606 | 0.164 | 0.595 | 0.122 | 0.937 |
| Sideswipe collision | 0.037 | 0.418 | 0.038 | 0.138 | 0.038 | 0.292 |
| Other multiple-vehicle collision | 0.027 | 0.305 | 0.026 | 0.094 | 0.030 | 0.230 |
| Total multiple-vehicle crashes | 0.307 | 3.472 | 0.362 | 1.314 | 0.265 | 2.035 |

Worksheet 1E -- Summary Results for Rural Two-Lane Two-Way Roadway Segments

| (1) | (2) | (3) | (4) | (5) |
|----------------------------|--|--|-----------------------------|------------------------------|
| Crash severity level | Crash Severity Distribution (proportion) | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (4) from Worksheet 1C | (8) from Worksheet 1C | | (3)/(4) |
| Total | 1.000 | 11.3 | 2.362310606 | 4.8 |
| Fatal and Injury (FI) | 0.321 | 3.6 | 2.362310606 | 1.5 |
| Property Damage Only (PDO) | 0.679 | 7.7 | 2.362310606 | 3.3 |

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| Worksheet 2A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|---|---|----------------------|-----------------------|----------------------------|
| General Information | | Location Information | | |
| Analyst | Darlene Lam | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals a Consor Comp | Intersection | JC Durrance Rd | |
| Date Performed | 08/11/23 | Jurisdiction | FDOT District One | |
| | | Analysis Year | 2052 | |
| Input Data | | Base Conditions | Site Conditions | |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST | |
| AADT _{major} (veh/day) | AADT _{MAX} = 19,500 (veh/day) | -- | 12,500 | |
| AADT _{minor} (veh/day) | AADT _{MAX} = 4,300 (veh/day) | -- | 350 | |
| Intersection skew angle (degrees) [If 4ST, does skew differ for minor legs?] | No | 0 | Skew for Leg 1 (All): | Skew for Leg 2 (4ST only): |
| Number of signalized or uncontrolled approaches with a left-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Number of signalized or uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Intersection lighting (present/not present) | | Not Present | Not Present | |
| Calibration Factor, C | | 1.00 | 0.74 | |

| Worksheet 2B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|--|---|--|---|---|
| (1) CMF for Intersection Skew Angle CMF ₁₁ from Equations 10-22 or 10-23 | (2) CMF for Left-Turn Lanes CMF ₂₁ from Table 10-13 | (3) CMF for Right-Turn Lanes CMF ₃₁ from Table 10-14 | (4) CMF for Lighting CMF ₄₁ from Equation 10-24 | (5) Combined CMF CMF _{COMB} (1)*(2)*(3)*(4) |
| 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

| Worksheet 2C -- Intersection Crashes for Rural Two-Lane Two-Way Roadway Intersections | | | | | | | |
|---|--|---|---|--|--|------------------------------|---|
| (1) Crash Severity Level | (2) N _{spl 3ST, 4ST or 4SG} from Equations 10-8, 10-9, or 10-10 | (3) Overdispersion Parameter, k from Section 10.6.2 | (4) Crash Severity Distribution from Table 10-5 | (5) N _{spl 3ST, 4ST or 4SG by Severity Distribution} (2) _{TOTAL} * (4) | (6) Combined CMFs from (5) of Worksheet 2B | (7) Calibration Factor, C | (8) Predicted average crash frequency, N _{predicted int} (5)*(6)*(7) |
| Total | 1.589 | 0.54 | 1.000 | 1.589 | 1.00 | 0.74 | 1.176 |
| Fatal and Injury (FI) | -- | -- | 0.415 | 0.659 | 1.00 | 0.74 | 0.488 |
| Property Damage Only (PDO) | -- | -- | 0.585 | 0.929 | 1.00 | 0.74 | 0.688 |

| Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Road Intersections | | | | | | |
|--|---|---|--|--|---|---|
| (1) Collision Type | (2) Proportion of Collision Type _{TOTAL} from Table 10-6 | (3) N _{predicted int (TOTAL)} (crashes/year) | (4) Proportion of Collision Type _{FI} from Table 10-6 | (5) N _{predicted int (FI)} (crashes/year) | (6) Proportion of Collision Type _{PDO} from Table 10-6 | (7) N _{predicted int (PDO)} (crashes/year) |
| | | (8) _{TOTAL} from Worksheet 2C | | (8) _{FI} from Worksheet 2C | | (8) _{PDO} from Worksheet 2C |
| Total | 1.000 | 1.176 | 1.000 | 0.488 | 1.000 | 0.688 |
| | | (2)x(3) _{TOTAL} | | (4)x(5) _{FI} | | (6)x(7) _{PDO} |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.019 | 0.022 | 0.008 | 0.004 | 0.026 | 0.018 |
| Collision with bicycle | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Collision with pedestrian | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.001 |
| Overturned | 0.013 | 0.015 | 0.022 | 0.011 | 0.007 | 0.005 |
| Ran off road | 0.244 | 0.287 | 0.240 | 0.117 | 0.247 | 0.170 |
| Other single-vehicle collision | 0.016 | 0.019 | 0.011 | 0.005 | 0.020 | 0.014 |
| Total single-vehicle crashes | 0.294 | 0.346 | 0.283 | 0.138 | 0.302 | 0.208 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.237 | 0.279 | 0.275 | 0.134 | 0.210 | 0.144 |
| Head-on collision | 0.052 | 0.061 | 0.081 | 0.040 | 0.032 | 0.022 |
| Rear-end collision | 0.278 | 0.327 | 0.260 | 0.127 | 0.292 | 0.201 |
| Sideswipe collision | 0.097 | 0.114 | 0.051 | 0.025 | 0.131 | 0.090 |
| Other multiple-vehicle collision | 0.042 | 0.049 | 0.050 | 0.024 | 0.033 | 0.023 |
| Total multiple-vehicle crashes | 0.706 | 0.830 | 0.717 | 0.350 | 0.698 | 0.480 |

| Worksheet 2E -- Summary Results for Rural Two-Lane Two-Way Road Intersections | | |
|---|--|--|
| (1) Crash severity level | (2) Crash Severity Distribution (proportion) (4) from Worksheet 2C | (3) Predicted average crash frequency (crashes / year) (8) from Worksheet 2C |
| Total | 1.000 | 1.2 |
| Fatal and Injury (FI) | 0.415 | 0.5 |
| Property Damage Only (PDO) | 0.585 | 0.7 |

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| Worksheet 2A -- General Information and Input Data for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|---|--|--|--|-------------------------------|
| General Information | | | Location Information | |
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals a Consor Comp 08/11/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Southern Leg of CR 721 FDOT District One 2052 | |
| Input Data | | Base Conditions | Site Conditions | |
| Intersection type (3ST, 4ST, 4SG) | | -- | 4ST | |
| AADT _{major} (veh/day) | AADT _{MAX} = 14,700 (veh/day) | -- | 12,500 | |
| AADT _{minor} (veh/day) | AADT _{MAX} = 3,500 (veh/day) | -- | 4,200 | |
| Intersection skew angle (degrees) [If 4ST, does skew differ for minor legs?] | Yes | 0 | Skew for Leg 1 (All): 36 | Skew for Leg 2 (4ST only): 36 |
| Number of signalized or uncontrolled approaches with a left-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Number of signalized or uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4) | | 0 | 0 | |
| Intersection lighting (present/not present) | | Not Present | Not Present | |
| Calibration Factor, C | | 1.00 | 0.74 | |

| Worksheet 2B -- Crash Modification Factors for Rural Two-Lane Two-Way Roadway Intersections | | | | |
|--|---|--|---|---|
| (1) CMF for Intersection Skew Angle CMF ₁₁ from Equations 10-22 or 10-23 | (2) CMF for Left-Turn Lanes CMF ₂₁ from Table 10-13 | (3) CMF for Right-Turn Lanes CMF ₃₁ from Table 10-14 | (4) CMF for Lighting CMF ₄₁ from Equation 10-24 | (5) Combined CMF CMF _{COMB} (1)*(2)*(3)*(4) |
| 1.21 | 1.00 | 1.00 | 1.00 | 1.21 |

| Worksheet 2C -- Intersection Crashes for Rural Two-Lane Two-Way Roadway Intersections | | | | | | | |
|---|--|---|---|--|--|------------------------------|---|
| (1) Crash Severity Level | (2) N _{spl 3ST, 4ST or 4SG} from Equations 10-8, 10-9, or 10-10 | (3) Overdispersion Parameter, k from Section 10.6.2 | (4) Crash Severity Distribution from Table 10-5 | (5) N _{spl 3ST, 4ST or 4SG by Severity Distribution} (2) _{TOTAL} * (4) | (6) Combined CMFs from (5) of Worksheet 2B | (7) Calibration Factor, C | (8) Predicted average crash frequency, N _{predicted int} (5)*(6)*(7) |
| Total | 8,928 | 0.24 | 1.000 | 8,928 | 1.21 | 0.74 | 8,025 |
| Fatal and Injury (FI) | -- | -- | 0.431 | 3,848 | 1.21 | 0.74 | 3,459 |
| Property Damage Only (PDO) | -- | -- | 0.569 | 5,080 | 1.21 | 0.74 | 4,566 |

| Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Two-Lane Two-Way Road Intersections | | | | | | |
|--|---|---|--|--|---|---|
| (1) Collision Type | (2) Proportion of Collision Type _{TOTAL} from Table 10-6 | (3) N _{predicted int (TOTAL)} (crashes/year) | (4) Proportion of Collision Type _{FI} from Table 10-6 | (5) N _{predicted int (FI)} (crashes/year) | (6) Proportion of Collision Type _{PDO} from Table 10-6 | (7) N _{predicted int (PDO)} (crashes/year) |
| | | (8) _{TOTAL} from Worksheet 2C | | (8) _{FI} from Worksheet 2C | | (8) _{PDO} from Worksheet 2C |
| Total | 1.000 | 8,025 | 1.000 | 3,459 | 1.000 | 4,566 |
| | | (2)x(3) _{TOTAL} | | (4)x(5) _{FI} | | (6)x(7) _{PDO} |
| SINGLE-VEHICLE | | | | | | |
| Collision with animal | 0.010 | 0.080 | 0.006 | 0.021 | 0.014 | 0.064 |
| Collision with bicycle | 0.001 | 0.008 | 0.001 | 0.003 | 0.001 | 0.005 |
| Collision with pedestrian | 0.001 | 0.008 | 0.001 | 0.003 | 0.001 | 0.005 |
| Overturned | 0.005 | 0.040 | 0.006 | 0.021 | 0.004 | 0.018 |
| Ran off road | 0.122 | 0.979 | 0.094 | 0.325 | 0.144 | 0.658 |
| Other single-vehicle collision | 0.008 | 0.064 | 0.004 | 0.014 | 0.010 | 0.046 |
| Total single-vehicle crashes | 0.147 | 1.180 | 0.112 | 0.387 | 0.174 | 0.794 |
| MULTIPLE-VEHICLE | | | | | | |
| Angle collision | 0.431 | 3,459 | 0.532 | 1,840 | 0.354 | 1,616 |
| Head-on collision | 0.040 | 0.321 | 0.060 | 0.208 | 0.025 | 0.114 |
| Rear-end collision | 0.242 | 1,942 | 0.210 | 0.726 | 0.266 | 1,215 |
| Sideswipe collision | 0.101 | 0.810 | 0.044 | 0.152 | 0.144 | 0.658 |
| Other multiple-vehicle collision | 0.039 | 0.313 | 0.042 | 0.145 | 0.037 | 0.169 |
| Total multiple-vehicle crashes | 0.853 | 6,845 | 0.888 | 3,071 | 0.826 | 3,772 |

| Worksheet 2E -- Summary Results for Rural Two-Lane Two-Way Road Intersections | | |
|---|--|--|
| (1) Crash severity level | (2) Crash Severity Distribution (proportion) (4) from Worksheet 2C | (3) Predicted average crash frequency (crashes / year) (8) from Worksheet 2C |
| Total | 1.000 | 8.0 |
| Fatal and Injury (FI) | 0.431 | 3.5 |
| Property Damage Only (PDO) | 0.569 | 4.6 |

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Worksheet 3A -- Predicted and Observed Crashes by Severity and Site Type Using the Site-Specific EB Method

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|--------------------------|--|----------------------|-----------------------|---|-----------------------------|---|--|
| Site type | Predicted average crash frequency (crashes/year) | | | Observed crashes, $N_{observed}$ (crashes/year) | Overdispersion Parameter, k | Weighted adjustment, w Equation A-5 from Part C Appendix | Expected average crash frequency, Equation A-4 from Part C Appendix |
| | $N_{predicted}$ (TOTAL) | $N_{predicted}$ (FI) | $N_{predicted}$ (PDO) | | | | |
| ROADWAY SEGMENTS | | | | | | | |
| Segment1 | 0.387 | 0.124 | 0.263 | | 2.769 | 0.482 | 0.2 |
| Segment2 | 7.442 | 2.389 | 5.053 | | 0.144 | 0.482 | 3.6 |
| Segment3 | 4.552 | 1.461 | 3.091 | | 0.236 | 0.482 | 2.2 |
| Segment4 | 11.703 | 3.757 | 7.946 | | 0.092 | 0.482 | 5.6 |
| Segment5 | 11.308 | 3.630 | 7.678 | | 0.100 | 0.470 | 5.3 |
| Segment6 | | | | | | 1.000 | 0.0 |
| Segment7 | | | | | | 1.000 | 0.0 |
| Segment8 | | | | | | 1.000 | 0.0 |
| INTERSECTIONS | | | | | | | |
| Intersection1 | 0.894 | 0.371 | 0.523 | | 0.540 | 0.675 | 0.6 |
| Intersection2 | 1.176 | 0.488 | 0.688 | | 0.540 | 0.612 | 0.7 |
| Intersection3 | 0.894 | 0.371 | 0.523 | | 0.540 | 0.675 | 0.6 |
| Intersection4 | 0.894 | 0.371 | 0.523 | | 0.540 | 0.675 | 0.6 |
| Intersection5 | 0.894 | 0.371 | 0.523 | | 0.540 | 0.675 | 0.6 |
| Intersection6 | 8.025 | 3.459 | 4.566 | | 0.240 | 0.342 | 2.7 |
| Intersection7 | | | | | | 1.000 | 0.0 |
| Intersection8 | | | | | | 1.000 | 0.0 |
| COMBINED (sum of column) | 48.167 | 16.791 | 31.376 | 0 | -- | -- | 22.8 |

Worksheet 3B -- Site-Specific EB Method Summary Results

| (1) | (2) | (3) |
|----------------------------|---|--|
| Crash severity level | $N_{predicted}$ | $N_{expected}$ |
| Total | (2) _{COMB} from Worksheet 3A 48.167 | (8) _{COMB} from Worksheet 3A 22.8 |
| Fatal and Injury (FI) | (3) _{COMB} from Worksheet 3A 16.791 | (3) _{TOTAL} * (2) _{FI} / (2) _{TOTAL} 7.9 |
| Property Damage Only (PDO) | (4) _{COMB} from Worksheet 3A 31.376 | (3) _{TOTAL} * (2) _{PDO} / (2) _{TOTAL} 14.9 |

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Worksheet 4A -- Predicted and Observed Crashes by Severity and Site Type Using the Project-Level EB Method

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|-------------------------|--|----------------------|-----------------------|---|-----------------------------|---------------------------|-------------------------------|---------------|---------------|---------------|---------------|---------------|
| Site type | Predicted average crash frequency (crashes/year) | | | Observed crashes, $N_{observed}$ (crashes/year) | Overdispersion Parameter, k | N_{w0} | N_{w1} | W_0 | N_0 | w_1 | N_1 | N_{pcomb} |
| | $N_{predicted}$ (TOTAL) | $N_{predicted}$ (FI) | $N_{predicted}$ (PDO) | | | Equation A-8 $(6)^*(2)^2$ | Equation A-9 $sqrt((6)^*(2))$ | Equation A-10 | Equation A-11 | Equation A-12 | Equation A-13 | Equation A-14 |
| ROADWAY SEGMENTS | | | | | | | | | | | | |
| Segment 1 | 0.387 | 0.124 | 0.263 | -- | 2.769 | 0.416 | 1.036 | -- | -- | -- | -- | -- |
| Segment 2 | 7.442 | 2.389 | 5.053 | -- | 0.144 | 7.983 | 1.036 | -- | -- | -- | -- | -- |
| Segment 3 | 4.552 | 1.461 | 3.091 | -- | 0.236 | 4.883 | 1.036 | -- | -- | -- | -- | -- |
| Segment 4 | 11.703 | 3.757 | 7.946 | -- | 0.092 | 12.554 | 1.036 | -- | -- | -- | -- | -- |
| Segment 5 | 11.308 | 3.630 | 7.678 | -- | 0.100 | 12.775 | 1.063 | -- | -- | -- | -- | -- |
| Segment 6 | | | | -- | | | | -- | -- | -- | -- | -- |
| Segment 7 | | | | -- | | | | -- | -- | -- | -- | -- |
| Segment 8 | | | | -- | | | | -- | -- | -- | -- | -- |
| INTERSECTIONS | | | | | | | | | | | | |
| Intersection 1 | 0.894 | 0.371 | 0.523 | -- | 0.540 | 0.431 | 0.695 | -- | -- | -- | -- | -- |
| Intersection 2 | 1.176 | 0.488 | 0.688 | -- | 0.540 | 0.746 | 0.797 | -- | -- | -- | -- | -- |
| Intersection 3 | 0.894 | 0.371 | 0.523 | -- | 0.540 | 0.431 | 0.695 | -- | -- | -- | -- | -- |
| Intersection 4 | 0.894 | 0.371 | 0.523 | -- | 0.540 | 0.431 | 0.695 | -- | -- | -- | -- | -- |
| Intersection 5 | 0.894 | 0.371 | 0.523 | -- | 0.540 | 0.431 | 0.695 | -- | -- | -- | -- | -- |
| Intersection 6 | 8.025 | 3.459 | 4.566 | -- | 0.240 | 15.455 | 1.388 | -- | -- | -- | -- | -- |
| Intersection 7 | | | | -- | | | | -- | -- | -- | -- | -- |
| Intersection 8 | | | | -- | | | | -- | -- | -- | -- | -- |
| COMBINED | 48.167 | 16.791 | 31.376 | | -- | 56.537 | 10.169 | 0.460 | 22.158 | 0.826 | 39.770 | 30.964 |

Worksheet 4B -- Project-Level EB Method Summary Results

| (1) | (2) | (3) |
|----------------------------|---|--|
| Crash severity level | $N_{predicted}$ | $N_{expected}$ |
| Total | (2) _{COMB} from Worksheet 4A 48.167 | (13) _{COMB} from Worksheet 4A 31.0 |
| Fatal and injury (FI) | (3) _{COMB} from Worksheet 4A 16.791 | (3) _{TOTAL} * (2) _{FI} / (2) _{TOTAL} 10.8 |
| Property damage only (PDO) | (4) _{COMB} from Worksheet 4A 31.376 | (3) _{TOTAL} * (2) _{PDO} / (2) _{TOTAL} 20.2 |

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| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|--|--|----------------------|--------------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | Lonesome Island Rd to JC Durrance Rd | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2032 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 0.085227273 | |
| AADT (veh/day) | AADT _{MAX} = 89,300 (veh/day) | | -- | 7,800 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 0.124 | 2.493 | 0.99 | 0.68 | 0.084 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 0.066 | 2.172 | 0.99 | 0.68 | 0.045 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 0.044 | 2.059 | 0.99 | 0.68 | 0.029 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} |
| | | | | | | | | 0.039 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI^a} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI^a} from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI^a} | | (8)*(9) _{PDO} |
| Total | 1.000 | 0.084 | 1.000 | 0.045 | 1.000 | 0.029 | 1.000 | 0.039 |
| Head-on collision | 0.006 | 0.001 | 0.013 | 0.001 | 0.018 | 0.001 | 0.002 | 0.000 |
| Sideswipe collision | 0.043 | 0.004 | 0.027 | 0.001 | 0.022 | 0.001 | 0.053 | 0.002 |
| Rear-end collision | 0.116 | 0.010 | 0.163 | 0.007 | 0.114 | 0.003 | 0.088 | 0.003 |
| Angle collision | 0.043 | 0.004 | 0.048 | 0.002 | 0.045 | 0.001 | 0.041 | 0.002 |
| Single-vehicle collision | 0.768 | 0.064 | 0.727 | 0.032 | 0.778 | 0.023 | 0.792 | 0.031 |
| Other collision | 0.024 | 0.002 | 0.022 | 0.001 | 0.023 | 0.001 | 0.024 | 0.001 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | |
| Total | 0.1 | 0.1 | 1.0 |
| Fatal and Injury (FI) | 0.0 | 0.1 | 0.5 |
| Fatal and Injury ^a (FI ^a) | 0.0 | 0.1 | 0.3 |
| Property Damage Only (PDO) | 0.0 | 0.1 | 0.5 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|--|--|----------------------|---------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | JC Durrance Rd to Greenbrier Ln | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2032 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 1.637121212 | |
| AADT (veh/day) | AADT _{MAX} = 89,300 (veh/day) | | -- | 7,800 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 2.384 | 0.130 | 0.99 | 0.68 | 1.605 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 1.273 | 0.113 | 0.99 | 0.68 | 0.857 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 0.836 | 0.107 | 0.99 | 0.68 | 0.563 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} |
| | | | | | | | | 0.748 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI^a} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI^a} from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI^a} | | (8)*(9) _{PDO} |
| Total | 1.000 | 1.605 | 1.000 | 0.857 | 1.000 | 0.563 | 1.000 | 0.748 |
| Head-on collision | 0.006 | 0.010 | 0.013 | 0.011 | 0.018 | 0.010 | 0.002 | 0.001 |
| Sideswipe collision | 0.043 | 0.069 | 0.027 | 0.023 | 0.022 | 0.012 | 0.053 | 0.040 |
| Rear-end collision | 0.116 | 0.186 | 0.163 | 0.140 | 0.114 | 0.064 | 0.088 | 0.066 |
| Angle collision | 0.043 | 0.069 | 0.048 | 0.041 | 0.045 | 0.025 | 0.041 | 0.031 |
| Single-vehicle collision | 0.768 | 1.233 | 0.727 | 0.623 | 0.778 | 0.438 | 0.792 | 0.593 |
| Other collision | 0.024 | 0.039 | 0.022 | 0.019 | 0.023 | 0.013 | 0.024 | 0.018 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | |
| Total | 1.6 | 1.6 | 1.0 |
| Fatal and Injury (FI) | 0.9 | 1.6 | 0.5 |
| Fatal and Injury ^a (FI ^a) | 0.6 | 1.6 | 0.3 |
| Property Damage Only (PDO) | 0.7 | 1.6 | 0.5 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|--|--|----------------------|----------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | Greenbrier Ln to DC Bar Ranch Rd | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2032 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 1.001325758 | |
| AADT (veh/day) | AADT _{MAX} = 89,300 (veh/day) | | -- | 7,800 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 1.458 | 0.212 | 0.99 | 0.68 | 0.982 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 0.779 | 0.185 | 0.99 | 0.68 | 0.524 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 0.511 | 0.175 | 0.99 | 0.68 | 0.344 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} |
| | | | | | | | | 0.458 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} ^a from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI} ^a | | (8)*(9) _{PDO} |
| Total | 1.000 | 0.982 | 1.000 | 0.524 | 1.000 | 0.344 | 1.000 | 0.458 |
| Head-on collision | 0.006 | 0.006 | 0.013 | 0.007 | 0.018 | 0.006 | 0.002 | 0.001 |
| Sideswipe collision | 0.043 | 0.042 | 0.027 | 0.014 | 0.022 | 0.008 | 0.053 | 0.024 |
| Rear-end collision | 0.116 | 0.114 | 0.163 | 0.085 | 0.114 | 0.039 | 0.088 | 0.040 |
| Angle collision | 0.043 | 0.042 | 0.048 | 0.025 | 0.045 | 0.015 | 0.041 | 0.019 |
| Single-vehicle collision | 0.768 | 0.754 | 0.727 | 0.381 | 0.778 | 0.268 | 0.792 | 0.362 |
| Other collision | 0.024 | 0.024 | 0.022 | 0.012 | 0.023 | 0.008 | 0.024 | 0.011 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | |
| Total | 1.0 | 1.0 | 1.0 |
| Fatal and Injury (FI) | 0.5 | 1.0 | 0.5 |
| Fatal and Injury ^a (FI ^a) | 0.3 | 1.0 | 0.3 |
| Property Damage Only (PDO) | 0.5 | 1.0 | 0.5 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|--|--|----------------------|-----------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | DC Bar Ranch Rd to Lykes Rd | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2032 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 2.574621212 | |
| AADT (veh/day) | AADT _{MAX} = 89,300 (veh/day) | | -- | 7,800 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 3.750 | 0.083 | 0.99 | 0.68 | 2.524 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 2.002 | 0.072 | 0.99 | 0.68 | 1.348 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 1.314 | 0.068 | 0.99 | 0.68 | 0.885 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} |
| | | | | | | | | 1.177 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI^a} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI^a} from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI^a} | | (8)*(9) _{PDO} |
| Total | 1.000 | 2.524 | 1.000 | 1.348 | 1.000 | 0.885 | 1.000 | 1.177 |
| Head-on collision | 0.006 | 0.015 | 0.013 | 0.018 | 0.018 | 0.016 | 0.002 | 0.002 |
| Sideswipe collision | 0.043 | 0.109 | 0.027 | 0.036 | 0.022 | 0.019 | 0.053 | 0.062 |
| Rear-end collision | 0.116 | 0.293 | 0.163 | 0.220 | 0.114 | 0.101 | 0.088 | 0.104 |
| Angle collision | 0.043 | 0.109 | 0.048 | 0.065 | 0.045 | 0.040 | 0.041 | 0.048 |
| Single-vehicle collision | 0.768 | 1.939 | 0.727 | 0.980 | 0.778 | 0.688 | 0.792 | 0.932 |
| Other collision | 0.024 | 0.061 | 0.022 | 0.030 | 0.023 | 0.020 | 0.024 | 0.028 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | |
| Total | 2.5 | 2.6 | 1.0 |
| Fatal and Injury (FI) | 1.3 | 2.6 | 0.5 |
| Fatal and Injury ^a (FI ^a) | 0.9 | 2.6 | 0.3 |
| Property Damage Only (PDO) | 1.2 | 2.6 | 0.5 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|--|--|----------------------|------------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | Lykes Rd to Southern Leg of CR 721 | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2032 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 2.362310606 | |
| AADT (veh/day) | AADT _{MAX} = 89,300 (veh/day) | | -- | 7,800 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 3.441 | 0.090 | 0.99 | 0.68 | 2.316 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 1.837 | 0.078 | 0.99 | 0.68 | 1.237 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 1.206 | 0.074 | 0.99 | 0.68 | 0.812 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} |
| | | | | | | | | 1.080 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI^a} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI^a} from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI^a} | | (8)*(9) _{PDO} |
| Total | 1.000 | 2.316 | 1.000 | 1.237 | 1.000 | 0.812 | 1.000 | 1.080 |
| Head-on collision | 0.006 | 0.014 | 0.013 | 0.016 | 0.018 | 0.015 | 0.002 | 0.002 |
| Sideswipe collision | 0.043 | 0.100 | 0.027 | 0.033 | 0.022 | 0.018 | 0.053 | 0.057 |
| Rear-end collision | 0.116 | 0.269 | 0.163 | 0.202 | 0.114 | 0.093 | 0.088 | 0.095 |
| Angle collision | 0.043 | 0.100 | 0.048 | 0.059 | 0.045 | 0.037 | 0.041 | 0.044 |
| Single-vehicle collision | 0.768 | 1.779 | 0.727 | 0.899 | 0.778 | 0.632 | 0.792 | 0.855 |
| Other collision | 0.024 | 0.056 | 0.022 | 0.027 | 0.023 | 0.019 | 0.024 | 0.026 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | |
| Total | 2.3 | 2.4 | 1.0 |
| Fatal and Injury (FI) | 1.2 | 2.4 | 0.5 |
| Fatal and Injury ^a (FI ^a) | 0.8 | 2.4 | 0.3 |
| Property Damage Only (PDO) | 1.1 | 2.4 | 0.5 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|--|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Lonesome Island Rd FDOT District One 2032 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 7,800 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 150 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{li}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (F _i) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spt int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 0.575 | 0.460 | 0.50 | 2.20 | 0.634 |
| Fatal and Injury (F _i) | -12.664 | 1.107 | 0.272 | 0.252 | 0.569 | 0.40 | 2.20 | 0.223 |
| Fatal and Injury ^a (F _i ^a) | -11.989 | 1.013 | 0.228 | 0.171 | 0.566 | 0.40 | 2.20 | 0.151 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} |
| | | | | | | | | 0.411 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|---|---|---|---|--|------------------------------------|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{F_i} | N _{predicted int} (F _i) (crashes/year) | Proportion of Collision Type (F _i) from Table 11-9 | N _{predicted int} (F _i ^a) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{F_i} from Worksheet 2C | from Table 11-9 | (7) _{F_i} ^a from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 0.634 | 1.000 | 0.223 | 1.000 | 0.151 | 1.000 | 0.411 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{F_i} | | (6)*(7) _{F_i} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.029 | 0.018 | 0.043 | 0.010 | 0.052 | 0.008 | 0.020 | 0.008 |
| Sideswipe collision | 0.133 | 0.084 | 0.058 | 0.013 | 0.057 | 0.009 | 0.179 | 0.074 |
| Rear-end collision | 0.289 | 0.183 | 0.247 | 0.055 | 0.142 | 0.021 | 0.315 | 0.130 |
| Angle collision | 0.263 | 0.167 | 0.369 | 0.082 | 0.381 | 0.058 | 0.198 | 0.081 |
| Single-vehicle collision | 0.234 | 0.148 | 0.219 | 0.049 | 0.284 | 0.043 | 0.244 | 0.100 |
| Other collision | 0.052 | 0.033 | 0.064 | 0.014 | 0.084 | 0.013 | 0.044 | 0.018 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| | (7) from Worksheet 2C |
| Total | 0.6 |
| Fatal and Injury (F _i) | 0.2 |
| Fatal and Injury ^a (F _i ^a) | 0.2 |
| Property Damage Only (PDO) | 0.4 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|--|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 JC Durrance Rd FDOT District One 2032 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 7,800 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 200 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{li}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (F _i) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spt int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 0.615 | 0.460 | 0.50 | 2.20 | 0.679 |
| Fatal and Injury (F _i) | -12.664 | 1.107 | 0.272 | 0.272 | 0.569 | 0.40 | 2.20 | 0.241 |
| Fatal and Injury ^a (F _i ^a) | -11.989 | 1.013 | 0.228 | 0.182 | 0.566 | 0.40 | 2.20 | 0.161 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} 0.438 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|--|---|---|--|---|--|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{F_i} | N _{predicted int} (F _i) (crashes/year) | Proportion of Collision Type (F _i) from Table 11-9 | N _{predicted int} (F _i ^a) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{F_i} from Worksheet 2C | from Table 11-9 | (7) _{F_i} ^a from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 0.679 | 1.000 | 0.241 | 1.000 | 0.161 | 1.000 | 0.438 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{F_i} | | (6)*(7) _{F_i} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.029 | 0.020 | 0.043 | 0.010 | 0.052 | 0.008 | 0.020 | 0.009 |
| Sideswipe collision | 0.133 | 0.090 | 0.058 | 0.014 | 0.057 | 0.009 | 0.179 | 0.078 |
| Rear-end collision | 0.289 | 0.196 | 0.247 | 0.060 | 0.142 | 0.023 | 0.315 | 0.138 |
| Angle collision | 0.263 | 0.178 | 0.369 | 0.089 | 0.381 | 0.062 | 0.198 | 0.087 |
| Single-vehicle collision | 0.234 | 0.159 | 0.219 | 0.053 | 0.284 | 0.046 | 0.244 | 0.107 |
| Other collision | 0.052 | 0.035 | 0.064 | 0.015 | 0.084 | 0.014 | 0.044 | 0.019 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| | (7) from Worksheet 2C |
| Total | 0.7 |
| Fatal and Injury (F _i) | 0.2 |
| Fatal and Injury ^a (F _i ^a) | 0.2 |
| Property Damage Only (PDO) | 0.4 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|---|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Greenbrier Ln FDOT District One 2032 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 7,800 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 150 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{4l}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (F _i) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spt int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 0.575 | 0.460 | 0.50 | 2.20 | 0.634 |
| Fatal and Injury (F _i) | -12.664 | 1.107 | 0.272 | 0.252 | 0.569 | 0.40 | 2.20 | 0.223 |
| Fatal and Injury ^a (F _i ^a) | -11.989 | 1.013 | 0.228 | 0.171 | 0.566 | 0.40 | 2.20 | 0.151 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} |
| | | | | | | | | 0.411 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|---|---|---|--|---|------------------------------------|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{F_i} | N _{predicted int} (F _i) (crashes/year) | Proportion of Collision Type (F _f) | N _{predicted int} (F _f) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{F_i} from Worksheet 2C | from Table 11-9 | (7) _{F_f} from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 0.634 | 1.000 | 0.223 | 1.000 | 0.151 | 1.000 | 0.411 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{F_i} | | (6)*(7) _{F_f} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.029 | 0.018 | 0.043 | 0.010 | 0.052 | 0.008 | 0.020 | 0.008 |
| Sideswipe collision | 0.133 | 0.084 | 0.058 | 0.013 | 0.057 | 0.009 | 0.179 | 0.074 |
| Rear-end collision | 0.289 | 0.183 | 0.247 | 0.055 | 0.142 | 0.021 | 0.315 | 0.130 |
| Angle collision | 0.263 | 0.167 | 0.369 | 0.082 | 0.381 | 0.058 | 0.198 | 0.081 |
| Single-vehicle collision | 0.234 | 0.148 | 0.219 | 0.049 | 0.284 | 0.043 | 0.244 | 0.100 |
| Other collision | 0.052 | 0.033 | 0.064 | 0.014 | 0.084 | 0.013 | 0.044 | 0.018 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| | (7) from Worksheet 2C |
| Total | 0.6 |
| Fatal and Injury (F _i) | 0.2 |
| Fatal and Injury ^a (F _i ^a) | 0.2 |
| Property Damage Only (PDO) | 0.4 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|---|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 DC Bar Ranch Rd FDOT District One 2032 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 7,800 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 150 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{4l}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (F _i) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spt int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 0.575 | 0.460 | 0.50 | 2.20 | 0.634 |
| Fatal and Injury (F _i) | -12.664 | 1.107 | 0.272 | 0.252 | 0.569 | 0.40 | 2.20 | 0.223 |
| Fatal and Injury ^a (F _i ^a) | -11.989 | 1.013 | 0.228 | 0.171 | 0.566 | 0.40 | 2.20 | 0.151 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} |
| | | | | | | | | 0.411 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|---|---|---|---|--|------------------------------------|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{F_i} | N _{predicted int} (F _i) (crashes/year) | Proportion of Collision Type (F _i) from Table 11-9 | N _{predicted int} (F _i ^a) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{F_i} from Worksheet 2C | from Table 11-9 | (7) _{F_i} ^a from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 0.634 | 1.000 | 0.223 | 1.000 | 0.151 | 1.000 | 0.411 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{F_i} | | (6)*(7) _{F_i} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.029 | 0.018 | 0.043 | 0.010 | 0.052 | 0.008 | 0.020 | 0.008 |
| Sideswipe collision | 0.133 | 0.084 | 0.058 | 0.013 | 0.057 | 0.009 | 0.179 | 0.074 |
| Rear-end collision | 0.289 | 0.183 | 0.247 | 0.055 | 0.142 | 0.021 | 0.315 | 0.130 |
| Angle collision | 0.263 | 0.167 | 0.369 | 0.082 | 0.381 | 0.058 | 0.198 | 0.081 |
| Single-vehicle collision | 0.234 | 0.148 | 0.219 | 0.049 | 0.284 | 0.043 | 0.244 | 0.100 |
| Other collision | 0.052 | 0.033 | 0.064 | 0.014 | 0.084 | 0.013 | 0.044 | 0.018 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| | (7) from Worksheet 2C |
| Total | 0.6 |
| Fatal and Injury (F _i) | 0.2 |
| Fatal and Injury ^a (F _i ^a) | 0.2 |
| Property Damage Only (PDO) | 0.4 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Build 2032

Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|--|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Lykes Rd FDOT District One 2032 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 7,800 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 150 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{4l}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (F _i) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spt int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 0.575 | 0.460 | 0.50 | 2.20 | 0.634 |
| Fatal and Injury (F _i) | -12.664 | 1.107 | 0.272 | 0.252 | 0.569 | 0.40 | 2.20 | 0.223 |
| Fatal and Injury ^a (F _i ^a) | -11.989 | 1.013 | 0.228 | 0.171 | 0.566 | 0.40 | 2.20 | 0.151 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} |
| | | | | | | | | 0.411 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|---|---|---|---|--|------------------------------------|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{F_i} | N _{predicted int} (F _i) (crashes/year) | Proportion of Collision Type (F _i) from Table 11-9 | N _{predicted int} (F _i ^a) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{F_i} from Worksheet 2C | from Table 11-9 | (7) _{F_i} ^a from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 0.634 | 1.000 | 0.223 | 1.000 | 0.151 | 1.000 | 0.411 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{F_i} | | (6)*(7) _{F_i} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.029 | 0.018 | 0.043 | 0.010 | 0.052 | 0.008 | 0.020 | 0.008 |
| Sideswipe collision | 0.133 | 0.084 | 0.058 | 0.013 | 0.057 | 0.009 | 0.179 | 0.074 |
| Rear-end collision | 0.289 | 0.183 | 0.247 | 0.055 | 0.142 | 0.021 | 0.315 | 0.130 |
| Angle collision | 0.263 | 0.167 | 0.369 | 0.082 | 0.381 | 0.058 | 0.198 | 0.081 |
| Single-vehicle collision | 0.234 | 0.148 | 0.219 | 0.049 | 0.284 | 0.043 | 0.244 | 0.100 |
| Other collision | 0.052 | 0.033 | 0.064 | 0.014 | 0.084 | 0.013 | 0.044 | 0.018 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| | (7) from Worksheet 2C |
| Total | 0.6 |
| Fatal and Injury (F _i) | 0.2 |
| Fatal and Injury ^a (F _i ^a) | 0.2 |
| Property Damage Only (PDO) | 0.4 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Build 2032

Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|--|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Southern Leg of CR FDOT District One 2032 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 4ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 7,800 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 7,400 (veh/day) | -- | 2,700 |
| Intersection skew angle (degrees) | | 0 | 36 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 2 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 3 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 1.64 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{li}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.09 | 0.52 | 0.74 | 0.90 | 0.38 |
| Fatal and Injury (F _i) | 1.10 | 0.42 | 0.59 | 0.90 | 0.24 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|---|-------|--------------|--|--|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients from Table 11-7 or 11-8 | | | N _{spf int} from Equation 11-11 or 11-12 | Overdispersion Parameter, k from Table 11-7 or 11-8 | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -10.008 | 0.848 | 0.448 | 3.100 | 0.494 | 0.38 | 1.64 | 1.916 |
| Fatal and Injury (F _i) | -11.554 | 0.888 | 0.525 | 1.737 | 0.742 | 0.24 | 1.64 | 0.693 |
| Fatal and Injury ^a (F _i ^a) | -10.734 | 0.828 | 0.412 | 0.943 | 0.655 | 0.24 | 1.64 | 0.377 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} 1.223 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|--|--|--|---|---|--|---|---|
| Collision Type | Proportion of Collision Type _{TOTAL} from Table 11-9 | N _{predicted int} (TOTAL) (crashes/year) (7) _{TOTAL} from Worksheet 2C | Proportion of Collision Type _{F_i} from Table 11-9 | N _{predicted int} (F _i) (crashes/year) (7) _{F_i} from Worksheet 2C | Proportion of Collision Type (F _f) from Table 11-9 | N _{predicted int} (F _f) (crashes/year) (7) _{F_f} from Worksheet 2C | Proportion of Collision Type (PDO) from Table 11-9 | N _{predicted int} (PDO) (crashes/year) (7) _{PDO} from Worksheet 2C |
| | | | | | | | | |
| Total | 1.000 | 1,916 | 1.000 | 0.693 | 1.000 | 0.377 | 1.000 | 1.223 |
| Head-on collision | 0.016 | 0.031 | 0.018 | 0.012 | 0.023 | 0.009 | 0.015 | 0.018 |
| Sideswipe collision | 0.107 | 0.205 | 0.042 | 0.029 | 0.040 | 0.015 | 0.156 | 0.191 |
| Rear-end collision | 0.228 | 0.437 | 0.213 | 0.148 | 0.108 | 0.041 | 0.240 | 0.294 |
| Angle collision | 0.395 | 0.757 | 0.534 | 0.370 | 0.571 | 0.215 | 0.292 | 0.357 |
| Single-vehicle collision | 0.202 | 0.387 | 0.148 | 0.103 | 0.199 | 0.075 | 0.243 | 0.297 |
| Other collision | 0.052 | 0.100 | 0.045 | 0.031 | 0.059 | 0.022 | 0.054 | 0.066 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|---|
| Crash severity level | Predicted average crash frequency (crashes / year) (7) from Worksheet 2C |
| Total | 1.9 |
| Fatal and Injury (F _i) | 0.7 |
| Fatal and Injury ^a (F _i ^a) | 0.4 |
| Property Damage Only (PDO) | 1.2 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Build 2032

Worksheet 3A -- Predicted and Observed Crashes by Severity and Site Type Using the Site-Specific EB Method

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|---------------------------|--|-----------------------------|------------------------------|--|-----------------------------|---|--|
| Site type | Predicted average crash frequency (crashes/year) | | | Observed crashes, N_{observed} (crashes/year) | Overdispersion Parameter, k | Weighted adjustment, w Equation A-5 from Part C Appendix | Expected average crash frequency, Equation A-4 from Part C Appendix |
| | $N_{\text{predicted}}$ (TOTAL) | $N_{\text{predicted}}$ (FI) | $N_{\text{predicted}}$ (PDO) | | | | |
| ROADWAY SEGMENTS | | | | | | | |
| Divided Multilane - DSeg1 | 0.084 | 0.045 | 0.039 | | 2.493 | 0.828 | 0.069 |
| Divided Multilane - DSeg2 | 1.605 | 0.857 | 0.748 | | 0.130 | 0.828 | 1.328 |
| Divided Multilane - DSeg3 | 0.982 | 0.524 | 0.458 | | 0.212 | 0.828 | 0.813 |
| Divided Multilane - DSeg4 | 2.524 | 1.348 | 1.177 | | 0.083 | 0.828 | 2.089 |
| Divided Multilane - DSeg5 | 2.316 | 1.237 | 1.080 | | 0.090 | 0.828 | 1.917 |
| Segment 6 | | | | | | 1.000 | 0.000 |
| Segment 7 | | | | | | 1.000 | 0.000 |
| Segment 8 | | | | | | 1.000 | 0.000 |
| INTERSECTIONS | | | | | | | |
| Multilane - Int1 | 0.634 | 0.223 | 0.411 | | 0.460 | 0.774 | 0.491 |
| Multilane - Int2 | 0.679 | 0.241 | 0.438 | | 0.460 | 0.762 | 0.517 |
| Multilane - Int3 | 0.634 | 0.223 | 0.411 | | 0.460 | 0.774 | 0.491 |
| Multilane - Int4 | 0.634 | 0.223 | 0.411 | | 0.460 | 0.774 | 0.491 |
| Multilane - Int5 | 0.634 | 0.223 | 0.411 | | 0.460 | 0.774 | 0.491 |
| Multilane - Int6 | 1.916 | 0.693 | 1.223 | | 0.494 | 0.514 | 0.984 |
| Intersection 7 | | | | | | 1.000 | 0.000 |
| Intersection 8 | | | | | | 1.000 | 0.000 |
| COMBINED (sum of column) | 12.643 | 5.836 | 6.806 | 0 | -- | -- | 9.681 |

Worksheet 3B -- Site-Specific EB Method Summary Results

| (1) | (2) | (3) |
|----------------------------|---|---|
| Crash severity level | $N_{\text{predicted}}$ | N_{expected} |
| Total | (2) _{COMB} from Worksheet 3A 12.643 | (8) _{COMB} from Worksheet 3A 9.7 |
| Fatal and injury (FI) | (3) _{COMB} from Worksheet 3A 5.836 | (3) _{TOTAL} * (2) _{FI} / (2) _{TOTAL} 4.5 |
| Property damage only (PDO) | (4) _{COMB} from Worksheet 3A 6.806 | (3) _{TOTAL} * (2) _{PDO} / (2) _{TOTAL} 5.2 |

Build 2032

Worksheet 4A -- Predicted and Observed Crashes by Severity and Site Type Using the Project-Level EB Method

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|--------------------------|--|----------------------|-----------------------|---|-----------------------------|--------------------------|------------------------------|---------------|---------------|---------------|---------------|---------------|
| Site type | Predicted average crash frequency (crashes/year) | | | Observed crashes, $N_{observed}$ (crashes/year) | Overdispersion Parameter, k | N_{w0} | N_{w1} | W_0 | N_0 | w_1 | N_1 | N_{pcomb} |
| | $N_{predicted}$ (TOTAL) | $N_{predicted}$ (FI) | $N_{predicted}$ (PDO) | | | Equation A-8 $(6)*(2)^2$ | Equation A-9 $sqrt((6)*(2))$ | Equation A-10 | Equation A-11 | Equation A-12 | Equation A-13 | Equation A-14 |
| ROADWAY SEGMENTS | | | | | | | | | | | | |
| Segment 1 (Divided) | 0.084 | 0.045 | 0.039 | -- | 2.493 | 0.017 | 0.456 | -- | -- | -- | -- | -- |
| Segment 2 | 1.605 | 0.857 | 0.748 | -- | 0.130 | 0.334 | 0.456 | -- | -- | -- | -- | -- |
| Segment 3 | 0.982 | 0.524 | 0.458 | -- | 0.212 | 0.205 | 0.456 | -- | -- | -- | -- | -- |
| Segment 4 | 2.524 | 1.348 | 1.177 | -- | 0.083 | 0.526 | 0.456 | -- | -- | -- | -- | -- |
| Segment 5 | 2.316 | 1.237 | 1.080 | -- | 0.090 | 0.483 | 0.456 | -- | -- | -- | -- | -- |
| Segment 6 | | | | -- | | | | -- | -- | -- | -- | -- |
| Segment 7 | | | | -- | | | | -- | -- | -- | -- | -- |
| Segment 8 | | | | -- | | | | -- | -- | -- | -- | -- |
| INTERSECTIONS | | | | | | | | | | | | |
| Intersection 1 | 0.634 | 0.223 | 0.411 | -- | 0.460 | 0.185 | 0.540 | -- | -- | -- | -- | -- |
| Intersection 2 | 0.679 | 0.241 | 0.438 | -- | 0.460 | 0.212 | 0.559 | -- | -- | -- | -- | -- |
| Intersection 3 | 0.634 | 0.223 | 0.411 | -- | 0.460 | 0.185 | 0.540 | -- | -- | -- | -- | -- |
| Intersection 4 | 0.634 | 0.223 | 0.411 | -- | 0.460 | 0.185 | 0.540 | -- | -- | -- | -- | -- |
| Intersection 5 | 0.634 | 0.223 | 0.411 | -- | 0.460 | 0.185 | 0.540 | -- | -- | -- | -- | -- |
| Intersection 6 | 1.916 | 0.693 | 1.223 | -- | 0.494 | 1.814 | 0.973 | -- | -- | -- | -- | -- |
| Intersection 7 | | | | -- | | | | -- | -- | -- | -- | -- |
| Intersection 8 | | | | -- | | | | -- | -- | -- | -- | -- |
| COMBINED (sum of column) | 12.643 | 5.836 | 6.806 | | -- | 4.331 | 5.974 | 0.745 | 9.417 | 0.679 | 8.586 | 9.001 |

Worksheet 4B -- Project-Level EB Method Summary Results

| (1) | (2) | (3) |
|----------------------------|---|---|
| Crash severity level | $N_{predicted}$ | $N_{expected}$ |
| Total | (2) _{COMB} from Worksheet 4A 12.6 | (13) _{COMB} from Worksheet 4A 9.0 |
| Fatal and injury (FI) | (3) _{COMB} from Worksheet 4A 5.8 | (3) _{TOTAL} * (2) _{FI} / (2) _{TOTAL} 4.2 |
| Property damage only (PDO) | (4) _{COMB} from Worksheet 4A 6.8 | (3) _{TOTAL} * (2) _{PDO} / (2) _{TOTAL} 4.8 |

Build 2052

| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|--|--|----------------------|--------------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | Lonesome Island Rd to JC Durrance Rd | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2052 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 0.085227273 | |
| AADT (veh/day) | AADT _{MAX} = 89,300 (veh/day) | | -- | 12,500 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 0.204 | 2.493 | 0.99 | 0.68 | 0.137 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 0.104 | 2.172 | 0.99 | 0.68 | 0.070 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 0.066 | 2.059 | 0.99 | 0.68 | 0.044 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} 0.067 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI^a} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI^a} from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| Total | 1.000 | 0.137 | 1.000 | 0.070 | 1.000 | 0.044 | 1.000 | 0.067 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI^a} | | (8)*(9) _{PDO} |
| Head-on collision | 0.006 | 0.001 | 0.013 | 0.001 | 0.018 | 0.001 | 0.002 | 0.000 |
| Sideswipe collision | 0.043 | 0.006 | 0.027 | 0.002 | 0.022 | 0.001 | 0.053 | 0.004 |
| Rear-end collision | 0.116 | 0.016 | 0.163 | 0.011 | 0.114 | 0.005 | 0.088 | 0.006 |
| Angle collision | 0.043 | 0.006 | 0.048 | 0.003 | 0.045 | 0.002 | 0.041 | 0.003 |
| Single-vehicle collision | 0.768 | 0.105 | 0.727 | 0.051 | 0.778 | 0.034 | 0.792 | 0.053 |
| Other collision | 0.024 | 0.003 | 0.022 | 0.002 | 0.023 | 0.001 | 0.024 | 0.002 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | |
| Total | 0.1 | 0.1 | 1.6 |
| Fatal and Injury (FI) | 0.1 | 0.1 | 0.8 |
| Fatal and Injury ^a (FI ^a) | 0.0 | 0.1 | 0.5 |
| Property Damage Only (PDO) | 0.1 | 0.1 | 0.8 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|-----------------------------------|------------------|----------------------|---------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | JC Durrance Rd to Greenbrier Ln | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2052 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 1.637121212 | |
| AADT (veh/day) | AADT _{MAX} = | 89,300 (veh/day) | -- | 12,500 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 3.910 | 0.130 | 0.99 | 0.68 | 2.633 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 2.000 | 0.113 | 0.99 | 0.68 | 1.346 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 1.262 | 0.107 | 0.99 | 0.68 | 0.850 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} |
| | | | | | | | | 1.286 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI^a} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI^a} from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI^a} | | (8)*(9) _{PDO} |
| Total | 1.000 | 2.633 | 1.000 | 1.346 | 1.000 | 0.850 | 1.000 | 1.286 |
| Head-on collision | 0.006 | 0.016 | 0.013 | 0.018 | 0.018 | 0.015 | 0.002 | 0.003 |
| Sideswipe collision | 0.043 | 0.113 | 0.027 | 0.036 | 0.022 | 0.019 | 0.053 | 0.068 |
| Rear-end collision | 0.116 | 0.305 | 0.163 | 0.219 | 0.114 | 0.097 | 0.088 | 0.113 |
| Angle collision | 0.043 | 0.113 | 0.048 | 0.065 | 0.045 | 0.038 | 0.041 | 0.053 |
| Single-vehicle collision | 0.768 | 2.022 | 0.727 | 0.979 | 0.778 | 0.661 | 0.792 | 1.019 |
| Other collision | 0.024 | 0.063 | 0.022 | 0.030 | 0.023 | 0.020 | 0.024 | 0.031 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | |
| Total | 2.6 | 1.6 | 1.6 |
| Fatal and Injury (FI) | 1.3 | 1.6 | 0.8 |
| Fatal and Injury ^a (FI ^a) | 0.8 | 1.6 | 0.5 |
| Property Damage Only (PDO) | 1.3 | 1.6 | 0.8 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|--|--|----------------------|----------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | Greenbrier Ln to DC Bar Ranch Rd | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2052 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 1.001325758 | |
| AADT (veh/day) | AADT _{MAX} = 89,300 (veh/day) | | -- | 12,500 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 2.392 | 0.212 | 0.99 | 0.68 | 1.610 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 1.223 | 0.185 | 0.99 | 0.68 | 0.824 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 0.772 | 0.175 | 0.99 | 0.68 | 0.520 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} |
| | | | | | | | | 0.787 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI^a} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI^a} from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI^a} | | (8)*(9) _{PDO} |
| Total | 1.000 | 1.610 | 1.000 | 0.824 | 1.000 | 0.520 | 1.000 | 0.787 |
| Head-on collision | 0.006 | 0.010 | 0.013 | 0.011 | 0.018 | 0.009 | 0.002 | 0.002 |
| Sideswipe collision | 0.043 | 0.069 | 0.027 | 0.022 | 0.022 | 0.011 | 0.053 | 0.042 |
| Rear-end collision | 0.116 | 0.187 | 0.163 | 0.134 | 0.114 | 0.059 | 0.088 | 0.069 |
| Angle collision | 0.043 | 0.069 | 0.048 | 0.040 | 0.045 | 0.023 | 0.041 | 0.032 |
| Single-vehicle collision | 0.768 | 1.237 | 0.727 | 0.599 | 0.778 | 0.404 | 0.792 | 0.623 |
| Other collision | 0.024 | 0.039 | 0.022 | 0.018 | 0.023 | 0.012 | 0.024 | 0.019 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | |
| Total | 1.6 | 1.0 | 1.6 |
| Fatal and Injury (FI) | 0.8 | 1.0 | 0.8 |
| Fatal and Injury ^a (FI ^a) | 0.5 | 1.0 | 0.5 |
| Property Damage Only (PDO) | 0.8 | 1.0 | 0.8 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|--|--|----------------------|-----------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | DC Bar Ranch Rd to Lykes Rd | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2052 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 2.574621212 | |
| AADT (veh/day) | AADT _{MAX} = 89,300 (veh/day) | | -- | 12,500 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 6.150 | 0.083 | 0.99 | 0.68 | 4.140 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 3.146 | 0.072 | 0.99 | 0.68 | 2.118 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 1.985 | 0.068 | 0.99 | 0.68 | 1.336 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} |
| | | | | | | | | 2.023 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI^a} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI^a} from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI^a} | | (8)*(9) _{PDO} |
| Total | 1.000 | 4.140 | 1.000 | 2.118 | 1.000 | 1.336 | 1.000 | 2.023 |
| Head-on collision | 0.006 | 0.025 | 0.013 | 0.028 | 0.018 | 0.024 | 0.002 | 0.004 |
| Sideswipe collision | 0.043 | 0.178 | 0.027 | 0.057 | 0.022 | 0.029 | 0.053 | 0.107 |
| Rear-end collision | 0.116 | 0.480 | 0.163 | 0.345 | 0.114 | 0.152 | 0.088 | 0.178 |
| Angle collision | 0.043 | 0.178 | 0.048 | 0.102 | 0.045 | 0.060 | 0.041 | 0.083 |
| Single-vehicle collision | 0.768 | 3.180 | 0.727 | 1.539 | 0.778 | 1.040 | 0.792 | 1.602 |
| Other collision | 0.024 | 0.099 | 0.022 | 0.047 | 0.023 | 0.031 | 0.024 | 0.049 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | |
| Total | 4.1 | 2.6 | 1.6 |
| Fatal and Injury (FI) | 2.1 | 2.6 | 0.8 |
| Fatal and Injury ^a (FI ^a) | 1.3 | 2.6 | 0.5 |
| Property Damage Only (PDO) | 2.0 | 2.6 | 0.8 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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| Worksheet 1A -- General Information and Input Data for Rural Multilane Roadway Segments | | | | | |
|---|--|--|----------------------|------------------------------------|--|
| General Information | | | Location Information | | |
| Analyst | Darlene Lam | | Roadway | SR 70 | |
| Agency or Company | American Consulting Professionals | | Roadway Section | Lykes Rd to Southern Leg of CR 721 | |
| Date Performed | 08/14/23 | | Jurisdiction | FDOT District One | |
| | | | Analysis Year | 2052 | |
| Input Data | | | Base Conditions | Site Conditions | |
| Roadway type (divided / undivided) | | | Undivided | Divided | |
| Length of segment, L (mi) | | | -- | 2.362310606 | |
| AADT (veh/day) | AADT _{MAX} = 89,300 (veh/day) | | -- | 12,500 | |
| Lane width (ft.) | | | 12 | 12 | |
| Shoulder width (ft.) - right shoulder width for divided [if differ for directions of travel, use average width] | | | 8 | 10 | |
| Shoulder type - right shoulder type for divided | | | Paved | Composite | |
| Median width (ft.) - for divided only | | | 30 | 40 | |
| Side Slopes - for undivided only | | | 1:7 or flatter | | |
| Lighting (present/not present) | | | Not Present | Not Present | |
| Auto speed enforcement (present/not present) | | | Not Present | Not Present | |
| Calibration Factor, Cr | | | 1.00 | 0.68 | |

| Worksheet 1B (a) -- Crash Modification Factors for Rural Multilane Divided Roadway Segments | | | | | |
|---|------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| (1) | (2) | (3) | (4) | (5) | (6) |
| CMF for Lane Width | CMF for Right Shoulder Width | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| <i>CMF 1rd</i> | <i>CMF 2rd</i> | <i>CMF 3rd</i> | <i>CMF 4rd</i> | <i>CMF 5rd</i> | <i>CMF comb</i> |
| from Equation 11-16 | from Table 11-17 | from Table 11-18 | from Equation 11-17 | from Section 11.7.2 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |

| Worksheet 1C (a) -- Roadway Segment Crashes for Rural Multilane Divided Roadway Segments | | | | | | | | |
|--|------------------|-------|-------|----------|-----------------------------|---------------|------------------------|---|
| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
| Crash Severity Level | SPF Coefficients | | | N spf rd | Overdispersion Parameter, k | Combined CMFs | Calibration Factor, Cr | Predicted average crash frequency, N _{predicted rs(d)} |
| | from Table 11-5 | | | | | | | |
| | a | b | c | | | | | |
| Total | -9.025 | 1.049 | 1.549 | 5.643 | 0.090 | 0.99 | 0.68 | 3.799 |
| Fatal and Injury (FI) | -8.837 | 0.958 | 1.687 | 2.886 | 0.078 | 0.99 | 0.68 | 1.943 |
| Fatal and Injury ^a (FI ^a) | -8.505 | 0.874 | 1.740 | 1.821 | 0.074 | 0.99 | 0.68 | 1.226 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} |
| | | | | | | | | 1.856 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1D (a) -- Crashes by Severity Level and Collision Type for Rural Multilane Divided Roadway Segments | | | | | | | | |
|---|---|---|--|--|--|---|---|---|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted rs(d)} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted rs(d)} (FI) (crashes/year) | Proportion of Collision Type _{FI^a} | N _{predicted rs} (FI ^a) (crashes/year) | Proportion of Collision Type _{PDO} | N _{predicted rs(d)} (PDO) (crashes/year) |
| | from Table 11-6 | (7) _{TOTAL} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI} from Worksheet 1C (a) | from Table 11-6 | (7) _{FI^a} from Worksheet 1C (a) | from Table 11-6 | (7) _{PDO} from Worksheet 1C (a) |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI^a} | | (8)*(9) _{PDO} |
| Total | 1.000 | 3.799 | 1.000 | 1.943 | 1.000 | 1.226 | 1.000 | 1.856 |
| Head-on collision | 0.006 | 0.023 | 0.013 | 0.025 | 0.018 | 0.022 | 0.002 | 0.004 |
| Sideswipe collision | 0.043 | 0.163 | 0.027 | 0.052 | 0.022 | 0.027 | 0.053 | 0.098 |
| Rear-end collision | 0.116 | 0.441 | 0.163 | 0.317 | 0.114 | 0.140 | 0.088 | 0.163 |
| Angle collision | 0.043 | 0.163 | 0.048 | 0.093 | 0.045 | 0.055 | 0.041 | 0.076 |
| Single-vehicle collision | 0.768 | 2.917 | 0.727 | 1.413 | 0.778 | 0.954 | 0.792 | 1.470 |
| Other collision | 0.024 | 0.091 | 0.022 | 0.043 | 0.023 | 0.028 | 0.024 | 0.045 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

| Worksheet 1E -- Summary Results for Rural Multilane Roadway Segments | | | |
|--|--|-----------------------------|------------------------------|
| (1) | (2) | (3) | (4) |
| Crash severity level | Predicted average crash frequency (crashes/year) | Roadway segment length (mi) | Crash rate (crashes/mi/year) |
| | (7) from Worksheet 1C (a) or (b) | | (2)/(3) |
| Total | 3.8 | 2.4 | 1.6 |
| Fatal and Injury (FI) | 1.9 | 2.4 | 0.8 |
| Fatal and Injury ^a (FI ^a) | 1.2 | 2.4 | 0.5 |
| Property Damage Only (PDO) | 1.9 | 2.4 | 0.8 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|--|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Lonesome Island Rd FDOT District One 2052 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 12,500 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 200 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|---|---|--|---|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF ₁) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF ₂) from Table 11-22 | CMF for Right-Turn Lanes (CMF ₃) from Table 11-23 | CMF for Lighting (CMF ₄) from Equation 11-22 | Combined CMF (CMF _{COMB}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (F _i) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spf int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 1.086 | 0.460 | 0.50 | 2.20 | 1.197 |
| Fatal and Injury (F _i) | -12.664 | 1.107 | 0.272 | 0.458 | 0.569 | 0.40 | 2.20 | 0.406 |
| Fatal and Injury ^a (F _i ^a) | -11.989 | 1.013 | 0.228 | 0.294 | 0.566 | 0.40 | 2.20 | 0.260 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} 0.791 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|---|---|---|--|---|------------------------------------|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{F_i} | N _{predicted int} (F _i) (crashes/year) | Proportion of Collision Type (F _f) | N _{predicted int} (F _f) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{F_i} from Worksheet 2C | from Table 11-9 | (7) _{F_f} from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 1.197 | 1.000 | 0.406 | 1.000 | 0.260 | 1.000 | 0.791 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{F_i} | | (6)*(7) _{F_f} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.029 | 0.035 | 0.043 | 0.017 | 0.052 | 0.014 | 0.020 | 0.016 |
| Sideswipe collision | 0.133 | 0.159 | 0.058 | 0.024 | 0.057 | 0.015 | 0.179 | 0.142 |
| Rear-end collision | 0.289 | 0.346 | 0.247 | 0.100 | 0.142 | 0.037 | 0.315 | 0.249 |
| Angle collision | 0.263 | 0.315 | 0.369 | 0.150 | 0.381 | 0.099 | 0.198 | 0.157 |
| Single-vehicle collision | 0.234 | 0.280 | 0.219 | 0.089 | 0.284 | 0.074 | 0.244 | 0.193 |
| Other collision | 0.052 | 0.062 | 0.064 | 0.026 | 0.084 | 0.022 | 0.044 | 0.035 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| | (7) from Worksheet 2C |
| Total | 1.2 |
| Fatal and Injury (F _i) | 0.4 |
| Fatal and Injury ^a (F _i ^a) | 0.3 |
| Property Damage Only (PDO) | 0.8 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|--|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 JC Durrance Rd FDOT District One 2052 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 12,500 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 350 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|-----------------------|---|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF ₁) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2L}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3R}) from Table 11-23 | CMF for Lighting (CMF _{4L}) from Equation 11-22 | Combined CMF (CMF _{COMB}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (FI) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spf int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 1.239 | 0.460 | 0.50 | 2.20 | 1.366 |
| Fatal and Injury (FI) | -12.664 | 1.107 | 0.272 | 0.534 | 0.569 | 0.40 | 2.20 | 0.473 |
| Fatal and Injury ^a (FI ^a) | -11.989 | 1.013 | 0.228 | 0.334 | 0.566 | 0.40 | 2.20 | 0.296 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{FI} 0.893 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|---|--|--|-----------------------------------|--|------------------------------------|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{FI} | N _{predicted int} (FI) (crashes/year) | Proportion of Collision Type (Ff) | N _{predicted int} (FI ^a) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{FI} from Worksheet 2C | from Table 11-9 | (7) _{FI} ^a from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 1.366 | 1.000 | 0.473 | 1.000 | 0.296 | 1.000 | 0.893 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{FI} | | (6)*(7) _{FI} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.029 | 0.040 | 0.043 | 0.020 | 0.052 | 0.015 | 0.020 | 0.018 |
| Sideswipe collision | 0.133 | 0.182 | 0.058 | 0.027 | 0.057 | 0.017 | 0.179 | 0.160 |
| Rear-end collision | 0.289 | 0.395 | 0.247 | 0.117 | 0.142 | 0.042 | 0.315 | 0.281 |
| Angle collision | 0.263 | 0.359 | 0.369 | 0.175 | 0.381 | 0.113 | 0.198 | 0.177 |
| Single-vehicle collision | 0.234 | 0.320 | 0.219 | 0.104 | 0.284 | 0.084 | 0.244 | 0.218 |
| Other collision | 0.052 | 0.071 | 0.064 | 0.030 | 0.084 | 0.025 | 0.044 | 0.039 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| | (7) from Worksheet 2C |
| Total | 1.4 |
| Fatal and Injury (FI) | 0.5 |
| Fatal and Injury ^a (FI ^a) | 0.3 |
| Property Damage Only (PDO) | 0.9 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|---|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Greenbrier Ln FDOT District One 2052 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 12,500 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 200 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{li}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (F _i) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spf int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 1.086 | 0.460 | 0.50 | 2.20 | 1.197 |
| Fatal and Injury (F _i) | -12.664 | 1.107 | 0.272 | 0.458 | 0.569 | 0.40 | 2.20 | 0.406 |
| Fatal and Injury ^a (F _i ^a) | -11.989 | 1.013 | 0.228 | 0.294 | 0.566 | 0.40 | 2.20 | 0.260 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} |
| | | | | | | | | 0.791 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|---|---|---|--|---|------------------------------------|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{F_i} | N _{predicted int} (F _i) (crashes/year) | Proportion of Collision Type (F _f) | N _{predicted int} (F _f) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{F_i} from Worksheet 2C | from Table 11-9 | (7) _{F_f} from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 1.197 | 1.000 | 0.406 | 1.000 | 0.260 | 1.000 | 0.791 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{F_i} | | (6)*(7) _{F_f} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.029 | 0.035 | 0.043 | 0.017 | 0.052 | 0.014 | 0.020 | 0.016 |
| Sideswipe collision | 0.133 | 0.159 | 0.058 | 0.024 | 0.057 | 0.015 | 0.179 | 0.142 |
| Rear-end collision | 0.289 | 0.346 | 0.247 | 0.100 | 0.142 | 0.037 | 0.315 | 0.249 |
| Angle collision | 0.263 | 0.315 | 0.369 | 0.150 | 0.381 | 0.099 | 0.198 | 0.157 |
| Single-vehicle collision | 0.234 | 0.280 | 0.219 | 0.089 | 0.284 | 0.074 | 0.244 | 0.193 |
| Other collision | 0.052 | 0.062 | 0.064 | 0.026 | 0.084 | 0.022 | 0.044 | 0.035 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| Total | (7) from Worksheet 2C 1.2 |
| Fatal and Injury (F _i) | 0.4 |
| Fatal and Injury ^a (F _i ^a) | 0.3 |
| Property Damage Only (PDO) | 0.8 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

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Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|---|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 DC Bar Ranch Rd FDOT District One 2052 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 12,500 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 200 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{li}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (F _i) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|---|-------|--------------|--|--|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients from Table 11-7 or 11-8 | | | N _{spf int} from Equation 11-11 or 11-12 | Overdispersion Parameter, k from Table 11-7 or 11-8 | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 1.086 | 0.460 | 0.50 | 2.20 | 1.197 |
| Fatal and Injury (F _i) | -12.664 | 1.107 | 0.272 | 0.458 | 0.569 | 0.40 | 2.20 | 0.406 |
| Fatal and Injury ^a (F _i ^a) | -11.989 | 1.013 | 0.228 | 0.294 | 0.566 | 0.40 | 2.20 | 0.260 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} 0.791 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|--|--|--|---|---|--|---|---|
| Collision Type | Proportion of Collision Type _{TOTAL} from Table 11-9 | N _{predicted int} (TOTAL) (crashes/year) (7) _{TOTAL} from Worksheet 2C | Proportion of Collision Type _{F_i} from Table 11-9 | N _{predicted int} (F _i) (crashes/year) (7) _{F_i} from Worksheet 2C | Proportion of Collision Type (F _f) from Table 11-9 | N _{predicted int} (F _f) (crashes/year) (7) _{F_f} from Worksheet 2C | Proportion of Collision Type (PDO) from Table 11-9 | N _{predicted int} (PDO) (crashes/year) (7) _{PDO} from Worksheet 2C |
| | | | | | | | | |
| Total | 1.000 | 1.197 | 1.000 | 0.406 | 1.000 | 0.260 | 1.000 | 0.791 |
| Head-on collision | 0.029 | 0.035 | 0.043 | 0.017 | 0.052 | 0.014 | 0.020 | 0.016 |
| Sideswipe collision | 0.133 | 0.159 | 0.058 | 0.024 | 0.057 | 0.015 | 0.179 | 0.142 |
| Rear-end collision | 0.289 | 0.346 | 0.247 | 0.100 | 0.142 | 0.037 | 0.315 | 0.249 |
| Angle collision | 0.263 | 0.315 | 0.369 | 0.150 | 0.381 | 0.099 | 0.198 | 0.157 |
| Single-vehicle collision | 0.234 | 0.280 | 0.219 | 0.089 | 0.284 | 0.074 | 0.244 | 0.193 |
| Other collision | 0.052 | 0.062 | 0.064 | 0.026 | 0.084 | 0.022 | 0.044 | 0.035 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|---|
| Crash severity level | Predicted average crash frequency (crashes / year) (7) from Worksheet 2C |
| Total | 1.2 |
| Fatal and Injury (F _i) | 0.4 |
| Fatal and Injury ^a (F _i ^a) | 0.3 |
| Property Damage Only (PDO) | 0.8 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Build 2052

Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|--|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Lykes Rd FDOT District One 2052 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 3ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 12,500 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 23,000 (veh/day) | -- | 200 |
| Intersection skew angle (degrees) | | 0 | 0 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 1 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 0 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 2.20 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{li}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.00 | 0.56 | 1.00 | 0.90 | 0.50 |
| Fatal and Injury (F _i) | 1.00 | 0.45 | 1.00 | 0.90 | 0.40 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spf int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -12.526 | 1.204 | 0.236 | 1.086 | 0.460 | 0.50 | 2.20 | 1.197 |
| Fatal and Injury (F _i) | -12.664 | 1.107 | 0.272 | 0.458 | 0.569 | 0.40 | 2.20 | 0.406 |
| Fatal and Injury ^a (F _i ^a) | -11.989 | 1.013 | 0.228 | 0.294 | 0.566 | 0.40 | 2.20 | 0.260 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} 0.791 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|---|---|---|--|---|------------------------------------|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{F_i} | N _{predicted int} (F _i) (crashes/year) | Proportion of Collision Type (F _f) | N _{predicted int} (F _f) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{F_i} from Worksheet 2C | from Table 11-9 | (7) _{F_f} from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 1.197 | 1.000 | 0.406 | 1.000 | 0.260 | 1.000 | 0.791 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{F_i} | | (6)*(7) _{F_f} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.029 | 0.035 | 0.043 | 0.017 | 0.052 | 0.014 | 0.020 | 0.016 |
| Sideswipe collision | 0.133 | 0.159 | 0.058 | 0.024 | 0.057 | 0.015 | 0.179 | 0.142 |
| Rear-end collision | 0.289 | 0.346 | 0.247 | 0.100 | 0.142 | 0.037 | 0.315 | 0.249 |
| Angle collision | 0.263 | 0.315 | 0.369 | 0.150 | 0.381 | 0.099 | 0.198 | 0.157 |
| Single-vehicle collision | 0.234 | 0.280 | 0.219 | 0.089 | 0.284 | 0.074 | 0.244 | 0.193 |
| Other collision | 0.052 | 0.062 | 0.064 | 0.026 | 0.084 | 0.022 | 0.044 | 0.035 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|---|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| Total | 1.2 |
| Fatal and Injury (F _i) | 0.4 |
| Fatal and Injury ^a (F _f) | 0.3 |
| Property Damage Only (PDO) | 0.8 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Build 2052

Worksheet 2A -- General Information and Input Data for Rural Multilane Highway Intersections

| General Information | | Location Information | |
|---|--|--|--|
| Analyst Agency or Company Date Performed | Darlene Lam American Consulting Professionals 08/14/23 | Roadway Intersection Jurisdiction Analysis Year | SR 70 Southern Leg of CR FDOT District One 2052 |
| Input Data | | Base Conditions | Site Conditions |
| Intersection type (3ST, 4ST, 4SG) | | -- | 4ST |
| AADT _{major} (veh/day) | AADT _{MAX} = 78,300 (veh/day) | -- | 12,500 |
| AADT _{minor} (veh/day) | AADT _{MAX} = 7,400 (veh/day) | -- | 4,200 |
| Intersection skew angle (degrees) | | 0 | 36 |
| Number of non-STOP-controlled approaches with left-turn lanes (0, 1, 2) | | 0 | 2 |
| Number of non-STOP-controlled approaches with right-turn lanes (0, 1, 2, 3, or 4) | | 0 | 3 |
| Intersection lighting (present/not present) | | Not Present | Present |
| Calibration Factor, C _i | | 1.00 | 1.64 |

Worksheet 2B -- Crash Modification Factors for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) |
|------------------------------------|--|--|---|--|--|
| Crash Severity Level | CMF for Intersection Skew Angle (CMF _{sk}) from Equations 11-18 or 11-20 and 11-19 or 11-21 | CMF for Left-Turn Lanes (CMF _{2l}) from Table 11-22 | CMF for Right-Turn Lanes (CMF _{3r}) from Table 11-23 | CMF for Lighting (CMF _{li}) from Equation 11-22 | Combined CMF (CMF _{comb}) (2)*(3)*(4)*(5) |
| Total | 1.09 | 0.52 | 0.74 | 0.90 | 0.38 |
| Fatal and Injury (F _i) | 1.10 | 0.42 | 0.59 | 0.90 | 0.24 |

Note: The 4-leg Signalized Intersection (4SG) models do not have base conditions and so can only be used for estimation purposes. As a result, there are not CMFs provided for the 4SG condition.

Worksheet 2C -- Intersection Crashes for Rural Multilane Highway Intersections

| (1) | (2) | | | (3) | (4) | (5) | (6) | (7) |
|--|------------------|-------|--------------|----------------------|-----------------------------|--|---------------------------------------|---|
| Crash Severity Level | SPF Coefficients | | | N _{spf int} | Overdispersion Parameter, k | Combined CMFs from (6) of Worksheet 2B | Calibration Factor, C _i | Predicted average crash frequency, N _{predicted int} (3)*(5)*(6) |
| | a | b | c or d (4SG) | | | | | |
| Total | -10.008 | 0.848 | 0.448 | 5.636 | 0.494 | 0.38 | 1.64 | 3.484 |
| Fatal and Injury (F _i) | -11.554 | 0.888 | 0.525 | 3.330 | 0.742 | 0.24 | 1.64 | 1.329 |
| Fatal and Injury ^a (F _i ^a) | -10.734 | 0.828 | 0.412 | 1.672 | 0.655 | 0.24 | 1.64 | 0.668 |
| Property Damage Only (PDO) | -- | -- | -- | -- | -- | -- | -- | (7) _{TOTAL} - (7) _{F_i} |
| | | | | | | | | 2.155 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2D -- Crashes by Severity Level and Collision Type for Rural Multilane Highway Intersections

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|--------------------------|---|---|---|---|--|---|------------------------------------|---|
| Collision Type | Proportion of Collision Type _{TOTAL} | N _{predicted int} (TOTAL) (crashes/year) | Proportion of Collision Type _{F_i} | N _{predicted int} (F _i) (crashes/year) | Proportion of Collision Type (F _f) | N _{predicted int} (F _f) (crashes/year) | Proportion of Collision Type (PDO) | N _{predicted int} (PDO) (crashes/year) |
| | from Table 11-9 | (7) _{TOTAL} from Worksheet 2C | from Table 11-9 | (7) _{F_i} from Worksheet 2C | from Table 11-9 | (7) _{F_f} from Worksheet 2C | from Table 11-9 | (7) _{PDO} from Worksheet 2C |
| Total | 1.000 | 3,484 | 1.000 | 1,329 | 1.000 | 0.668 | 1.000 | 2,155 |
| | | (2)*(3) _{TOTAL} | | (4)*(5) _{F_i} | | (6)*(7) _{F_f} ^a | | (8)*(9) _{PDO} |
| Head-on collision | 0.016 | 0.056 | 0.018 | 0.024 | 0.023 | 0.015 | 0.015 | 0.032 |
| Sideswipe collision | 0.107 | 0.373 | 0.042 | 0.056 | 0.040 | 0.027 | 0.156 | 0.336 |
| Rear-end collision | 0.228 | 0.794 | 0.213 | 0.283 | 0.108 | 0.072 | 0.240 | 0.517 |
| Angle collision | 0.395 | 1.376 | 0.534 | 0.710 | 0.571 | 0.381 | 0.292 | 0.629 |
| Single-vehicle collision | 0.202 | 0.704 | 0.148 | 0.197 | 0.199 | 0.133 | 0.243 | 0.524 |
| Other collision | 0.052 | 0.181 | 0.045 | 0.060 | 0.059 | 0.039 | 0.054 | 0.116 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Worksheet 2E -- Summary Results for Rural Multilane Highway Intersections

| (1) | (2) |
|--|--|
| Crash severity level | Predicted average crash frequency (crashes / year) |
| | (7) from Worksheet 2C |
| Total | 3.5 |
| Fatal and Injury (F _i) | 1.3 |
| Fatal and Injury ^a (F _i ^a) | 0.7 |
| Property Damage Only (PDO) | 2.2 |

NOTE: ^a Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

Build 2052

Worksheet 3A -- Predicted and Observed Crashes by Severity and Site Type Using the Site-Specific EB Method

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|---------------------------|---|-----------------------------|---------------------------------|---|----------------------------------|--|--|
| Site type | Predicted average crash frequency (crashes/year) | | | Observed crashes, N_{observed} (crashes/year) | Overdispersion Parameter, k | Weighted adjustment, w Equation A-5 from Part C Appendix | Expected average crash frequency, Equation A-4 from Part C Appendix |
| | $N_{\text{predicted}}$ (TOTAL) | $N_{\text{predicted}}$ (FI) | $N_{\text{predicted}}$ (PDO) | | | | |
| ROADWAY SEGMENTS | | | | | | | |
| Divided Multilane - DSeg1 | 0.137 | 0.070 | 0.067 | | 2.493 | 0.745 | 0.102 |
| Divided Multilane - DSeg2 | 2.633 | 1.346 | 1.286 | | 0.130 | 0.745 | 1.962 |
| Divided Multilane - DSeg3 | 1.610 | 0.824 | 0.787 | | 0.212 | 0.745 | 1.200 |
| Divided Multilane - DSeg4 | 4.140 | 2.118 | 2.023 | | 0.083 | 0.745 | 3.086 |
| Divided Multilane - DSeg5 | 3.799 | 1.943 | 1.856 | | 0.090 | 0.745 | 2.831 |
| Segment 6 | | | | | | 1.000 | 0.000 |
| Segment 7 | | | | | | 1.000 | 0.000 |
| Segment 8 | | | | | | 1.000 | 0.000 |
| INTERSECTIONS | | | | | | | |
| Multilane - Int1 | 1.197 | 0.406 | 0.791 | | 0.460 | 0.645 | 0.772 |
| Multilane - Int2 | 1.366 | 0.473 | 0.893 | | 0.460 | 0.614 | 0.839 |
| Multilane - Int3 | 1.197 | 0.406 | 0.791 | | 0.460 | 0.645 | 0.772 |
| Multilane - Int4 | 1.197 | 0.406 | 0.791 | | 0.460 | 0.645 | 0.772 |
| Multilane - Int5 | 1.197 | 0.406 | 0.791 | | 0.460 | 0.645 | 0.772 |
| Multilane - Int6 | 3.484 | 1.329 | 2.155 | | 0.494 | 0.367 | 1.280 |
| Intersection 7 | | | | | | 1.000 | 0.000 |
| Intersection 8 | | | | | | 1.000 | 0.000 |
| COMBINED (sum of column) | 21.959 | 9.728 | 12.231 | 0 | -- | -- | 14.390 |

Worksheet 3B -- Site-Specific EB Method Summary Results

| (1) | (2) | (3) |
|----------------------------|---|---|
| Crash severity level | $N_{\text{predicted}}$ | N_{expected} |
| Total | (2) _{COMB} from Worksheet 3A 21.959 | (8) _{COMB} from Worksheet 3A 14.4 |
| Fatal and injury (FI) | (3) _{COMB} from Worksheet 3A 9.728 | (3) _{TOTAL} * (2) _{FI} / (2) _{TOTAL} 6.4 |
| Property damage only (PDO) | (4) _{COMB} from Worksheet 3A 12.231 | (3) _{TOTAL} * (2) _{PDO} / (2) _{TOTAL} 8.0 |

Build 2052

Worksheet 4A -- Predicted and Observed Crashes by Severity and Site Type Using the Project-Level EB Method

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
|--------------------------|--|----------------------|-----------------------|---|-----------------------------|--------------------------|------------------------------|---------------|---------------|---------------|---------------|---------------|
| Site type | Predicted average crash frequency (crashes/year) | | | Observed crashes, $N_{observed}$ (crashes/year) | Overdispersion Parameter, k | N_{w0} | N_{w1} | W_0 | N_0 | w_1 | N_1 | N_{pcomb} |
| | $N_{predicted}$ (TOTAL) | $N_{predicted}$ (FI) | $N_{predicted}$ (PDO) | | | Equation A-8 $(6)*(2)^2$ | Equation A-9 $sqrt((6)*(2))$ | Equation A-10 | Equation A-11 | Equation A-12 | Equation A-13 | Equation A-14 |
| ROADWAY SEGMENTS | | | | | | | | | | | | |
| Segment 1 (Divided) | 0.137 | 0.070 | 0.067 | -- | 2.493 | 0.047 | 0.585 | -- | -- | -- | -- | -- |
| Segment 2 | 2.633 | 1.346 | 1.286 | -- | 0.130 | 0.899 | 0.585 | -- | -- | -- | -- | -- |
| Segment 3 | 1.610 | 0.824 | 0.787 | -- | 0.212 | 0.550 | 0.585 | -- | -- | -- | -- | -- |
| Segment 4 | 4.140 | 2.118 | 2.023 | -- | 0.083 | 1.414 | 0.585 | -- | -- | -- | -- | -- |
| Segment 5 | 3.799 | 1.943 | 1.856 | -- | 0.090 | 1.298 | 0.585 | -- | -- | -- | -- | -- |
| Segment 6 | | | | -- | | | | -- | -- | -- | -- | -- |
| Segment 7 | | | | -- | | | | -- | -- | -- | -- | -- |
| Segment 8 | | | | -- | | | | -- | -- | -- | -- | -- |
| INTERSECTIONS | | | | | | | | | | | | |
| Intersection 1 | 1.197 | 0.406 | 0.791 | -- | 0.460 | 0.660 | 0.742 | -- | -- | -- | -- | -- |
| Intersection 2 | 1.366 | 0.473 | 0.893 | -- | 0.460 | 0.859 | 0.793 | -- | -- | -- | -- | -- |
| Intersection 3 | 1.197 | 0.406 | 0.791 | -- | 0.460 | 0.660 | 0.742 | -- | -- | -- | -- | -- |
| Intersection 4 | 1.197 | 0.406 | 0.791 | -- | 0.460 | 0.660 | 0.742 | -- | -- | -- | -- | -- |
| Intersection 5 | 1.197 | 0.406 | 0.791 | -- | 0.460 | 0.660 | 0.742 | -- | -- | -- | -- | -- |
| Intersection 6 | 3.484 | 1.329 | 2.155 | -- | 0.494 | 5.997 | 1.312 | -- | -- | -- | -- | -- |
| Intersection 7 | | | | -- | | | | -- | -- | -- | -- | -- |
| Intersection 8 | | | | -- | | | | -- | -- | -- | -- | -- |
| COMBINED (sum of column) | 21.959 | 9.728 | 12.231 | | -- | 13.703 | 7.996 | 0.616 | 13.521 | 0.733 | 16.097 | 14.809 |

Worksheet 4B -- Project-Level EB Method Summary Results

| (1) | (2) | (3) |
|----------------------------|---|---|
| Crash severity level | $N_{predicted}$ | $N_{expected}$ |
| Total | (2) _{COMB} from Worksheet 4A 22.0 | (13) _{COMB} from Worksheet 4A 14.8 |
| Fatal and injury (FI) | (3) _{COMB} from Worksheet 4A 9.7 | (3) _{TOTAL} * (2) _{FI} / (2) _{TOTAL} 6.6 |
| Property damage only (PDO) | (4) _{COMB} from Worksheet 4A 12.2 | (3) _{TOTAL} * (2) _{PDO} / (2) _{TOTAL} 8.2 |

HSM Predictive Method Comparison
 SR 70
 Analysis Years: 2032 to 2052
 Dlam, 8/15/2023

| HSM Predicted Crashes ² | | | |
|--|-------------------------|---------------|---------------------|
| Opening Year 2032 | | | |
| | No-Build | Build | |
| Fatal/Injury | 11.042 | 5.836 | |
| Prop Damage Only | 20.389 | 6.806 | |
| Total | 31.431 | 12.642 | |
| | | | |
| Avg Cost per Fatal/Inj Crash ¹ | \$ 1,031,178.59 | \$ | 883,459.08 |
| Avg Cost per Prop Damage Only Crash ¹ | \$ 4,034.80 | \$ | 3,842.30 |
| | | | |
| Cost for all predicted Fatal/Inj Crash ¹ | \$ 11,386,274.02 | \$ | 5,155,867.22 |
| Cost for all predicted Prop Damage Only Crash ¹ | \$ 82,265.54 | \$ | 26,150.69 |
| Total | \$ 11,468,539.55 | \$ | 5,182,017.91 |
| Design Year 2052 | | | |
| | Fatal/Injury | 16.791 | 9.728 |
| | Prop Damage Only | 31.376 | 12.231 |
| Total | 48.167 | 21.959 | |
| | | | |
| Avg Cost per Fatal/Inj Crash ¹ | \$ 1,031,178.59 | \$ | 883,459.08 |
| Avg Cost per Prop Damage Only Crash ¹ | \$ 4,034.80 | \$ | 3,842.30 |
| | | | |
| Cost for all predicted Fatal/Inj Crash ¹ | \$ 17,314,519.75 | \$ | 8,594,289.98 |
| Cost for all predicted Prop Damage Only Crash ¹ | \$ 126,595.88 | \$ | 46,995.17 |
| Total | \$ 17,441,115.63 | \$ | 8,641,285.15 |

Cumulative Predicted Cost of Crash 2032-52 (Present Day Costs)

| Crash Type | No Build | Build |
|-------------------|--------------------------|--------------------------|
| Fatal/Injury | \$ 301,358,334.51 | \$ 144,376,650.53 |
| Prop. Damage Only | \$ 2,193,044.93 | \$ 768,031.58 |
| Total | \$ 303,551,379.45 | \$ 145,144,682.12 |

Percent Difference of Predicted 2032-52 Cost of Build vs No-Build

| Crash Type | Build\$ / No-Build\$ | % Difference | |
|-------------------|----------------------|--------------|--------------|
| Fatal/Injury | 0.48 | 52% | lower |
| Prop. Damage Only | 0.35 | 65% | lower |
| Total | 0.48 | 52% | lower |

¹ Avg Cost per crash based on KABCO factors and Costs per FDM Chapter 122

| | No-Build R2LUndiv | Build R4LDiv | |
|------------|-------------------|--------------|-------|
| Fatal | \$ 10,890,000 | 0.033 | 0.028 |
| Sev Injury | \$ 888,030 | 0.093 | 0.9 |
| Mod Injur | \$ 180,180 | 0.164 | 0.187 |
| Minor Inju | \$ 103,950 | 0.186 | 0.196 |
| PDO | \$ 7,700 | 0.524 | 0.499 |

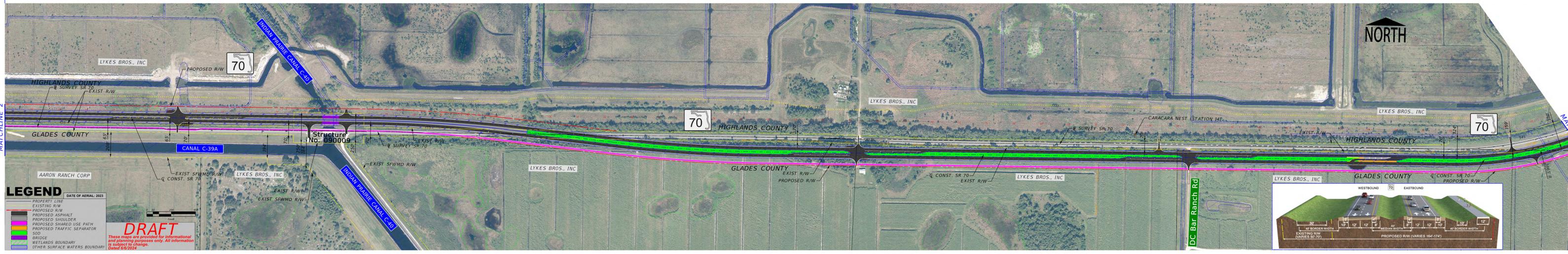
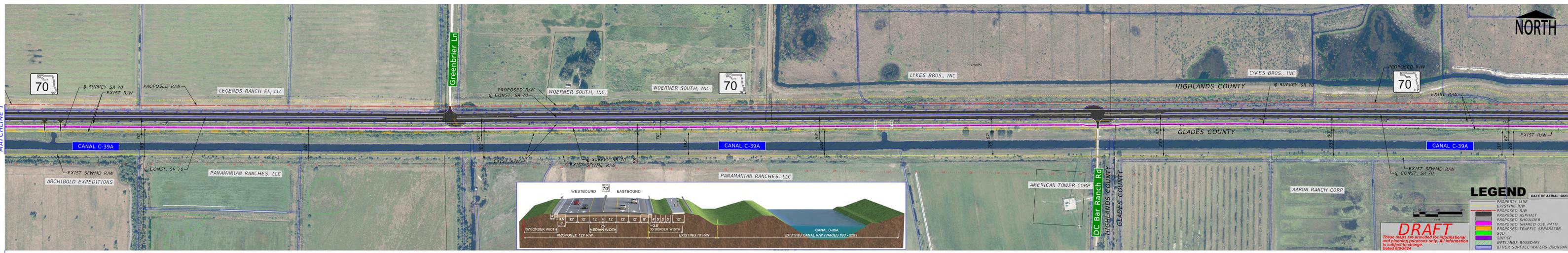
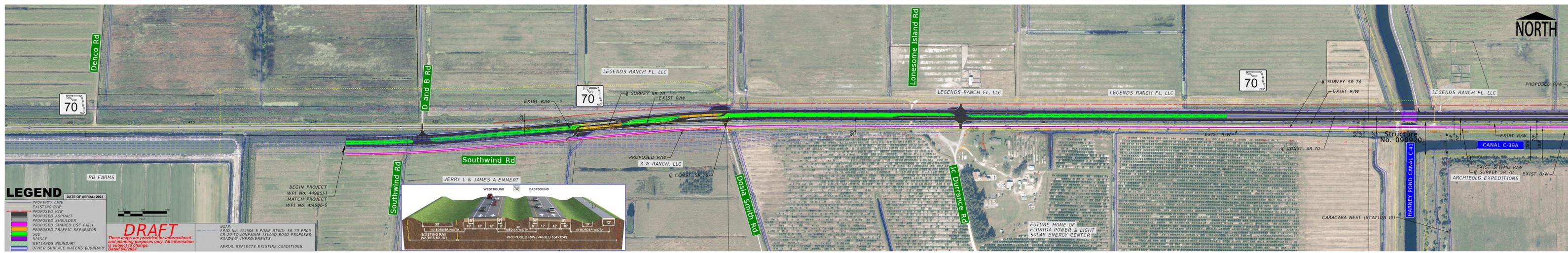
Avg Cost Calculated

| | | |
|----------------|-----------------|---------------|
| Fatal & Injury | \$ 1,031,178.59 | \$ 883,459.08 |
| PDO | \$ 4,034.80 | \$ 3,842.30 |

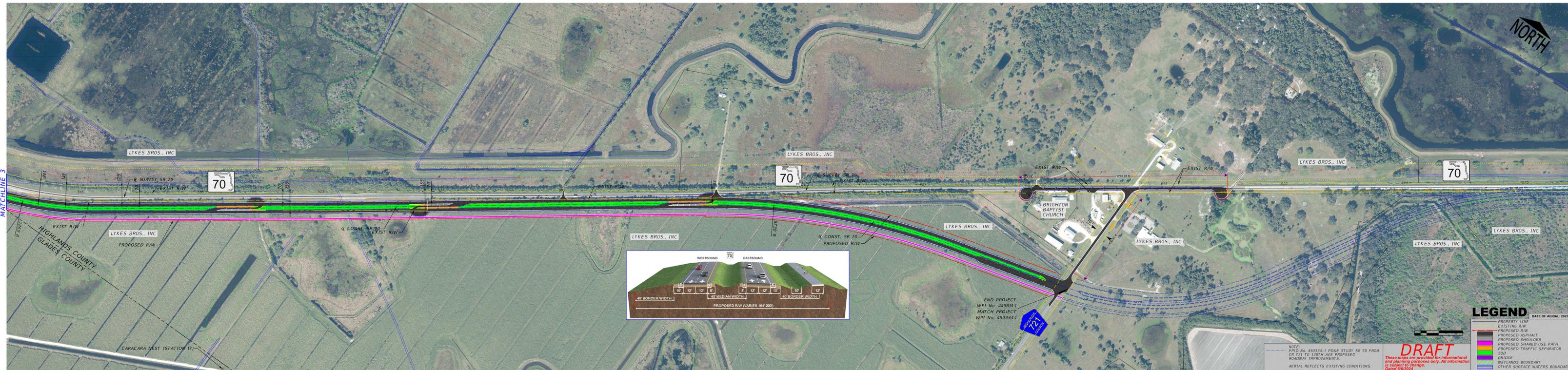
¹ Crash costs and type factors from FDM Chapter 122

² Combined both segment and intersection predicted crashes per HSM sheets

APPENDIX K: Preliminary Roadway Design Concepts



SR 70 from LONESOME ISLAND RD to SOUTHERN LEG CR 721
FPID 449851-1-22-01



SR 70 from LONESOME ISLAND RD to SOUTHERN LEG CR 721
 FPID 449851-1-22-01

